RESEARCH ARTICLE

Orderings of component level versus system level at active redundancies for coherent systems with dependent components

Rongfang Yan D, Junrui Wang D and Bin Lu

College of Mathematics and Statistics, Northwest Normal University, Lanzhou 730070, China. E-mail: yanrf@nwnu.edu.cn.

Keywords: active redundancy, coherent system, copula, distorted distribution, relative aging, stochastic orders

Abstract

This paper investigates the issue of stochastic comparison of multi-active redundancies at the component level versus the system level. Based on the assumption that all components are statistically dependent, in the case of complete matching and nonmatching spares, we present some interesting comparison results in the sense of the hazard rate, reversed hazard rate and likelihood ratio orders, respectively. And we also obtain two comparison results between relative agings of resulting systems at the component level and the system level. Several numerical examples are provided to illustrate the theoretical results.

1. Introduction

In the field of reliability research, redundancy allocation is widely used to improve the reliability of a system. In general, there is a important type of redundancy known as active redundancy commonly used in reliability engineering and system security. Active redundancy means that spares have been attached in parallel to components of system and they start functioning at the same time as original components. The research of this topic is mainly divided into two levels: active redundancy at the component level (ARCL) and at the system level (ARSL). In the former case, the main problem is where to allocate active spares in a system to improve the reliability; see, for example, Boland et al. [6], Li and Ding [25], Li et al. [27], Zhao et al. [52], Zhuang and Li [54], You et al. [48], Fang and Li [12,13], Chen et al. [8], Yan and Luo [43], You and Li [47], Zhang [49], Ling et al. [28], Yan et al. [45], Kim [21], Navarro et al. [36] and Zhang et al. [51]. In the later case, Barlow and Proschan [1] first proposed a wellknown BP principle that ARCL is more reliable ARSL in the sense of usual stochastic ordering for the coherent system with independent components. Over the past few decades, more and more researchers have been digging into the related problems, including whether the BP principle still holds for other stronger stochastic orders, and what effect of dependence among components on BP principle. This study can be divided into three aspects: (1) complete matching, in which all spares and components are identical; (2) matching, in which only the coupled spares and the original components are identical and (3) nonmatching, none of coupled spares has the same distribution as the original components. Based on the assumption that among original components, among spares, and spares and original components are all independent, for complete matching, Boland and El-Neweihi [5], Singh and Singh [41] and Gupta and Nanda [15] have extended the BP principle to the (reversed) hazard rate order and the likelihood ratio order. For matching case, Misra et al. [30], Hazra and Nanda [17] and the references therein devoted to enhance the BP principle to the (reversed) hazard rate order, the likelihood ratio order, and some shifted stochastic orders. However, due to the complexity of distribution theory, there are few results for the case of nonmatching. Misra et al. [30] established the BP principle in the sense of the reversed

[©] The Author(s), 2021. Published by Cambridge University Press

hazard rate order for coherent system with independent identical distributed (i.i.d.) components. Hazra and Nanda [17] and Kuiti *et al.* [24] showed that the BP principle holds in the reversed hazard rate order and the stochastic precedence order for k-out-of-n system with i.i.d. components.

In the past years, under the assumptions that spares are dependent identical distributed (d.i.d.) and independent of original components, some scholars have devoted to study the BP principles of systems with d.i.d. original components. For example, in the case of matching and nonmatching, Gupta and Kumar [14] firstly gave some sufficient or necessary conditions to compare ARCL and ARSL in sense of the likelihood ratio, (reversed) hazard rate, and usual stochastic orders for a general coherent system. Furthermore, for the case of complete matching and nonmatching, based on the framework of possibly heterogeneous multiple redundancy hypothesis, Zhang *et al.* [50] further employed various stochastic orders to study this topic. Recently, based on the work of Zhang *et al.* [50], for the case of matching and nonmatching, Yan and Wang [44] extended the BP principle from d.i.d. original components to dependent nonidentical distributed (d.n.i.d.) components. For more research of the BP principle, refer to Boland and El-Neweihi [5], Brito *et al.* [7], Nanda and Kamal [31], Zhao *et al.* [53], Da and Ding [9] and Kuiti *et al.* [23], among others.

The above results obtained in the literature are carried out under the assumption that spares and original components are independent. However, in practice, affected by the common stress level, all spares and components in a resulting system by ARCL or ARSL may be dependent. Recent years, the research of this issue are lot of attention. Kotz *et al.* [22] studied bounds for the mean lifetime of the system of a original component and one active redundancy component having positively or negatively dependent lifetimes. For series and parallel systems with one redundancy component, Belzunce *et al.* [3,4] investigated the optimal allocation policy under the assumption that the redundancy component and the original component are dependent. Jeddi and Doostparast [19] employed to study the optimal allocation policy in engineering systems with dependent systems formed by modules, including active redundancy at components' level versus redundancies at modules' level. In particularly, under the assumption of dependent components within the modules and dependent modules, they compare the reliability functions of systems formed by possibly dependent modules consisting of heterogeneous components with redundancies at components' levels.

In addition, researcher often come across the following question: how to measure if one system is aging faster than other systems as time progress, like different brands of mobile phones and different engines made by different companies, the most effective way is relative aging. Relative aging includes aging faster orders in the hazard and reversed hazard rates. Kalashnikov and Rachev [20] provided the notion of aging faster orders in the hazard rate, based on the monotonicity of two hazard rate ratios, and Sengupta and Deshpande [39] further proposed the notion of aging faster orders in the reversed hazard rate, based on the monotonicity of two reversed hazard rate ratios. Afterward, Belzunce et al. [2], Misra and Francis [29], Li and Li [26], Ding et al. [11] and Ding and Zhang [10] made further efforts to enrich those existing results in the literature. Few articles were considered relative agings of resulting systems at the component level and the system level. Hazra and Misra [16] not only provided some sufficient conditions for one coherent system to dominate another and a used coherent system and a coherent system made out of used components are compared with respect to aging faster orders, but also, under the assumption that original and redundant components are independent, investigated whether ARCL is more effective than ARSL with respect to aging faster orders in the case of complete matching, however, this work does not take into account the dependence between components and spares.

To sum up, the work of Zhang *et al.* [50], Hazra and Misra [16] and Yan and Wang [44] were derived within the context of independence between spares and original components. As a follow-up, the current article further investigates the case that the vector of the spare lifetimes and the vector of the original component lifetimes are dependent. In this framework, we consider the issue of stochastic comparison of multi-active complete matching and nonmatching spares redundancies at the component level versus the system level, respectively. In particularly, we present some interesting comparison results in the

sense of various stochastic orders, and we also obtain two comparison results between relative agings of resulting systems at the component level and the system level, and thus we effectively extended the corresponding conclusions in Zhang *et al.* [50] and Hazra and Misra [16] and further efforts to enrich those existing results in the literature.

The rest of this paper is organized as follows. Section 2 introduces some preliminaries. Section 3 gives sufficient conditions under which the lifetimes of ARCL and ARSL can be compared by means of some stochastic orders and some numerical examples are provided to illustrate the theoretical results. In Section 4, according to editor suggestion, we present an application in engineering. Finally, Section 5 concludes this study. According to the reviewer's suggestion, all proofs are delegated to the Appendix for ease of presentation.

2. Preliminaries

Throughout the article, increasing and decreasing mean nondecreasing and nonincreasing, respectively. Furthermore, the notion " $a \stackrel{\text{sgn}}{=} b$ " means that "a" and "b" have the same sign, " $=_{\text{st}}$ " means equality in distribution, and the symbols " \lor " and " \land " mean the maximum and the minimum, respectively. It is also assumed that random variables mentioned in this paper are nonnegative and absolutely continuous.

Before proceeding to the main results, let us first recall concepts of stochastic orders, relative aging, copula, distorted distribution and the notion of coherent system, which will be used in the sequel.

For a nonnegative random variable X, denote the distribution function, the survival function, the density function, the hazard rate function and the reversed hazard rate function of X by F_X , \bar{F}_X , f_X , h_X and \tilde{h}_X , respectively.

Definition 1. For two random variables X and Y, X is said to be smaller than Y in the

- (i) usual stochastic order (denoted by $X \leq_{st} Y$) if $\overline{F}_X(t) \leq \overline{F}_Y(t)$ for all $t \in (0, \infty)$;
- (ii) hazard rate order (denoted by $X \leq_{hr} Y$) if $\overline{F}_Y(t)/\overline{F}_X(t)$ is increasing in $t \in (0, \infty)$ or, equivalently, if $h_X(t) \geq h_Y(t)$;
- (iii) reversed hazard rate order (denoted by $X \leq_{rh} Y$) if $F_Y(t)/F_X(t)$ is increasing in $t \in (0, \infty)$ or, equivalently, $\tilde{h}_X(t) \leq \tilde{h}_Y(t)$;
- (iv) likelihood ratio order (denoted by $X \leq_{lr} Y$) if $f_Y(t)/f_X(t)$ is increasing in $t \in (0, \infty)$.

Definition 2. For two random variables X and Y, X is said to be aging faster than Y in

- (i) the hazard rate (denoted by $X \prec_c Y$) if $h_X(t)/h_Y(t)$ is increasing on $(0, +\infty)$ [20];
- (ii) the reversed hazard rate (denoted by $X \prec_b Y$) if $\tilde{h}_Y(t)/\tilde{h}_X(t)$ is increasing on $(0, +\infty)$ [38].

The following implications are well known (see Theorem 1.C.4. in [40])

- (i) $X \leq_{\operatorname{lr}} Y \Longrightarrow X \leq_{\operatorname{hr}} (\leq_{\operatorname{rh}})Y \Longrightarrow X \leq_{\operatorname{st}} Y;$
- (ii) $X \prec_c Y + X \ge_{hr} Y \Longrightarrow X \ge_{lr} Y;$
- (iii) $X \prec_b Y + X \leq_{\text{rh}} Y \Rightarrow X \leq_{\text{lr}} Y$.

For more details of stochastic orders and their applications, refer to Shaked and Shantikumar [40].

Definition 3. A copula is a function $C : I^n \to I$ with the following properties:

- (*i*) $C(v_1, v_2 ... v_n)$ is increasing in v_i , i = 1, 2, ..., n,
- (*ii*) $C(1,...,1,v_i,1,...1) = v_i$, for all i = 1, 2, ..., n,
- (*iii*) C(0,...,0) = 0 and C(1,...,1) = 1, and

(iv) for any $x_1, x_2, \ldots, x_n, y_1, y_2, \ldots, y_n$, if $x_j \le y_j, j = 1, 2, \ldots, n$, then

$$\sum_{i_1=1}^2 \sum_{i_2=1}^2 \cdots \sum_{i_n=1}^2 (-1)^{i_1+i_2+\cdots+i_n} C(v_{1i_1}, u_{2i_2}, \ldots, v_{ni_n}),$$

where $v_{j1} = x_j, v_{j2} = y_j, j = 1, 2, ..., n$.

The following Lemma is very useful in sequel.

Lemma 1 ([37.)] Let $C : I^n \to I$ be a copula. Then, for any $v_j \in [0, 1]$, j = 1, 2, ..., n, the partial derivative $\partial C(v_1, v_2, ..., v_n)/\partial v_i$ exits for almost all v_i ($i \neq j = 1, 2, ..., n$), and for such v_i (i = 1, 2, ..., n),

$$0 \le \frac{\partial C(v_1, v_2, \dots, v_n)}{\partial v_i} \le 1.$$
(1)

In particular, when $v_1 = v_2 = \cdots = v_n = v$, denote $\beta_n(v) = C(v, v, \dots, v)$, for all $v \in (0, 1)$. For more details of copula, refer to Nelsen [37].

A system is called a coherent system, if the system structure function is increasing in each component and all components in the system are relevant. In other words, an improvement of a component cannot lead to a deterioration in the performance of the system.

For a general coherent system with *n* dependent heterogeneous components having lifetimes X_1, \ldots, X_n , let $\mathbf{X} = (X_1, \ldots, X_n)$, and denote *F*, \overline{F} and *f* the distribution function, the survival function and the density function of X_i ($i = 1, 2, \ldots, n$), respectively. Then, the joint distribution function of \mathbf{X} can be expressed as

$$H(x_1, \dots, x_n) = P(X_1 \le x_1, \dots, X_n \le x_n) = C(F(x_1), \dots, F(x_n)),$$
(2)

where *C* is a copula of X_1, \ldots, X_n . Denote $\tau(\mathbf{X})$ the lifetime of the coherent system. Then, according to Navarro *et al.* [34], the survival function of $\tau(\mathbf{X})$ is

$$\bar{H}_{\tau(\mathbf{X})}(x) = P(\tau(\mathbf{X}) > x) = q(\bar{F}(x)), \quad x \ge 0,$$
(3)

where $q : [0, 1] \mapsto [0, 1]$ is the distortion function of the system, which is increasing continuous and satisfies q(0) = 0, and q(1) = 1, and depends only on the structure function of the system and the survival copula of components.

For more details about distorted distribution, refer to Navarro and Durante [32] and Navarro *et al.* [32].

3. Main results

3.1. System description

Consider a coherent system SO composed of *n* d.i.d. components C_1, C_2, \ldots, C_n . Denote X_i the random lifetime of C_i $(i = 1, 2, \ldots, n)$, and F_1 the X'_i 's common distribution function. For *mn* dependent spares $R_{11}, R_{12}, \ldots, R_{1n}; R_{21}, R_{22}, \ldots, R_{2n}; \ldots; R_{m1}, R_{m2}, \ldots, R_{mn}$, denote $Y_{j1}, Y_{j2}, \ldots, Y_{jn}$ the random lifetimes of spares $R_{j1}, R_{j2}, \ldots, R_{jn}$, respectively $(j = 1, 2, \ldots, m)$. Suppose that $Y_{j1}, Y_{j2}, \ldots, Y_{jn}$ have the common distribution function F_{j+1} $(j = 1, 2, \ldots, m)$. To improve the reliability of the coherent system, we can implement ARCL or ARSL for the system. For ARCL, we first allocate the spares $R_{1i}, R_{2i}, \ldots, R_{mi}$ to component C_i by active redundancy and form a subsystem with lifetime

$$SP_i = X_i \vee Y_{1i} \vee \cdots \vee Y_{mi}, \quad i = 1, 2, \dots, n.$$

And then SP₁, SP₂,..., SP_n can result in a new system having the same structure with the original system. Suppose that the lifetime of the coherent system SO is $\tau(X_1, X_2, ..., X_n)$, and thus the lifetime of the resulting system at ARCL can be expressed as

$$\tau_{\text{ARCL}} = \tau(\text{SP}_1, \text{SP}_2, \dots, \text{SP}_n)$$

= $\tau(X_1 \lor Y_{11} \lor \dots \lor Y_{m1}, X_2 \lor Y_{12} \lor \dots \lor Y_{m2}, \dots, X_n \lor Y_{1n} \lor \dots \lor Y_{mn}).$ (4)

For ARSL, by copying the original coherent system structure, for any j (j = 1, 2, ..., m), we can obtain a coherent subsystem SQ_j composed of spares $R_{j1}, R_{j2}, ..., R_{jn}$, and further form the parallel system of SO, SQ₁, SQ₂,..., SQ_m. Consider that the lifetime of the system SQ_j is $\tau(Y_{j1}, Y_{j2}, ..., Y_{jn})$ (j = 1, 2, ..., m), then the lifetime of the resulting system at ARSL can be written as

$$\tau_{\text{ARSL}} = \vee \{\tau(X_1, X_2, \dots, X_n), \tau(Y_{11}, Y_{12}, \dots, Y_{1n}), \dots, \tau(Y_{m1}, Y_{m2}, \dots, Y_{mn})\}.$$
(5)

Affected by the common stress level, all spares and components in a resulting system by ARCL or ARSL may be dependent. For simplicity, throughout the paper, we always suppose that $SP_1, SP_2, \ldots, SP_n; Y_{j1}, Y_{j2}, \ldots, Y_{jn}$ $(j = 1, 2, \ldots, m)$ and X_1, X_2, \ldots, X_n have the common copula C', and $X_i, Y_{1i}, Y_{2i}, \ldots, Y_{mi}$ $(i = 1, 2, \ldots, n)$ and SO, SQ_1, SQ_2, \ldots, SQ_m also have the common copula C. Then, in the case of noncomplete matching, the survival functions of ARCL and ARSL can be expressed as

$$F_{\text{ARCL}}(u_1, u_2, \dots, u_{m+1}) = P(\tau_{\text{ARCL}} > t) = q(1 - C(u_1, u_2, \dots, u_{m+1}))$$

and

$$\bar{F}_{\text{ARSL}}(u_1, u_2, \dots, u_{m+1})$$

= $P(\tau_{\text{ARSL}} > t) = 1 - C(1 - q(1 - u_1), 1 - q(1 - u_2), \dots, 1 - q(1 - u_{m+1})),$

respectively. Where the distortion function q depend on the system structure and copula C'. In the complete matching case, note that $u_1 = u_2 = \cdots = u_{m+1} = u$, hence the survival functions of ARCL and ARSL are given by

$$F_{\text{ARCL}}(u) = q(1 - \beta_{m+1}(u))$$

and

$$F_{\text{ARSL}}(u) = 1 - \beta_{m+1}(1 - q(1 - u)),$$

respectively.

From convenience, for a differentiable function f, define

$$K_f(x) = \frac{xf'(x)}{f(x)}, \quad L_f(x) = \frac{(1-x)f'(x)}{1-f(x)}.$$

3.2. Complete matching case

In this subsection, we discuss the case of coherent system with d.i.d. components and multiple spares. For the coherent system with d.i.d. components and spares, within independence between spares and original components, assuming that $q(2p - p^2) \ge 2q(p) - (q(p))^2$, Gupta and Kumar [14] proved that

$$\tau_{\text{ARCL}} \ge_{\text{st}} \tau_{\text{ARSL}},\tag{6}$$

which means that ARCL is better than ARSL in the sense of the usual stochastic ordering for a coherent system. However, the spares and original components may be dependent. Therefore, the independence between spares and original components assumption in Eq. (6) seems unreasonable in some practical

scenarios. Next, we firstly provide a sufficient condition to show that ARCL is superior to ARSL in the sense of the usual stochastic ordering under the assumption of dependence between spares and original components.

Theorem 1. It holds that $\tau_{ARCL} \geq_{st} \tau_{ARSL}$, if and only if

$$q(1 - \beta_{m+1}(u)) + \beta_{m+1}(1 - q(1 - u)) \ge 1, \quad \text{for all } u \in (0, 1).$$
(7)

It should be mentioned that Eq. (6) is just the special case of Theorem 1 if m = 1 and $\beta_2(u) = u^2$.

The following example illustrates that under the condition of Theorem 1, $\tau_{ARCL} \ge_{hr} \tau_{ARSL}$ or $\tau_{ARCL} \ge_{rh} \tau_{ARSL}$ not necessarily holds.

Example 1. Consider a coherent system $T = \wedge \{X_1, \forall \{X_2, X_3\}\}$ with identical distributed components X_1, X_2 and X_3 having Clayton-Oakes (CO) copula

$$C'(v_1, v_2, v_3) = \left(\sum_{i=1}^3 v_i^{1-\theta_1} - 2\right)^{1/(1-\theta_1)}, \quad v_i \in [0, 1],$$
(8)

where $\theta_1 > 1$ is a fixed number. Let Y_{11} , Y_{12} and Y_{13} be lifetimes of d.i.d. spares having common survival function and copula (8). Furthermore, suppose

$$C(v_1, v_2) = \frac{v_1 v_2}{1 - \theta_2 (1 - v_1)(1 - v_2)}, \quad v_i \in [0, 1],$$

where $\theta_2 \in [-1, 1]$ is a fixed number. Obvious that, m = 1, and taking $\theta_1 = 2, \theta_2 = 1/2$ then

$$\beta_2(u) = \frac{2u^2}{2 - (1 - u)^2}$$

and the reliability function of this system can be expressed as

$$q(1-u) = \frac{2-2u}{1+u} - \frac{1-u}{1+2u},$$

and for any $u \in [0, 1]$, it follows from

$$q(1 - \beta_3(u)) + \beta_3(1 - q(1 - u)) - 1 = \frac{8(u - 1)^2 u^3 (21u^3 + 19u^2 + 7u + 1)}{(u + 1)^2 (3u^2 + 2u + 1)(-u^4 + 36u^3 + 28u^2 + 8u + 1)}$$

$$\stackrel{\text{sgn}}{=} -u^4 + 36u^3 + 28u^2 + 8u + 1$$

$$= 28 + 36u - u^2 \ge 0,$$

and thus, the condition (7) is satisfied. But Figure 1 shows neither $\tau_{ARCL} \ge_{hr} \tau_{ARSL}$ nor $\tau_{ARCL} \ge_{rh} \tau_{ARSL}$ holds.

Assuming the independence of spares and original components and the framework of multiple redundancies case, under conditions vq'(v)/q(v) is decreasing in $v \in (0, 1)$ and $q(v) \le v$, Zhang *et al.* [50] proved that

$$\tau_{\text{ARCL}} \ge_{\text{hr}} \tau_{\text{ARSL}}.$$
(9)

Similarly, the independence between spares and original components assumption in Eq. (9) seems unreasonable in some practical scenarios. Next, we extend corresponding result to the hypothesis of dependence between spares and original components.



Figure 1. Plots of functions $\overline{F}_{ARCL}/\overline{F}_{ARSL}$ and F_{ARCL}/F_{ARSL} .

Theorem 2. If

- (1) $K_q(1-u)$ is increasing in $u \in (0,1)$,
- (2) $L_{\beta_{m+1}}(u)$ is increasing in $u \in (0, 1)$ and
- (3) $q(1-u) \le 1 u$ for all $u \in (0, 1)$,

then

 $\tau_{\text{ARCL}} \geq_{hr} \tau_{\text{ARSL}}.$

Remark 1. When spares and original components are independent, we have $\beta_{m+1}(u) = u^{m+1}$, it is obvious that $L_{\beta_{m+1}}(u)$ is increasing in $u \in (0, 1)$ and v = 1 - u, Eq. (9) is just the special case of Theorem 2. Theorem 2 also generalizes Theorem 2 of Gupta and Kumar [14] to the case of dependence of spares and components.

The next numerical example serves as a practical support for the condition required in Theorem 2.

Example 2. Consider a coherent system $T = \wedge \{X_1, X_2, X_3, X_4\}$ with identical distributed components X_1, X_2, X_3, X_4 having Gumbel–Barnett copula C'.

$$C'(v_1, v_2, v_3, v_4) = \left(\prod_{1=1}^4 v_i\right) e^{-\theta_1 \prod_{1=1}^4 \log v_i}, \quad v_i \in [0, 1],$$
(10)

where $\theta_1 > 0$. Let Y_{j1} , Y_{j2} , Y_{j3} , Y_{j4} (j = 1, 2) be lifetimes of d.i.d. spares having common survival function and copula (10). Furthermore, suppose

$$C(v_1, v_2, v_3) = \prod_{i=1}^{3} v_i + \theta_2 \prod_{i=1}^{3} v_i (1 - v_i), \quad v_i \in [0, 1],$$
(11)

where $\theta_2 \in [-1, 1]$ is a fixed number. Obvious that, m = 2, then,

$$\beta_3(u) = u^3(1 + \theta_2(1 - u)^3),$$

and the reliability function of this system can be expressed as

$$q(1-u) = (1-u)^4 e^{-\theta_1 (\log(1-u))^4},$$

$$K_{q}(1-u) = \frac{(1-u)q'(1-u)}{q(1-u)} = 4 - 4\theta_{1}(\log(1-u))^{4},$$

$$L_{\beta_{3}}(u) = \frac{(1-u)\beta_{3}'(u)}{1-\beta_{3}(u)} = \frac{3u^{2}(\theta_{2}(1-2u)(1-u)^{2}+1)}{-\theta_{2}u^{5}+2\theta_{2}u^{4}-\theta_{2}u^{3}+u^{2}+u+1}.$$
(12)

According to Example 3.13 of Zhang et al. [50], we know that $K_q(1-u)$ is increasing in u, and $q(1-u) \leq 1-u$, for all $u \in (0, 1)$. It can be verified that the condition (2) in Theorem 2 is satisfied (Appendix A.3). Thus, $\tau_{ARCL} \geq_{hr} \tau_{ARSL}$ holds.

The following Theorem 3 gives the reversed hazard rate ordering between τ_{ARCL} and τ_{ARSL} .

Theorem 3. If

(1) $K_{\beta_{m+1}}(u)$ is decreasing in $u \in (0, 1)$, (2) $L_q(1-u)$ is decreasing in $u \in (0, 1)$ and (3) $q(1-u) \le 1-u$ for all $u \in (0, 1)$,

then

 $\tau_{\text{ARCL}} \geq_{rh} \tau_{\text{ARSL}}$.

The proof could be completed along the same lines as in Theorem 6, and is hence omitted. The next numerical example serves as a practical support for the condition required in Theorem 3.

Example 3. Consider a coherent system $T = \wedge \{X_1, X_2\}$ with identical distributed components X_1 and X_2 , which have Archimedean copula (see Table 4.1 in [37])

$$C'(v_1, v_2) = \max\left\{\frac{\theta^2 v_1 v_2 - (1 - v_1)(1 - v_2)}{\theta^2 - (\theta - 1)^2 (1 - v_1)(1 - v_2)}, 0\right\}, \quad v_1, v_2 \in [0, 1],$$
(13)

where $\theta \in [1, \infty]$ is a fixed number. Let Y_{11} , Y_{12} be lifetimes of d.i.d. spares having common survival function and copula (13). Furthermore, suppose C = C'. It is obvious that m = 1, for all $\theta \in [1, \infty]$, we have

$$\begin{split} F_{\text{ARCL}}(u) &= 1 - q(1 - \beta_2(u)) = \begin{cases} 0, & 0 \le u \le \frac{1}{1+\theta}, \\ \frac{2\theta(\theta u + u - 1)}{2\theta^2 + \theta(u - 2) + 1 - u}, & \frac{1}{1+\theta} \le u < \frac{1 + 2\theta^2}{1 + \theta + 2\theta^2}, \\ \frac{1 + \theta + 2\theta^2}{1 + \theta + 2\theta^2} \le u < 1, \end{cases} \\ F_{\text{ARSL}}(u) &= \beta_2(1 - q(1 - u)) = \begin{cases} 0, & 0 \le u \le \frac{\theta}{1 + \theta + \theta^2}, \\ \frac{2\theta^2 u + \theta(u - 1) + u}{2\theta^2 - \theta(u + 1) + u}, & \frac{\theta}{1 + \theta + \theta^2} \le u < \frac{\theta}{1 + \theta}, \\ 1, & \frac{\theta}{1 + \theta} \le u < 1, \end{cases} \\ L_q(1 - u) &= \frac{uq'(1 - u)}{1 - q(1 - u)} = \begin{cases} \frac{\theta}{\theta + (\theta - 1)u}, & 0 \le u \le \frac{\theta}{1 + \theta}, \\ 0, & \frac{\theta}{1 + \theta} < u \le 1, \end{cases} \\ K_{\beta_2}(u) &= \frac{u\beta_2'(u)}{\beta_2(u)} = \begin{cases} 0, & 0 \le u < \frac{1}{1 + \theta}, \\ \frac{2\theta^2 u}{1 - 2\theta - (1 - \theta)u][1 - (1 + \theta)u]}, & \frac{1}{1 + \theta} \le u \le 1, \end{cases} \end{split}$$

$$\Lambda(u) = \frac{F_{\text{ARCL}}(u)}{F_{\text{ARSL}}(u)} = \begin{cases}
0, & 0 \le u < \frac{1}{1+\theta}, \\
\frac{2\theta(2\theta^2 - \theta u + u - \theta)(\theta u + u - 1)}{(1 - 2\theta + 2\theta^2 - u + \theta u)(2\theta^2 u + \theta u + u - \theta)}, & \frac{1}{1+\theta} \le u < \frac{\theta}{1+\theta}, \\
1 - q(1 - \beta_2(u)), & \frac{\theta}{1+\theta} \le u \le \frac{1 + 2\theta^2}{1+\theta + 2\theta^2}, \\
1, & \frac{1 + 2\theta^2}{1+\theta + 2\theta^2} \le u \le 1.
\end{cases}$$
(14)

For any $\theta \in [1, 3.2]$, to prove $\Lambda(u)$ is increasing in $u \in [0, 1]$, we just need to prove that $\Lambda(u)$ is increasing in $u \in [1/(1+\theta), \theta/(1+\theta)]$. It is obvious that $L_q(1-u)$ is nonnegative and increasing in $(1-u) \in [1/(1+\theta), \theta/(1+\theta)]$. By Theorem 3, it is sufficient to show that $K_{\beta_2}(u)$ is decreasing in $u \in [1/(1+\theta), \theta/(1+\theta)]$. Denote

$$w_{2}(u) = \frac{2\theta^{2}u}{[1 - 2\theta - (1 - \theta)u][1 - (1 + \theta)u]}, \quad \frac{1}{1 + \theta} \le u \le \frac{\theta}{1 + \theta}$$

Note that

$$w'_2(u) \stackrel{\text{sgn}}{=} (\theta^2 - 1)u^2 + 1 - 2\theta$$

and $w'_2(0) < 0$, $w'_2(\sqrt{(2\theta - 1)}/(\theta^2 - 1)) = 0$. It can be verified that $\theta \in [1, 3.2]$ implies

$$0 < \frac{1}{1+\theta} < \frac{\theta}{1+\theta} < \sqrt{\frac{2\theta-1}{\theta^2-1}},$$

which confirms $w'_2(u)$ is negative in $u \in [1/(1+\theta), \theta/(1+\theta)]$. And thus, $K_{\beta_2}(u)$ is decreasing in $u \in [1/(1+\theta), \theta/(1+\theta)]$.

When $\theta = 3.3, 8, 100$, Figure 2(a), (c) and (e) illustrates that the condition (1) of Theorem 3 cannot be satisfied, respectively, and corresponding Figure 2(b), (d) and (f) negates the result of Theorem 3, respectively. It seems that the condition (1) in Theorem 3 be a necessary condition. Unfortunately, we cannot give a mathematical validation.

Remark 2. An insightful reviewer pointed out, whether the conditions of Theorem 3 can be satisfied by the copula in Example 3 for all $\theta \in [1, \infty]$. Unfortunately, we give a negative answer as above.

The following example shows that the condition of Theorem 2 do not necessarily imply $\tau_{ARCL} \prec_c \tau_{ARSL}$ and $\tau_{ARCL} \ge_{lr} \tau_{ARSL}$. And thus, the following Theorem 4 gives some condition to strength from $\tau_{ARCL} \ge_{hr} \tau_{ARSL}$ to $\tau_{ARCL} \prec_c \tau_{ARSL}$ and $\tau_{ARCL} \ge_{lr} \tau_{ARSL}$.

Example 4. Consider a coherent system $T = \wedge \{X_1, \forall \{X_2, X_3\}\}$ with identical distributed components X_1, X_2, X_3 having Farlie–Gumbel–Morgenstern (FGM) copula C (11). Let $Y_{j1}, Y_{j2}, Y_{j3} (j = 1, 2)$ be lifetimes of d.i.d. spares having common copula (11). Furthermore, suppose C = C'. It is obvious that m = 2, for all $\theta \in [1, \infty]$, we have

$$\beta_3(u) = u^3(1 + \theta(1 - u)^3),$$

and the reliability function of this system can be expressed as

$$q(1-u) = 2(1-u)^2 - (1-u)^3 - \theta u^3 (1-u)^3,$$



Figure 2. For $\theta = 3.3$, 8, 100, (a)–(c) and (e) plots of the function $K_{\beta_2}(u)$, respectively, and (b)–(d) and (f) plots of the function $\Lambda'(u)$.

$$K_q(1-u) = \frac{(1-u)q'(1-u)}{q(1-u)} = \frac{6\theta u^4 - 9\theta u^3 + 3\theta u^2 + 3u + 1}{\theta u^4 - \theta u^3 + u + 1},$$
$$L_{\beta_3}(u) = \frac{(1-u)\beta_3'(u)}{1-\beta_3(u)} = \frac{3u^2(\theta(1-2u)(1-u)^2 + 1)}{-\theta u^5 + 2\theta u^4 - \theta u^3 + u^2 + u + 1}.$$

It is obvious that $K_q(1-u)$ is increasing in u, and $q(1-u) \le 1-u$, for all $u \in (0, 1)$ (see Example 3.14 of Zhang et al. [50]). According to Example 2, it is obvious that $L_{\beta_3}(u)$ is increasing in $u \in (0, 1)$. Thus, $\tau_{ARCL} \ge_{hr} \tau_{ARSL}$ holds. Figure 3 illustrates that the relative hazard rate ordering and the likelihood rate ordering do not hold.



Figure 3. For $\theta = -1$, plots of functions f_{ARCL}/f_{ARSL} , h_{ARCL}/h_{ARSL} and $\bar{F}_{ARCL}/\bar{F}_{ARSL}$.

For the case of complete matching redundancies, when original components independent of spares, suppose that

$$\left(\frac{(1-q(p))^m q'(p)}{1-(1-q(p))^{m+1}}\right) \left(\frac{q(1-(1-p)^{m+1})}{(1-p)^m q'(1-(1-p)^{m+1})}\right)$$

is increasing in $p \in (0, 1)$, Hazra and Misra [16] proved that

$$\tau_{\text{ARCL}} \prec_c \tau_{\text{ARSL}},\tag{15}$$

and under the conditions that pR'(p)/R(p) is decreasing and positive for all $p \in (0, 1)$, where $R(p) = L_q(p)$, they also prove that

$$\tau_{\text{ARCL}} \succ_b \tau_{\text{ARSL}}.$$
(16)

To make Eqs. (15) and (16) more reasonable in some practical scenarios. Next, we promote the corresponding result in Theorems 4 and 5 to the hypothesis of dependence between spares and original components, respectively.

Theorem 4. If

(1) $uK'_q(1-u)/K_q(1-u)$ is nonpositive and increasing in $u \in (0, 1)$, (2) $uL'_{\beta_{m+1}}(u)/L_{\beta_{m+1}}(u)$ is positive and decreasing in $u \in (0, 1)$ and (3) $1-q(1-u) \ge uq'(1-u)$, for all $u \in (0, 1)$,

then

$$\tau_{\text{ARCL}} \prec_c \tau_{\text{ARSL}}$$

and

$$\tau_{\text{ARCL}} \geq_{lr} \tau_{\text{ARSL}}.$$

It should be noted that Eq. (15) is just the special case of Theorem 4 if $\beta_{m+1}(u) = u^{m+1}$ and p = 1 - u. The next numerical example serves as a practical support for the condition required in Theorem 4.

Example 5. Consider a coherent system $T = \wedge \{X_1, X_2, X_3, X_4\}$ with identical distributed components X_1, X_2, X_3 and X_4 having Gumbel–Barnett copula copula C' (10). Let $Y_{j1}, Y_{j2}, Y_{j3}, Y_{j4}$ (j = 1, 2, 3) be lifetimes of d.i.d. spares having common survival function and copula (10). Specifically, we assume C = C'. It is obvious that m = 3, then, the reliability function of this system can be represented as

$$q(1-u) = (1-u)^4 e^{-\theta \log^4(1-u)}$$



Figure 4. (a) Plots of the function $uK'_q(1-u)/K_q(1-u)$, (b) plots of the function $uL'_{\beta_{m+1}}(u)/L_{\beta_{m+1}}(u)$, (c) plots of the function $\beta_4(u) - u\beta_4'(u)$ and (d) plots of the function 1 - q(u) - (1-u)q'(u).

Clearly,

$$\begin{split} \beta_4(u) &= u^4 e^{-\theta \log^4(u)}.\\ \beta_4(u) &= u^4 e^{-\theta \log^4(u)} \left[4\theta \log^3(u) - 3 \right],\\ 1 &= q(u) - (1-u)q'(u) = e^{-\theta \log^4(u)} \left[-4\theta (u-1)u^3 \log^3(u) + e^{\theta \log^4(u)} + (3u-4)u^3 \right], \end{split}$$

and

$$\begin{split} K_q(1-u) &= 4 - 4\theta \log^3(1-u), \quad L_{\beta_4}(u) = \frac{4(u-1)u^3[\theta \log^3(u)-1]}{e^{a\log^4(u)} - u^4}, \\ \frac{uK'_q(1-u)}{K_q(1-u)} &= -\frac{3\theta u \log^2(1-u)}{(u-1)[\theta \log^3(1-u)-1]}, \\ \frac{uL'_{\beta_4}(u)}{L_{\beta_4}(u)} &= \frac{4\theta^2(u-1)\log^6(u)e^{\theta \log^4(u)} + \theta \log^3(u)[(7-8u)e^{\theta \log^4(u)} + u^4]}{(u-1)[u^4 - e^{\theta \log^4(u)}][\theta \log^3(u)-1]} \\ &+ \frac{3\theta(u-1)\log^2(u)[u^4 - e^{\theta \log^4(u)}] + (4u-3)e^{\theta \log^4(u)} - u^4}{(u-1)[u^4 - e^{\theta \log^4(u)}][\theta \log^3(u)-1]}. \end{split}$$

Let $\theta = 0.1, 0.2, 0.5, 1, 2$, Figure 4(a) and (b) shows that all $uK'_q(u)/K_q(u)$ are nonpositive and decreasing in $u \in (0, 1)$, and all $uL'_{\beta_4}(u)/L_{\beta_4}(u)$ are positive and decreasing in $u \in (0, 1)$. Figure 4(c) and (d) shows that all $\beta_4(u) \le u\beta'_4(u)$ and $1 - q(u) \ge (1 - u)q'(u)$, for all $u \in (0, 1)$. Figure 5 shows that all f_{ARCL}/f_{ARSL} are increasing in $u \in (0, 1)$. And thus, $\tau_{ARCL} <_c \tau_{ARSL}$ and $\tau_{ARCL} \ge_{lr} \tau_{ARSL}$ hold.



Figure 5. Plots of the function $f_{ARCL}(u)/f_{ARSL}(u)$ *.*



Figure 6. For $\theta = 1.6$, (a) plot of the function f_{ARCL}/f_{ARSL} and (b) plot of the function h_{ARCL}/h_{ARSL} .

Under the setup of Example 3, taking $\theta = 1.6$. Figure 6(a) and (b) illustrates that neither $\tau_{ARCL} >_b \tau_{ARSL}$ nor $\tau_{ARCL} \ge_{lr} \tau_{ARSL}$ holds. The following Theorem 5 gives the likelihood ordering and aging faster ordering in terms of the reversed hazard rate between the component and system levels under the framework of complete matching redundancies.

Theorem 5. If

- (1) $(1-u)K'_{\beta_{m+1}}(u)/K_{\beta_{m+1}}(u)$ is nonpositive decreasing in $u \in (0, 1)$,
- (2) $(1-u)L'_q(1-u)/L_q(1-u)$ is nonnegative increasing in $u \in (0,1)$ and
- (3) $q(1-u) \le \min\{1-u, (1-u)q'(1-u)\}, \text{ for all } u \in (0,1),$

```
then
```

 $\tau_{\text{ARCL}} \succ_b \tau_{\text{ARSL}},$

and

 $\tau_{\text{ARCL}} \geq_{lr} \tau_{\text{ARSL}}.$

Remark 3. For the case of complete matching redundancies, when original components independent of spares, then $\beta_{m+1}(u) = u^{m+1}$. It should be noted that Eq. (16) is just the special case of Theorem 5 if $\beta_{m+1}(u) = u^{m+1}$ and p = 1 - u.

3.3. Nonmatching case

For the coherent system with d.i.d. components and spares, suppose that spares and original components are independent, in the nonmatching case, under conditions ((1 - p)q'(p))/(1 - q(p)) is increasing in $p \in (0, 1)$, Zhang *et al.* [50] proved that

$$\tau_{\text{ARCL}} \ge_{\text{rh}} \tau_{\text{ARSL}}.$$
(17)

The following theorem generalizes Eq. (17) to the coherent systems with dependence of spares and original components in the case of the reversed hazard rate ordering. It incorporates or generalizes many known results in the literature. For more details, refer to Theorem 3.2 of Gupta and Nanda [15], Theorem 3.1 of Misra *et al.* [30], Theorem 3 of Gupta and Kumar [14] and Theorem 3.4 of Zhang *et al.* [50]. For convenience, denote

$$\alpha_j^C(v_1, v_2, \dots, v_{m+1}) = \frac{v_j \partial C(v_1, v_2, \dots, v_{m+1}) / \partial v_j}{C(v_1, v_2, \dots, v_{m+1})}, \quad j = 1, 2, \dots, m+1$$

Theorem 6. If

(1) $\alpha_j^C(v_1, v_2, \dots, v_{m+1})$ is decreasing in $v_j \in (0, 1)$, for all $j = 1, 2, \dots, m+1$, (2) $L_q(1-u)$ is decreasing in $u \in (0, 1)$ and (3) $q(1-u) \le 1-u$ for all $u \in (0, 1)$,

then

 $\tau_{\text{ARCL}} \geq_{rh} \tau_{\text{ARSL}}$.

One natural question arises that whether the hazard rate ordering, aging faster ordering in terms of the reversed hazard rate and the hazard rate hold between τ_{ARCL} and τ_{ARSL} for the nonmatching case. Unfortunately, Counterexample 1 gives a negative answer even for the independent case.

Counterexample 3.1. For a coherent systems $T = \wedge \{X_1, X_2\}$ with i.i.d. components X_1 and X_2 having exponential lifetimes with parameters $\lambda = 2$. Let Y_1 and Y_2 be lifetimes of two i.i.d. spares having exponential lifetimes with parameters $\lambda = 1$. We have

$$F_{\text{ARCL}}(1 - e^{-x}, 1 - e^{-2x}) = 1 - (1 - (1 - e^{-2x})(1 - e^{-x}))^2$$

and

$$F_{\text{ARSL}}(1 - e^{-x}, 1 - e^{-2x}) = (1 - e^{-4x})(1 - e^{-2x}).$$

And it holds that

$$\begin{split} \tilde{h}_{\text{ARCL}}(1-e^{-x},1-e^{-2x}) &= \frac{2(e^x+3)(e^x+e^{2x}-1)}{1-e^x-2e^{2x}+e^{4x}+e^{5x}},\\ h_{\text{ARCL}}(1-e^{-x},1-e^{-2x}) &= \frac{2(e^{-x}(1-e^{-2x})+2e^{-2x}(1-e^{-x}))}{1-(1-e^{-2x})(1-e^{-x})},\\ \tilde{h}_{\text{ARSL}}(1-e^{-x},1-e^{-2x}) &= \frac{2(e^{2x}+3)}{e^{4x}-1},\\ h_{\text{ARSL}}(1-e^{-x},1-e^{-2x}) &= \frac{2e^{-2x}(1-e^{-4x})+4e^{-4x}(1-e^{-2x})}{1-(1-e^{-4x})(1-e^{-2x})}. \end{split}$$

From Figure 7(a), (b) and (c), it obviously can be seen that $\tilde{h}_{ARCL}/\tilde{h}_{ARSL}$, $\bar{F}_{ARCL}/\bar{F}_{ARSL}$ and h_{ARCL}/h_{ARSL} are all not monotone on $(0, \infty)$, which mean $\tau_{ARCL} >_b \tau_{ARSL}$, $\tau_{ARCL} >_c \tau_{ARSL}$ and $\tau_{ARCL} \ge_{hr} \tau_{ARSL}$ are all invalid.



Figure 7. (a) Plot of the function $\tilde{h}_{ARCL}/\tilde{h}_{ARSL}$, (b) plot of the function $\bar{F}_{ARCL}/\bar{F}_{ARSL}$ and (c) plot of the function h_{ARCL}/h_{ARSL} .

4. Application

From a practical point of view, modern systems, such as the new energy vehicles industry, respond to the requirements of safe and stable operation; it is hoped that the probability of the running interruption of the core components can be reduced. A possible component level versus system level at active redundancies for coherent systems with dependent components application scenarios are provided below for practical use and reference for future research.

As the power source and energy carrier of new energy vehicles, power battery is a key component. However, the backwardness of power battery-related technologies seriously restricts the development of electric vehicles, which are mainly manifested in poor endurance, short service life and unstable safety. In pure electric vehicles and grid energy storage applications, single batteries are connected in series to meet voltage requirements and in parallel to meet capacity requirements. Series and parallel connections often exist simultaneously. Among them, the battery used in the Beijing Olympic Games and the Shanghai World Expo for pure electric buses adopts a parallel-series connection, and the grid battery energy storage often adopts a series-parallel connection. Therefore, the battery formation mode is an extremely active research field in the lithium-ion battery management system, and the quality of its evaluation method largely determines the overall performance of the battery management system. As shown in Figure 8(a) and (b), we will explore the performance of the series-parallel battery group and the parallel-series battery group. To solve the above problems, we give the following assumptions:

(1) Suppose we have 12 batteries *B*₁₁, *B*₁₂, *B*₁₃, *B*₁₄, *B*₂₁, *B*₂₂, *B*₂₃, *B*₂₄, *B*₃₁, *B*₃₂, *B*₃₃, *B*₃₄, which are made in the same batch and the same manufacturer.



Figure 8. (a) Series-parallel battery group and (b) parallel-series battery group.

- (2) It is assumed that the failure data of a single battery has been obtained through the durability test, and the lifetime distribution of battery can be estimated from the failure data, let us assume a Weibull distribution;
- (3) Considering the influence of the environment and stress level of the battery group, it is assumed that the batteries that make up the battery group are interdependent, and the dependency is described by copula.
- (4) According to Section 3.1, suppose that

$$C'(v_1, v_2, v_3, v_4) = \left(\prod_{1=1}^4 v_i\right) e^{-\theta_1 \prod_{1=1}^4 \log v_i}, \quad v_i \in [0, 1]$$

$$C(v_1, v_2, v_3) = \prod_{i=1}^3 v_i + \theta_2 \prod_{i=1}^3 v_i (1 - v_i), \quad v_i \in [0, 1].$$

Next, we will use the work of this article to explore how to optimize the battery group method from a theoretical point of view to improve the life of the power battery group. From Example 2, we find the performance of the parallel-series battery group is better than the series-parallel battery group. Therefore, to improve the reliability of the battery group, the battery formation mode is the parallel-series group. The research results provide some theoretical support for engineers to design more complex power battery groups. However the series-parallel battery group is conducive to the detection and management of the individual cells of the system.

5. Conclusion

This paper investigates the case that the vector of the spare lifetimes and the vector of the original component lifetimes are dependent. In this framework, we consider the issue of stochastic comparison of multi-active complete matching and nonmatching spares redundancies at the component level versus the system level, respectively. In cases of the nonmatching and matching spares, we got the sufficient conditions that are presented to compare component and system redundancies by means of the hazard rate ordering and the reversed hazard rate ordering, and we also obtain the result for relative aging ordering. Our work extend the works of Zhang *et al.* [50] and Hazra and Misra [16] and complements existing literature. However, for the general case, that is, consider the assumption of all components are d.n.i.d., which is an important question in future study, and Yan *et al.* [46] stochastically compares allocations of standby redundancies in series systems with exponential components at the component level versus the system level in sense of the likelihood ratio ordering, that is,

$$\wedge (X_1 + Y_1, X_2 + Y_2) \ge_{\mathrm{lr}} [\wedge (X_1, X_2)] + [\wedge (Y_1, Y_2)].$$
(18)

Based on Eq. (18), it is also of great interest to consider the corresponding conclusion when replacing active redundancy in this article as standby redundancy, where Eqs. (4) and (5) are replaced as

$$\tau_{\text{ARCL}} = \tau (X_1 + Y_{11} + \dots + Y_{m1}, X_2 + Y_{12} + \dots + Y_{m2}, \dots, X_n + Y_{1n} + \dots + Y_{mn}),$$

$$\tau_{\text{ARSL}} = \tau (X_1, X_2, \dots, X_n) + \tau (Y_{11}, Y_{12}, \dots, Y_{1n}) + \dots + \tau (Y_{m1}, Y_{m2}, \dots, Y_{mn}),$$

respectively, which remains as an open problem. On the other hand, in design and analysis of the redundancy allocation issue, engineer must have some components or subsystems in the inventory to replace the failed part. The number of components in inventory may be limited by factors such as budget or storage space. Therefore, the redundancy allocation problem is to find a way to maximize reliability while reducing costs. For example, Hsieh [18] discusses the combination of cold standby strategy and component mixing and proposes hybrid strategy to optimize reliability redundancy allocation problem. Thus, in the follow-up, we have to consider not only the optimization of the allocation should be considered but also the minimization of the cost.

Acknowledgments. This work is supported by the National Natural Science Foundation of China (11861058). The authors are indebted to editor and anonymous referees, for insightful comments and help suggestions, which have greatly improved the presentation of this manuscript and for bringing our attention to recent publications in the relevant literature.

Competing interest. The authors declare no conflict of interest.

References

- [1] Barlow, R.E. & Proschan, F. (1975). Statistical theory of reliability and life testing. New York: Holt, Rinehart and Winston.
- [2] Belzunce, F., Manuel, F., Ruiz, J.M., & Carmen Ruiz, M. (2001). On partial orderings between coherent systems with different structures. *Probability in the Engineering and Informational Sciences* 15: 273–293.
- [3] Belzunce, F., Martínez-Puertas, H., & Ruiz, J.M. (2011). On optimal allocation of redundant components for series and parallel systems of two dependent components. *Journal of Statistical Planning and Inference* 141: 3094–3104.
- [4] Belzunce, F., Martínez-Puertas, H., & Ruiz, J.M. (2013). On allocation of redundant components for systems with dependent components. *European Journal of Operational Research* 230: 573–580.
- [5] Boland, P.J. & El-Neweihi, E. (1995). Component redundancy vs system redundancy in the hazard rate ordering. *IEEE Transactions on Reliability* 44: 614–619.
- [6] Boland, P.J., El-Neweihi, E., & Proschan, F. (1992). Stochastic order for redundancy allocations in series and parallel systems. Advances in Applied Probability 24(1): 161–171.
- [7] Brito, G., Zequeira, R.I., & Valdés, J.E. (2011). On the hazard rate and reversed hazard rate orderings in two-component series systems with active redundancies. *Statistics and Probability Letters* 81: 201–206.
- [8] Chen, J., Zhang, Y., Zhao, P., & Zhou, S. (2017). Allocation strategies of standby redundancies in series/parallel system. Communication in Statistics – Theory and Methods 47: 708–724.
- [9] Da, G. & Ding, W. (2016). Component level versus system level k-out-of- n assembly systems. *IEEE Transactions on Reliability* 65: 425–433.
- [10] Ding, W. & Zhang, Y. (2018). Relative ageing of series and parallel systems: effects of dependence and heterogeneity among components. *Operations Research Letters* 46: 219–224.
- [11] Ding, W., Fang, R., & Zhao, P. (2017). Relative aging of coherent systems. Naval Research Logistics 64: 345–354.
- [12] Fang, R. & Li, X. (2017). On matched active redundancy allocation for coherent systems with statistically dependent component lifetimes. *Naval Research Logistics* 64: 580–598.
- [13] Fang, R. & Li, X. (2020). Active redundancy allocation for coherent systems with independent and heterogeneous components. *Probability in the Engineering and Informational Sciences* 34: 72–91.
- [14] Gupta, N. & Kumar, S. (2014). Stochastic comparisons of component and system redundancies with dependent components. *Operations Research Letters* 42: 284–289.
- [15] Gupta, R.D. & Nanda, A.K. (2001). Some results on reversed hazard rate ordering. Communications in Statistics Theory and Methods 30: 2447–2457.
- [16] Hazra, N.K. & Misra, N. (2020). On relative ageing of coherent systems with dependent identically distributed components. Advances in Applied Probability 52: 348–376.
- [17] Hazra, N.K. & Nanda, A.K. (2014). Component redundancy versus system redundancy in different stochastic orderings. *IEEE Transactions on Reliability* 63: 567–582.
- [18] Hsieh, T.J. (2021). Component mixing with a cold standby strategy for the redundancy allocation problem. *Reliability Engineering and System Safety* 206: 10729.
- [19] Jeddi, H. & Doostparast, M. (2016). Optimal redundancy allocation problems in engineering systems with dependent component lifetimes. *Applied Stochastic Models in Business and Industry* 32: 199–208.

- [20] Kalashnikov, V.V. & Rachev, S.T. (1986). A characterization of queueing models and its stability. *Journal of Mathematical Sciences* 35: 2336–2360.
- [21] Kim, K.O. (2020). Reliability comparison of two unit redundancy systems under the load requirement. Probability in the Engineering and Informational Sciences, 35(3): 1–15.
- [22] Kotz, S., Lai, C.D., & Xie, M. (2003). On the effect of redundancy for systems with dependent components. *IIE Transactions* 35: 1103–1110.
- [23] Kuiti, M.R., Hazra, N.K., & Finkelstein, M. (2017). On component redundancy versus system redundancy for a k-out-of-n system, arXiv:1710.09202.
- [24] Kuiti, M.R., Hazra, N.K., & Finkelstein, M. (2020). A note on the stochastic precedence order between component redundancy and system redundancy for k-out-of-n systems. *Communication in Statistics Theory and Methods*, 1–9. doi: 10.1080/03610926.2020.1831539.
- [25] Li, X. & Ding, W. (2010). Optimal allocation of active redundancies to k-out-of-n systems with heterogeneous components. Journal of Applied Probability.47.(1): 254–263.
- [26] Li, C. & Li, X. (2016). Relative ageing of series and parallel systems with statistically independent and heterogeneous component lifetimes. *IEEE Transactions on Reliability* 65: 1014–1021.
- [27] Li, X., Yan, R., & Hu, X. (2011). On the allocation of redundancies in series and parallel systems. *Communication in Statistics Theory and Methods* 40: 959–968.
- [28] Ling, X., Wei, Y., & Li, P. (2019). On optimal heterogeneous components grouping in series-parallel and parallel-series systems. Probability in the Engineering and Informational Sciences 33: 564–578.
- [29] Misra, N. & Francis, J. (2015). Relative ageing of (n k + 1)-out-of-*n* systems. *Statistics and Probability Letters* 106: 272–280.
- [30] Misra, N., Dhariyal, I.D., & Nitin, G. (2009). Optimal allocation of active spares in series systems and comparison of component and system redundancies. *Journal of Applied Probability* 46: 19–34.
- [31] Nanda, K.A. & Kamal, H.N. (2013). Some results on active redundancy at component level versus system level. Operations Research Letters 41: 241–245.
- [32] Navarro, J. & Durante, F. (2017). Copula-based representations for the reliability of the residual lifetimes of coherent systems with dependent components. *Journal of Multivariate Analysis* 158: 87–102.
- [33] Navarro, J., Aguila, Y.D., Sordo, M.A., & Suárez, A. (2013). Stochastic ordering properties for systems with dependent identically distributed components. *Applied Stochastic Models in Business and Industry* 29: 264–278.
- [34] Navarro, J., Aguila, Y.D., Sordo, M.A., & Suárez-Llorens, A. (2015). Orderings of coherent systems with randomized dependent components. *European Journal of Operational Research* 240: 127–139.
- [35] Navarro, J., Aguila, Y.D., Sordo, M.A., & Suárez-Llorens, A. (2016). Preservation of stochastic orders under the formation of generalized distorted distributions. Applications to coherent systems. *Methodology and Computing in Applied Probability* 18: 529–545.
- [36] Navarro, J., Fernández-Martínez, P., Fernández-Sánchez, J., & Arriaza, A. (2020). Relationships between importance measures and redundancy in systems with dependent components. *Probability in the Engineering and Informational Sciences* 34: 583–604.
- [37] Nelsen, R.B. (2006). An introduction to copulas. New York: Springer.
- [38] Rezaei, M., Gholizadeh, B., & Izadkhah, S. (2014). On relative reversed hazard rate order. Communications in Statistics Theory and Methods 44: 300–308.
- [39] Sengupta, D. & Deshpande, J.V. (1994). Some results on the relative ageing of two life distributions. *Journal of Applied Probability* 31: 991–1003.
- [40] Shaked, M. & Shantikumar, J.G. (2007). Stochastic orders. New York: Springer.
- [41] Singh, H. & Singh, R.S. (1997). On allocation of spares at component level versus system level. Journal of Applied Probability 34: 283–287.
- [42] Torrado, N., Arriaza, A., & Navarro, J. (2021). A study on multi-level redundancy allocation in coherent systems formed by modules. *Reliability Engineering and System Safety* 213: 107694.
- [43] Yan, R. & Luo, T. (2018). On the optimal allocation of active redundancies in series system. *Communications in Statistics Theory and Methods* 47: 2379–2388.
- [44] Yan, R. & Wang, J. (2020). Component level versus system level at active redundancies for coherent systems with dependent heterogeneous components. *Communications in Statistics – Theory and Methods* 47: 1–21.
- [45] Yan, R., Lu, B., & Li, X. (2019). On redundancy allocation to series and parallel systems of two components. *Communications in Statistics Theory and Methods* 48: 4690–4701.
- [46] Yan, X., Zhang, Y., & Zhao, P. (2021). Standby redundancies at component level versus system level in series system. *Communications in Statistics – Theory and Methods* 50: 473–485.
- [47] You, Y. & Li, X. (2018). Ordering k-out-of-n systems with interdependent components and one active redundancy. Communication in Statistics – Theory and Methods 47: 1–13.
- [48] You, Y., Fang, R., & Li, X. (2016). Allocating active redundancies to k-out-of-n reliability systems with permutation monotone component lifetimes. *Applied Stochastic Models in Business and Industry* 32: 607–620.
- [49] Zhang, Y. (2018). Optimal allocation of active redundancies in weighted k-out-of-n systems. Statistics and Probability Letters 135: 110–117.

- [50] Zhang, Y., Amini-Seresht, E., & Ding, W. (2017). Component and system active redundancies for coherent systems with dependent components. *Applied Stochastic Models in Business and Industry* 33: 409–421.
- [51] Zhang, X., Zhang, Y., & Fang, R. (2020). Allocations of cold standbys to series and parallel systems with dependent components. *Applied Stochastic Models in Business and Industry* 36: 432–451.
- [52] Zhao, P., Chan, P.S., & Ng, H.K.T. (2012). Optimal allocation of redundancies in series systems. European Journal of Operational Research 220: 673–683.
- [53] Zhao, P., Zhang, Y., & Li, L. (2015). Redundancy allocation at component level versus system level. European Journal of Operational Research 241: 402–411.
- [54] Zhuang, J. & Li, X. (2015). Allocating redundancies to k-out-of-n systems with independent and heterogeneous components. Communications in Statistics – Theory and Methods 44: 5109–5119.

Appendix. Proof of all main results

Proof of Theorem 1

It is obvious that $\bar{F}_{ARCL}(u) - \bar{F}_{ARSL}(u) \ge 0$, which is equivalent to

$$q(1 - \beta_{m+1}(u)) + \beta_{m+1}(1 - q(1 - u)) \ge 1.$$

The proof is completed.

Proof of Theorem 2

According to Definition 1 (ii), the desired result is equivalent to

$$\Lambda(u) = \frac{\bar{F}_{\text{ARCL}}(u)}{\bar{F}_{\text{ARSL}}(u)} = \frac{q(1 - \beta_{m+1}(u))}{1 - \beta_{m+1}(1 - q(1 - u))}$$

is increasing in $u \in (0, 1)$. Observe that

$$\begin{split} \frac{\partial \Lambda(u)}{\partial u} & \stackrel{\text{sgn}}{=} \frac{q'(1-u)\beta'_{m+1}(1-q(1-u))}{1-\beta_{m+1}(1-q(1-u))} - \frac{\beta'_{m+1}(u)q'(1-\beta_{m+1}(u))}{q(1-\beta_{m+1}(u))} \\ & \stackrel{\text{sgn}}{=} \frac{q(1-u)\beta'_{m+1}(1-q(1-u))}{1-\beta_{m+1}(1-q(1-u))} \cdot \frac{(1-u)q'(1-u)}{q(1-u)} - \frac{(1-u)\beta'_{m+1}(u)}{1-\beta_{m+1}(u)} \\ & \cdot \frac{(1-\beta_{m+1}(u))q'(1-\beta_{m+1}(u))}{q(1-\beta_{m+1}(u))} \\ & \geq \frac{(1-u)\beta'_{m+1}(u)}{1-\beta_{m+1}(u)} \left[\frac{(1-u)q'(1-u)}{q(1-u)} - \frac{(1-\beta_{m+1}(u))q'(1-\beta_{m+1}(u))}{q(1-\beta_{m+1}(u))} \right] \\ & = L_{\beta_{m+1}}(u)[K_q(1-u) - K_q(1-\beta_{m+1}(u))] \\ & \geq 0. \end{split}$$

note that $\beta_{m+1}(x)$ and q(x) are increasing in $x \in [0, 1]$, and thus, $L_{\beta_{m+1}}(x)$ and $K_q(x)$ are nonnegative for all $x \in [0, 1]$, then, the first inequality is derived from conditions (1) and (2), and the second inequality comes from conditions (1), (2) and (3), which completes the proof.

Proof the nonnegative and increasing property of $L_{\beta_3}(u)$ in (12)

Obvious that

$$L_{\beta_3}(u) = \frac{(1-u)\beta'_3(u)}{1-\beta_3(u)}$$

$$\stackrel{\text{sgn}}{=} 3u^2(\theta_2(1-2u)(1-u)^2+1)$$

$$\stackrel{\text{sgn}}{=} 1+\theta_2(1-2u)(1-u)^2 =: \mu(u;\theta_2).$$



Figure A.1. Plots of the function $\eta(u; -1)$ *and* $\eta(u; 1)$ *.*

In the following, we prove the nonnegative of $\mu(u; \theta)$. *Case 1:* $u \in [0, \frac{1}{2}], \theta_2 \in [-1, 1]$. It is easy to see that

$$0 \le (1 - 2u)(1 - u)^2 \le 1,$$

for any $\theta_2 \in [-1, 1]$, we then have

$$\mu(u;\theta_2) \ge \mu(u;-1) = 1 - (1 - 2u)(1 - u)^2 \ge 0$$

Case 2: for $u \in (\frac{1}{2}, 1], \theta_2 \in [-1, 1]$. Note that

$$-1 < (1 - 2u)(1 - u)^2 \le 0,$$

for any $\theta_2 \in [-1, 1]$, we have

$$\mu(u;\theta_2) \ge \mu(u;1) = 1 + (1-2u)(1-u)^2 \ge 0.$$

It suffices to prove $L_{\beta_3}(u)$ is increasing in $u \in [0, 1]$. After some simplifications, we have

$$\eta(u;\theta_2) := L'_{\beta_3}(u) \stackrel{\text{sgn}}{=} a(u)\theta_2^2 + b(u)\theta_2 + c(u),$$

where

$$a(u) = u^{3}(1-u)^{4} \ge 0,$$

$$b(u) = (-3u^{5} - 2u^{4} + 2u^{3} + 12u^{2} - 11u + 2),$$

$$c(u) = u + 2 \ge 0.$$

Obvious that, taking u = 0 and u = 1, then $\eta(u; \theta_2) = 2\theta_2 + 2$ and $\eta(u; \theta_2) = 2$, respectively, and thus $\eta(u; \theta_2) \ge 0$. For any $u \in (0, 1, 1)$ from the properties of quadratic function, if $-b(u)/(2a(u)) \ge 0$, then

$$\eta(u; 1) \ge 0 \Longrightarrow \eta(u; \theta_2) \ge 0$$

Similarly, if $-b(u)/(2a(u)) \le 0$, then

$$\eta(u; -1) \ge 0 \Longrightarrow \eta(u; \theta_2) \ge 0$$

Figure A.1 shows that $\eta(u; 1) \ge 0$ and $\eta(u; -1) \ge 0$.

To sum up, for any $u \in [0, 1]$ and $\theta_2 \in [-1, 1]$, we have showed that $L_{\beta_3}(u)$ is nonnegative and increasing in u.

Proof of Theorem 4

We have two cases to prove this theorem.

Case 1: $\tau_{ARCL} \prec_c \tau_{ARSL}$. Denote $h_{ARCL}(u)$ and $h_{ARSL}(u)$ the hazard rate of τ_{ARCL} and τ_{ARSL} , respectively, then

$$h_{\text{ARCL}}(u) = \frac{\beta'_{m+1}(u)q'(1-\beta_{m+1}(u))}{q(1-\beta_{m+1}(u))},$$

$$h_{\text{ARSL}}(u) = \frac{q'(1-u)\beta'_{m+1}(1-q(1-u))}{1-\beta_{m+1}(1-q(1-u))}.$$

According to Definition 2 (i), the desired result is equivalent to $h_{ARCL}(u)/h_{ARSL}(u)$ is increasing in u_i , i = 1, 2, ..., m + 1. Obverse that,

$$\begin{split} \frac{h_{\text{ARCL}}(u)}{h_{\text{ARSL}}(u)} &= \frac{\beta'_{m+1}(u)q'(1-\beta_{m+1}(u))}{q(1-\beta_{m+1}(u))} \cdot \frac{1-\beta_{m+1}(1-q(1-u))}{q'(1-u)\beta'_{m+1}(1-q(1-u))} \\ &= \frac{(1-u)\beta'_{m+1}(u)}{1-\beta_{m+1}(u)} \cdot \frac{(1-\beta_{m+1}(u))q'(1-\beta_{m+1}(u))}{q(1-\beta_{m+1}(u))} \cdot \frac{q(1-u)}{(1-u)q'(1-u)} \\ &\times \frac{1-\beta_{m+1}(1-q(1-u))}{q(1-u)\beta'_{m+1}(1-q(1-u))} \\ &= \frac{L_{\beta_{m+1}}(u)}{L_{\beta_{m+1}}(1-q(1-u))} \cdot \frac{K_q(1-\beta_{m+1}(u))}{K_q(1-u)}. \end{split}$$

Note that $\beta_{m+1}(u)$ is increasing in $u \in [0, 1]$, which implies $L_{\beta_{m+1}}(u)$ is nonnegative for all $u \in [0, 1]$, and q(1 - u) are increasing in $(1 - u) \in [0, 1]$, which implies $K_q(1 - u)$ is nonnegative for all $(1 - u) \in [0, 1]$, we then have

$$\left[\frac{L_{\beta_{m+1}}(u)}{L_{\beta_{m+1}}(1-q(1-u))}\right]' \ge 0 \text{ and } \left[\frac{K_q(1-\beta_{m+1}(u))}{K_q(1-u)}\right]' \ge 0 \text{ imply } \left[\frac{h_{\text{ARCL}}(u)}{h_{\text{ARSL}}(u)}\right]' \ge 0,$$

and

$$\left[\frac{L_{\beta_{m+1}}(u)}{L_{\beta_{m+1}}(1-q(1-u))}\right]' \stackrel{\text{sgn}}{=} \frac{L'_{\beta_{m+1}}(u)}{L_{\beta_{m+1}}(u)} - \frac{q'(1-u)L'_{\beta_{m+1}}(1-q(1-u))}{L_{\beta_{m+1}}(1-q(1-u))}$$

From the assumption that $uL'_{\beta_{m+1}}(u)/L_{\beta_{m+1}}(u)$ is positive and decreasing in $u \in (0, 1)$ and $1 - q(1 - u) \ge uq'(1 - u)$, and $q(1 - u) \le 1 - u$, for all $u \in (0, 1)$, it follows that

$$\frac{uL'_{\beta_{m+1}}(u)}{L_{\beta_{m+1}}(u)} \ge \frac{(1-q(1-u))L'_{\beta_{m+1}}(1-q(1-u))}{L_{\beta_{m+1}}(1-q(1-u))} \ge \frac{uh'(1-u)L'_{\beta_{m+1}}(1-q(1-u))}{L_{\beta_{m+1}}(1-q(1-u))}.$$
 (A.1)

Similarity,

$$\left[\frac{K_q(1-\beta_{m+1}(u))}{K_q(1-u)}\right]' \stackrel{\text{sgn}}{=} \frac{K'_q(1-u)}{K_q(1-u)} - \frac{\beta'_{m+1}(u)K'_q(1-\beta_{m+1}(u))}{K_q(1-\beta_{m+1}(u))}$$

From the assumption that $uK'_q(1-u)/K_q(1-u)$ is nonpositive and increasing in $u \in (0, 1)$ and based on Lemma 1, it is obvious that $\beta_{m+1}(u) \le \min\{u, u\beta'_{m+1}(u)\}$, for all $u \in (0, 1)$, we have

$$\frac{uK'_q(1-u)}{K_q(1-u)} \ge \frac{\beta_{m+1}(u)K'_q(1-\beta_{m+1}(u))}{K_q(1-\beta_{m+1}(u))} \ge \frac{u\beta'_{m+1}(u)K'_q(1-\beta_{m+1}(u))}{K_q(1-\beta_{m+1}(u))}.$$
(A.2)

From (A.1) and (A.2), we get

$$\left[\frac{L_{\beta_{m+1}}(u)}{L_{\beta_{m+1}}(1-q(1-u))}\right]' \ge 0, \quad \left[\frac{K_q(1-\beta_{m+1}(u))}{K_q(1-u)}\right]' \ge 0$$

And thus $\tau_{\text{ARCL}} \prec_c \tau_{\text{ARSL}}$.

Case 2: $\tau_{ARCL} \ge_{lr} \tau_{ARSL}$. Based on Theorem 2, we have $uK'_q(1-u)/K_q(1-u)$ is nonpositive and increasing in $u \in (0, 1)$ implies $K_q(1-u)$ is decreasing in $(1-u) \in (0, 1)$, and $uL'_{\beta_{m+1}}(u)/L_{\beta_{m+1}}(u)$ is positive and decreasing in $u \in (0, 1)$ implies $L_{\beta_{m+1}}(u)$ is increasing in $u \in (0, 1)$. According to Theorem 1.C.4 in Shaked and Shantikumar [40], it is well know that $X \ge_{lr} Y$. Therefore, if conditions (1), (2) and (3) hold, we also have $\tau_{ARCL} \ge_{lr} \tau_{ARSL}$. That completes the proof.

Proof of Theorem 5

We have two cases to prove this theorem.

Case 1: $\tau_{ARCL} >_b \tau_{ARSL}$. Denote $\tilde{h}_{ARCL}(u)$ and $\tilde{h}_{ARSL}(u)$ the reversed hazard rate of τ_{ARCL} and τ_{ARSL} , respectively, then

$$\begin{split} \tilde{h}_{\text{ARCL}}(u) &= \frac{\beta'_{m+1}(u)q'(1-\beta_{m+1}(u))}{1-q(1-\beta_{m+1}(u))},\\ \tilde{h}_{\text{ARSL}}(u) &= \frac{q'(1-u)\beta'_{m+1}(1-q(1-u))}{\beta_{m+1}(1-q(1-u))}. \end{split}$$

According to Definition 2(ii), the desired result is equivalent to $\tilde{h}_{ARCL}(u)/\tilde{h}_{ARSL}(u)$ is increasing in u, we have

$$\frac{\tilde{h}_{\text{ARCL}}(u)}{\tilde{h}_{\text{ARSL}}(u)} = \frac{\beta'_{m+1}(u)q'(1-\beta_{m+1}(u))}{1-q(1-\beta_{m+1}(u))} \cdot \frac{\beta_{m+1}(1-q(1-u))}{q'(1-u)\beta'_{m+1}(1-q(1-u))} \\
= \frac{u\beta'_{m+1}(u)}{\beta_{m+1}(u)} \cdot \frac{\beta_{m+1}(u)q'(1-\beta_{m+1}(u))}{1-q(1-\beta_{m+1}(u))} \\
\cdot \frac{1-q(1-u)}{uh'(1-u)} \cdot \frac{\beta_{m+1}(1-q(1-u))}{(1-q(1-u))\beta'_{m+1}(1-q(1-u))} \\
= \frac{K_{\beta_{m+1}}(u)}{K_{\beta_{m+1}}(1-q(1-u))} \cdot \frac{L_q(1-\beta_{m+1}(u))}{L_q(1-u)}.$$

Note that $\beta_{m+1}(u)$ is increasing in $u \in [0, 1]$, which implies $K_{\beta_{m+1}}(u)$ is nonnegative for all $u \in [0, 1]$, and q(1 - u) are increasing in $(1 - u) \in [0, 1]$, which implies $L_q(1 - u)$ is nonnegative for all $(1 - u) \in [0, 1]$, we then have

$$\left[\frac{K_{\beta_{m+1}}(u)}{K_{\beta_{m+1}}(1-q(1-u))}\right]' \ge 0 \text{ and } \left[\frac{L_q(1-\beta_{m+1}(u))}{L_q(1-u)}\right]' \ge 0 \text{ imply } \left[\frac{\tilde{h}_{\text{ARCL}}(u)}{\tilde{h}_{\text{ARSL}}(u)}\right]' \ge 0$$

and

$$\left[\frac{K_{\beta_{m+1}}(u)}{K_{\beta_{m+1}}(1-q(1-u))}\right]' \stackrel{\text{sgn}}{=} \frac{K'_{\beta_{m+1}}(u)}{K_{\beta_{m+1}}(u)} - \frac{q'(1-u)K'_{\beta_{m+1}}(1-q(1-u))}{K_{\beta_{m+1}}(1-q(1-u))}$$

From the assumption that $(1-u)K'_{\beta_{m+1}}(u)/K_{\beta_{m+1}}(u)$ is nonpositive and decreasing in $u \in (0, 1)$ and $q(1-u) \leq \min\{1-u, (1-u)q'(1-u)\}$, for all $u \in (0, 1)$, we have

$$\frac{(1-u)K'_{\beta_{m+1}}(u)}{K_{\beta_{m+1}}(u)} \ge \frac{q(1-u)K'_{\beta_{m+1}}(1-q(1-u))}{K_{\beta_{m+1}}(1-q(1-u))} \ge \frac{(1-u)q'(1-u)K'_{\beta_{m+1}}(1-q(1-u))}{K_{\beta_{m+1}}(1-q(1-u))}.$$
 (A.3)

Similarity,

$$\left[\frac{L_q(1-\beta_{m+1}(u))}{L_q(1-u)}\right]' \stackrel{\text{sgn}}{=} \frac{L'_q(1-u)}{L_q(1-u)} - \frac{\beta'_{m+1}(u)L'_q(1-\beta_{m+1}(u))}{L_q(1-\beta_{m+1}(u))}$$

From the assumption that $(1-u)L'_q(1-u)/L_q(1-u)$ is positive and increasing in $u \in (0, 1)$ and according to Lemma 1, we have $1-\beta_{m+1}(u) \ge (1-u)\beta'_{m+1}(u)$, and $\beta_{m+1}(u) \le u$, hold, for all $u \in (0, 1)$, thus

$$\frac{(1-u)L'_q(1-u)}{L_q(1-u)} \ge \frac{(1-\beta_{m+1}(u))L'_q(1-\beta_{m+1}(u))}{L_q(1-\beta_{m+1}(u))} \ge \frac{(1-u)\beta'_{m+1}(u)L'_q(1-\beta_{m+1}(u))}{L_q(1-\beta_{m+1}(u))}.$$
 (A.4)

From (A.3) and (A.4), we get

$$\left[\frac{K_{\beta_{m+1}}(u)}{K_{\beta_{m+1}}(1-q(1-u))}\right]' \ge 0, \quad \left[\frac{L_q(1-\beta_{m+1}(u))}{L_q(1-u)}\right]' \ge 0.$$

And thus $\tau_{\text{ARCL}} \succ_b \tau_{\text{ARSL}}$.

Case 2: $\tau_{ARCL} \geq_{lr} \tau_{ARSL}$. According to Theorem 3, we have $(1 - t)K'_{\beta_{m+1}}(u)/K_{\beta_{m+1}}(u)$ is nonpositive decreasing in $u \in (0, 1)$ implies $K_{\beta_{m+1}}(u)$ is decreasing in $u \in (0, 1)$, and $xL'_q(x)/L_q(x)$ is nonnegative decreasing in $x \in (0, 1)$ implies $L_q(x)$ is increasing in $x \in (0, 1)$, where x = 1 - u. According to Theorem 1.C.4 in Shaked and Shantikumar [40], it is well know that $X \geq_{lr} Y$. Therefore, if conditions (1), (2) and (3) hold, we also have $\tau_{ARCL} \geq_{lr} \tau_{ARSL}$. That completes the proof.

Proof of Theorem 6

According to Definition 1(i), the desired result is equivalent to

$$\Lambda(u_1, u_2, \dots, u_{m+1}) = \frac{F_{\text{ARCL}}(u_1, u_2, \dots, u_{m+1})}{F_{\text{ARSL}}(u_1, u_2, \dots, u_{m+1})} = \frac{1 - q(1 - C(u_1, u_2, \dots, u_{m+1}))}{C(1 - q(1 - u_1), 1 - q(1 - u_2), \dots, 1 - q(1 - u_{m+1}))}$$

is increasing in $u_i \in (0, 1)$, $i = 1, 2, \dots, m + 1$. Observe that

$$\frac{\partial \Lambda(u_1, u_2, \dots, u_{m+1})}{\partial u_i} \stackrel{\text{sgn}}{=} \frac{q'(1 - C(\mathbf{u}))\partial C(\mathbf{u})/\partial u_i}{1 - q(1 - C(\mathbf{u}))} - \frac{q'(1 - u_i)\partial C(\mathbf{1} - \mathbf{q}(\mathbf{1} - \mathbf{u}))/\partial (1 - q(1 - u_i))}{C(\mathbf{1} - \mathbf{q}(\mathbf{1} - \mathbf{u}))}$$
$$\stackrel{\text{sgn}}{=} \alpha_i^C(\mathbf{u}) \cdot L_q(1 - C(\mathbf{u})) - \alpha_i^C(\mathbf{1} - \mathbf{q}(\mathbf{1} - \mathbf{u})) \cdot L_q(1 - u_i)$$
$$\geq 0,$$

where $\mathbf{u} = \{u_1, u_2, \dots, u_{m+1}\}, C(\mathbf{u}) = C(u_1, u_2, \dots, u_{m+1}), \mathbf{1} - \mathbf{q}(\mathbf{1} - \mathbf{u}) = \{1 - q(1 - u_1), 1 - q(1 - u_2), \dots, 1 - q(1 - u_{m+1})\}$. The inequality is derived from conditions (1), (2) and (3) based on $1 - q(1 - u_i) \ge u_i$ and $C(\mathbf{u}) \le u_i$, $i = 1, 2, \dots, m + 1$, which completes the proof.

Cite this article: Yan R, Wang J and Lu B (2022). Orderings of component level versus system level at active redundancies for coherent systems with dependent components. *Probability in the Engineering and Informational Sciences* **36**, 1275–1297. https://doi.org/10.1017/S0269964821000401