

Effects of phase difference between instability modes on boundary-layer transition

Minwoo Kim^{1,‡}, Seungtae Kim^{1,‡}, Jiseop Lim¹, Ray-Sing Lin¹,
Solkeun Jee^{1,†} and Donghun Park²

¹School of Mechanical Engineering, Gwangju Institute of Science and Technology, Gwangju 61005, Korea

²Department of Aerospace Engineering, Pusan National University, Busan 46241, Korea

(Received 13 January 2021; revised 27 July 2021; accepted 14 August 2021)

Phase effect on the modal interaction of flow instabilities is investigated for laminar-to-turbulent transition in a flat-plate boundary-layer flow. Primary and secondary three-dimensional (3-D) oblique waves at various initial phase differences between these two instability modes. Three numerical methods are used for a systematic approach for the entire transition process, i.e. before the onset of transition well into fully turbulent flow. Floquet analysis predicts the subharmonic resonance where a subharmonic mode locally resonates for a given basic flow composed of the steady laminar flow and the fundamental mode. Because Floquet analysis is limited to the resonating subharmonic mode, nonlinear parabolised stability equation analysis (PSE) is conducted with various phase shifts of the subharmonic mode with respect to the given fundamental mode. The application of PSE offers insights on the modal interaction affected by the phase difference up to the weakly nonlinear stage of transition. Large-eddy simulation (LES) is conducted for a complete transition to turbulent boundary layer because PSE becomes prohibitively expensive in the late nonlinear stage of transition. The modulation of the subharmonic resonance with the initial phase difference leads to a significant delay in the transition location up to $\Delta Re_{x,tr} \simeq 4 \times 10^5$ as predicted by the current LES. Effects of the initial phase difference on the spatial evolution of the modal shape of the subharmonic mode are further investigated. The mechanism of the phase evolution is discussed, based on current numerical results and relevant literature data.

Key words: boundary layer stability, nonlinear instability, transition to turbulence

1. Introduction

Laminar-to-turbulent transition may occur in boundary-layer flow after instability modes in the laminar region interact each other. Challenges in assessing the transition

[†] Email address for correspondence: sjee@gist.ac.kr

[‡] M. Kim and S. Kim contributed equally to this work.

mechanism arise owing to the nonlinear (or energetic) interaction. Various transition routes were suggested for wall-bounded flow by Morkovin (1969) about five decades ago. Disturbances outside the boundary layer are converted to a primary instability inside the boundary layer through the receptivity process, secondary instability normally occurs as the primary instability grows to sufficiently large amplitude and promotes modal interactions. The secondary instability (here, subharmonic resonance) occurs following the amplification of a three-dimensional (3-D) wave initiated by a two-dimensional (2-D) Tollmien–Schlichting (TS) wave, i.e. the primary instability mode of the Orr–Sommerfeld flow field. The 3-D wave has one-half the frequency of the fundamental TS wave.

Significant progress has been made in the understanding of secondary instabilities, which have been well reviewed in Herbert (1988), Kachanov (1994), Saric, Reed & White (2003) and Schmid (2007). Subharmonic secondary instability has been investigated extensively, using theoretical approaches (Craik 1971; Herbert 1984, 1988; Wu 2019), experimental studies (Kachanov & Levchenko 1984; Corke & Mangano 1989; Borodulin, Kachanov & Koptsev 2002; Würz *et al.* 2012a) and numerical investigation (El-Hady 1988; Nayfeh & Masad 1990; Bertolotti, Herbert & Spalart 1992; Joslin, Streett & Chang 1993; Xu, Lombard & Sherwin 2017; Jee, Joo & Lin 2018; Kim *et al.* 2019, 2020). The current study focuses on the subharmonic resonance in the natural transition path for incompressible flow. Other transition routes including a non-modal interaction leading to transient growth and bypass transition are well reviewed by Schmid (2007) and Durbin & Wu (2007), respectively.

It is well recognised that the early stage of secondary instability involves the parametric resonance of the subharmonic mode with respect to the basic flow composed of steady slow-varying laminar flow and the 2-D fundamental mode (Herbert 1984, 1988; El-Hady 1988; Nayfeh & Masad 1990). The parametric resonance of the subharmonic mode can be analysed with Floquet theory applied to the basic flow. Among several parameters of the instability modes affecting the growth of the subharmonic mode, key parameters have been identified as the local Reynolds number of the basic flow, the amplitude of the fundamental mode and the spanwise wavenumber of the subharmonic mode (Herbert 1988). Floquet analysis for subharmonic resonance (Herbert 1984; Herbert, Bertolotti & Santos 1987; Nayfeh & Masad 1990) has been validated for the well-controlled experiments of Klebanoff, Tidstrom & Sargent (1962) and Kachanov & Levchenko (1984).

Despite a vast amount of literature on subharmonic resonance, a complete understanding of the nonlinear interaction between the fundamental and the subharmonic modes has not been achieved. In particular, the nonlinear interaction influenced by the phase difference between the two waves has not gained enough attention in the research community. Recently, Park *et al.* (2021) reproduced the phase-dependent subharmonic resonance observed in the experiment of Borodulin *et al.* (2002) using nonlinear parabolised stability equation analysis (PSE). Yet, the effect of the phase difference on the subharmonic resonance has not been fully identified. Note that previous studies (Borodulin *et al.* 2002; Würz *et al.* 2012a; Park *et al.* 2021) were still confined to the pre-turbulence region due to experimental (Borodulin *et al.* 2002; Würz *et al.* 2012a) and numerical (Park *et al.* 2021) constraints.

The goal of the current study is to improve the understanding of the phase effect on boundary-layer transition, covering a wide transition range from the early stage of primary and secondary instabilities to turbulent flow. To achieve such a comprehensive investigation, three numerical methods are judiciously incorporated: Floquet analysis, PSE and large-eddy simulation (LES). Floquet analysis provides a resonating subharmonic mode (secondary instability) with respect to the fundamental mode (primary instability).

An in-house code has been developed for the current Floquet analysis based on previous studies (El-Hady 1988; Nayfeh & Masad 1990). Because Floquet analysis is limited to the resonant subharmonic mode (resonant phase difference), PSE is chosen as a higher-fidelity stability analysis for non-resonant phase differences. Because PSE can handle the nonlinearity and non-parallelism of the disturbance equations, the instability evolution affected by the phase can be investigated in the nonlinear transition region. A well-validated nonlinear PSE code by Park & Park (2013, 2016); Park *et al.* (2021) is used in the current study. Although PSE is an effective method for stability analysis in a pre-turbulence region, it is computationally prohibitive in turbulent flow. The authors have developed an LES method coupled with stability analysis (Kim *et al.* 2019, 2020; Lim *et al.* 2021) for a cost-effective and high-fidelity simulation of a transitional boundary layer. This LES method is used for a complete turbulent transition here, and the transition location controlled by the initial phase difference is quantified. It should be noted that the current LES approach (Kim *et al.* 2019, 2020) provides direct numerical simulation (DNS) fidelity in the laminar region where disturbances are deterministic.

In § 2, three methods, Floquet analysis, PSE and LES are described. The validation of the current Floquet analysis is discussed in § 3.1. The effect of the phase difference on the subharmonic resonance is thoroughly investigated using PSE and LES in § 3.2 and 3.3, respectively. The mechanism of the phase synchronisation from anti-resonant conditions is discussed in § 3.4. Because the amplitude of the fundamental mode (not the subharmonic mode) is a major parameter to affect the subharmonic resonance, amplitude effects on anti-resonance and phase synchronisation are further studied in § 3.5. A summary and conclusions are given in § 4.

2. Methods

Three numerical methods are used in this study. Parametric resonance of the subharmonic oblique wave is investigated using Floquet analysis. The PSE is conducted to study the effect of the phase difference on the parametric resonance. The LES is carried out to simulate complete transition to turbulent boundary layer. Floquet analysis, PSE and LES are briefly discussed in §§ 2.1, 2.2 and 2.3, respectively.

In this study, a total variable $\check{\psi}$ is decomposed to the undisturbed part Ψ and the disturbance ψ .

$$\check{\psi} = \Psi + \psi. \quad (2.1)$$

The Cartesian coordinate system is used with the streamwise x , wall-normal y and spanwise z direction, along with the corresponding velocity components u , v and w . Dimensionless variables are obtained with the length scale $\tilde{\delta}_r (R = R_o)$, the free-stream velocity \tilde{U}_∞ and the dynamic pressure $\tilde{\rho} \tilde{U}_\infty^2$, where the local length variable is $\tilde{\delta}_r = \sqrt{\tilde{x}_r \tilde{\nu} / \tilde{U}_\infty}$, \tilde{x}_r is the distance from the leading edge of a flat plate, $\tilde{\nu}$ is kinematic viscosity, the local Reynolds number is $R = \tilde{U}_\infty \tilde{\delta}_r / \tilde{\nu} = \sqrt{\tilde{U}_\infty \tilde{x}_r / \tilde{\nu}} = \sqrt{Re_x}$, the reference R is $R_o = 400$ and $\tilde{\rho}$ is the fluid density. The tilde denotes a dimensional variable.

2.1. Floquet analysis

Floquet analysis is based on a parametric formulation which describes a secondary instability for a given primary instability (Herbert 1984; Herbert *et al.* 1987; El-Hady 1988; Nayfeh & Masad 1990). The current Floquet analysis, briefly described here, adopts the

Analysis type	Basic flow (given)	Disturbance (unknown)	Equation for analysis
Primary instability analysis (2.4)	Laminar solution (2.3)	2-D fundamental TS wave	(A1)
Secondary instability analysis (Floquet)	Laminar + 2-D TS wave (2.5)	3-D subharmonic wave (2.6)	(A3)

Table 1. Basic flow and disturbance for each analysis of primary and secondary instability.

approach of Nayfeh & Masad (1990) and El-Hady (1988) instead of the stream-function approach of Herbert (1984) and Herbert *et al.* (1987).

The governing equations of a disturbance (u, v, w, p) for an undisturbed basic flow (U, V) are written as

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0, \tag{2.2a}$$

$$\frac{\partial u}{\partial t} + U \frac{\partial u}{\partial x} + v \frac{\partial U}{\partial y} + \frac{\partial p}{\partial x} - \frac{1}{R_o} \nabla^2 u + \left[u \frac{\partial U}{\partial x} + V \frac{\partial u}{\partial y} \right] + \mathbb{N}_u = 0, \tag{2.2b}$$

$$\frac{\partial v}{\partial t} + U \frac{\partial v}{\partial x} + \frac{\partial p}{\partial y} - \frac{1}{R_o} \nabla^2 v + \left[u \frac{\partial V}{\partial x} + V \frac{\partial v}{\partial y} + v \frac{\partial V}{\partial y} \right] + \mathbb{N}_v = 0, \tag{2.2c}$$

$$\frac{\partial w}{\partial t} + U \frac{\partial w}{\partial x} + \frac{\partial p}{\partial z} - \frac{1}{R_o} \nabla^2 w + \left[V \frac{\partial w}{\partial y} \right] + \mathbb{N}_w = 0, \tag{2.2d}$$

where the square-bracket terms represent the non-parallel nature of the basic flow. The nonlinear terms of the disturbance \mathbb{N} are negligible here.

The instability analysis involves two steps: primary and secondary instability. The primary instability analysis provides a 2-D fundamental TS wave for a given basic laminar flow, whereas the secondary instability analysis (Floquet) yields a 3-D subharmonic wave for a given basic flow in which the 2-D wave is additionally included. The current analysis is summarised in table 1 with a brief description below.

For the primary instability of a boundary layer, we consider the basic flow

$$\{U, V\} = \{U_L(y), 0\}, \tag{2.3}$$

where U_L is the laminar solution without any disturbance (here the Blasius solution). Then, a fundamental planar TS wave can be written as

$$\{u, v, p\} = \{\zeta_1(y), \zeta_3(y), \zeta_4(y)\} \exp[i(\alpha x - \omega t)] + \text{c.c.}, \tag{2.4}$$

where the notation c.c. indicates the complex conjugate. The functions $\zeta_1(y)$, $\zeta_3(y)$ and $\zeta_4(y)$ are the mode shape of the fundamental TS components u , v and p , respectively. For a spatially evolving disturbance, the complex wavenumber α and the real angular frequency ω are used.

To obtain the subharmonic oblique wave in the Floquet analysis, the basic flow (2.5) includes both the laminar flow and the fundamental 2-D TS wave.

$$U = U_L(y) + A [\zeta_1(y) \exp(i\theta) + \zeta_1^*(y) \exp(-i\theta)], \quad (2.5a)$$

$$V = A [\zeta_3(y) \exp(i\theta) + \zeta_3^*(y) \exp(-i\theta)], \quad (2.5b)$$

where A is the r.m.s. amplitude of the fundamental TS wave, ζ^* is the complex conjugate of the function ζ and $\theta(x, t) = \text{Re}(\alpha)x - \omega t$. The notations Re and Im indicate the real and the imaginary part of a complex variable, respectively. Floquet theory suggests that the approximate solution of (2.2) for the given basic flow of (2.5) can be written as

$$\begin{Bmatrix} u_{1/2} \\ v_{1/2} \\ p_{1/2} \end{Bmatrix} = \left[\begin{Bmatrix} \eta_1(y) \\ \eta_3(y) \\ \eta_4(y) \end{Bmatrix} \exp(i\theta/2) + \begin{Bmatrix} \eta_7(y) \\ \eta_9(y) \\ \eta_{10}(y) \end{Bmatrix} \exp(-i\theta/2) \right] \cos(\beta z) \exp(\gamma x), \quad (2.6a)$$

$$w_{1/2} = [\eta_5(y) \exp(i\theta/2) + \eta_{11}(y) \exp(-i\theta/2)] \sin(\beta z) \exp(\gamma x), \quad (2.6b)$$

where the subharmonic wavenumber in the streamwise direction is $\alpha_{1/2} = \text{Re}(\alpha)/2$, the subharmonic frequency is $\omega_{1/2} = \omega/2$ (so, $\theta/2 = \alpha_{1/2}x - \omega_{1/2}t$), the spanwise wavenumber of the subharmonic mode is β and the eigenvalue γ is real here. Further details are documented in Appendix A, including the exact equation for each analysis, boundary conditions and the computational method for the eigenvalue problems.

2.2. PSE

The method of PSE is an efficient way to treat weakly nonlinear regions where parametric resonance occurs. The amplitude of the subharmonic mode remains small so that the back influence of the subharmonic mode on the fundamental mode is negligible. A formal approach of PSE is to decompose the disturbance ψ into a fast-varying oscillatory-wave part and a slow-varying shape function, using Fourier expansion, as written in (2.7).

$$\psi(x, y, z, t) = \sum_{m=-N_m}^{N_m} \sum_{n=-N_n}^{N_n} \hat{\psi}_{(m,n)}(x, y) \exp \left[i \left\{ \int_{x_0}^x \alpha_{(m,n)}(s) ds + n\beta z - \frac{1}{2}m\omega t \right\} \right], \quad (2.7)$$

where the shape function $\hat{\psi}_{(m,n)}$ is a complex function, the streamwise wavenumber $\alpha_{(m,n)}$ is a complex number the spanwise wavenumber β is a real number. The subscript m and n indicates the temporal and spanwise modes, respectively. The wavenumber $\alpha_{(2,0)}$ of the fundamental TS wave corresponds to the wavenumber α in (2.4). The subharmonic wavenumber $\alpha_{(1,1)}$ is associated with the notations $\alpha_{1/2}$ and γ in (2.6), i.e. $\alpha_{(1,1)} = \alpha_{1/2} - i\gamma$. The spatial growth rate of the subharmonic mode is $\text{Im}(\alpha_{(1,1)}) = -\text{Re}(\gamma)$.

A set of partial differential equations for the shape functions with the unknown variable $\alpha_{(m,n)}$ is obtained for a given frequency (here the fundamental frequency ω) and the spanwise wavenumber β . These equations are parabolised and numerically solved in the PSE code developed in Park & Park (2013, 2016). Nonlinear PSE is conducted with $N_m = 6$ and $N_n = 3$, keeping a total of 28 modes including the mean distortion (0, 0) mode, in the domain of $400 \leq R \leq 700$. A fourth-order central scheme and a second-order backward scheme are used for the wall-normal and the streamwise direction, respectively. Uniform grids with 107 points are used in the streamwise direction. At least 80 points are placed in the boundary layer with a total 220 points in the wall-normal domain, extending

to $200\tilde{\delta}_r$. Further details of the PSE code and numerical approaches are documented in Park & Park (2013, 2016), Kim *et al.* (2019) and Park *et al.* (2021).

It should be noted that the PSE code is based on the compressible form of the disturbance equation. To approximate the incompressible boundary layer, the mean flow of very low free-stream speed whose Mach number is 0.0269 is chosen (i.e. 9.16 m s^{-1} with the standard atmospheric condition at sea level). At this Mach number condition and at the corresponding mean flow conditions, the density and temperature fluctuations behave as redundant variables in the PSE analysis. Although the compressible formulation is used and all terms are kept, the results can be regarded as nearly identical to those obtained from the incompressible formulation as they have been validated through many cases (Bertolotti *et al.* 1992; Chang *et al.* 1993; Gao, Park & Park 2011; Park & Park 2013). In addition, the results from the Floquet theory are used as the inlet boundary conditions for the PSE as well as LES. For the initial condition of PSE, the pressure and velocity disturbances are set as the Floquet theory results, while the density and temperature disturbances are set as zero. As a consequence, there might be a small difference in comparison with the solution with the compressible formulation. However, this discrepancy is also almost negligible owing to the very low Mach number considered.

2.3. LES

Because neither Floquet analysis nor PSE are efficient for incorporating higher instability in the late stage of transition, LES is conducted to model the boundary-layer flow well into a fully turbulent state. The total variable $\check{\psi}$ is decomposed to the spatially filtered $\bar{\psi}$ and the filtered residual part ψ' for LES.

$$\check{\psi} = \bar{\psi} + \psi'. \quad (2.8)$$

Note that there is no distinction between $\check{\psi}$ and $\bar{\psi}$ in the computation of laminar flow because LES is essentially DNS in this case (Kim *et al.* 2019, 2020). The residual part ψ' is a turbulence fluctuation, so $\psi' = 0$ in the pre-transition region where the deterministic disturbance ψ (see (2.1)) is well resolved with the current fine grid.

The filtered incompressible dimensionless Navier–Stokes equations are written as (2.9).

$$\frac{\partial \bar{u}_i}{\partial x_i} = 0, \quad (2.9a)$$

$$\frac{\partial \bar{u}_j}{\partial t} + \frac{\partial}{\partial x_i} (\bar{u}_i \bar{u}_j) = \frac{1}{R} \frac{\partial^2 \bar{u}_j}{\partial x_i \partial x_i} - \frac{\partial \tau_{ij}^r}{\partial x_i} - \frac{\partial \bar{p}}{\partial x_j}, \quad (2.9b)$$

$$\tau_{ij}^r = -2\nu_t \bar{S}_{ij}, \quad (2.9c)$$

$$\bar{S}_{ij} = \frac{1}{2} \left(\frac{\partial \bar{u}_i}{\partial x_j} + \frac{\partial \bar{u}_j}{\partial x_i} \right), \quad (2.9d)$$

where the residual stress tensor τ_{ij}^r is modelled to be linearly proportional to the resolved strain rate \bar{S}_{ij} . The turbulence viscosity ν_t is obtained with the wall-adapting local eddy-viscosity model (see Nicoud & Ducros 1999). The model coefficient is $C_w = 0.5$ as suggested in Nicoud & Ducros (1999) and tested in the transitional boundary layer in Kim *et al.* (2019, 2020). The sub-grid-scale turbulence model is judiciously chosen for wall-resolved LES in the transitional boundary layer (Kim *et al.* 2020), the model is

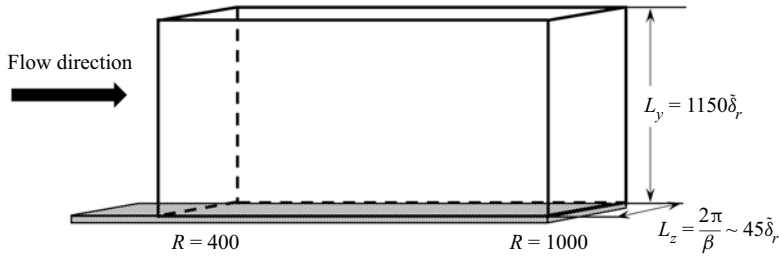


Figure 1. Schematic diagram of the LES computational domain.

properly activated only in the very late transition stage and the subsequent turbulent region in the current simulation.

The computational domain is depicted in figure 1. At the LES inlet, the fundamental and subharmonic modes are assigned to the laminar solution. The convective outlet is applied at the exit boundary, and no-slip condition at the wall. The fine grid of Kim *et al.* (2019) is used here with a small enough time step $\Delta t = (1/256)(2\pi/\omega)$ where ω is the angular frequency of the fundamental mode. Further details on the LES approach can be found in Kim *et al.* (2019, 2020).

2.4. Inlet conditions for PSE and LES

Both PSE and LES computations require a disturbance at the inlet boundary, which is located at $R = 400$. The 2-D TS wave and the pair of the 3-D oblique waves are obtained from the current Floquet analysis. Following the Floquet analysis of Herbert *et al.* (1987), which has been validated for the experiment of Kachanov & Levchenko (1984), the angular frequency of the 2-D wave is $\omega = 0.0496$ and the spanwise wavenumber of the 3-D wave is $\beta = 0.132$ based on the current non-dimensionalisation. These two parameters can be rewritten as $F = \omega/R \times 10^6 = 124$ and $b = \beta/R \times 10^3 = 0.33$, respectively, which are also commonly used in the literature. The r.m.s. amplitudes of the 2-D wave and the 3-D wave are $A_{(2,0)} = 4.0 \times 10^{-3}$ and $A_{(1,1)} = 1.64 \times 10^{-5}$, respectively, at the inlet, where the free-stream velocity is used for the scaling. At the LES and PSE inlet boundary, 2-D fundamental and 3-D subharmonic modes are added to the laminar solution; namely a zero-pressure-gradient flat-plate flow at $R = 400$.

The current Floquet analysis provides the mode shape of the fundamental (2-D TS wave) ζ and the subharmonic (3-D oblique wave) η modes, as shown in figure 2. The amplitude of each mode is scaled with the maximum value of each mode. The u component dominates both the fundamental and subharmonic modes. The amplitude peak of the fundamental and subharmonic modes is located at approximately one quarter of the boundary-layer thickness. The phase profile of the fundamental mode ζ_1 is relatively constant near the amplitude peak, whereas the phase of η_1 changes continuously.

The phase difference $\Delta\phi$ between the fundamental and the subharmonic modes is defined as (2.10), following experimental studies of Borodulin *et al.* (2002); Würz *et al.* (2012a).

$$\Delta\phi = \frac{1}{2}\phi_{(2,0)} - \phi_{(1,1)} \quad \text{at } y_{(1,1),max}, \quad (2.10)$$

where $y_{(1,1),max}$ is the location for the amplitude peak of the subharmonic mode which is $y_{(1,1),max} = 1.43$ at the inlet. The initial phase difference between the fundamental and subharmonic modes is $\Delta\phi_{in} = 130^\circ$ from the Floquet analysis. In the current PSE and LES

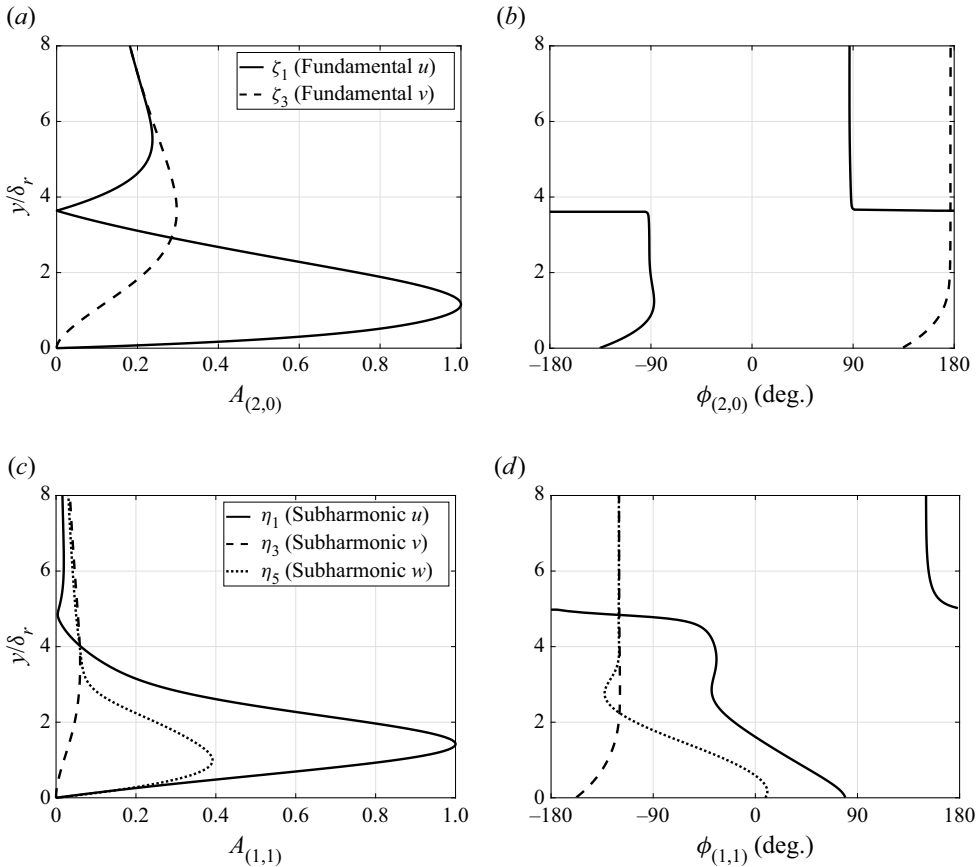


Figure 2. The fundamental and the subharmonic modes obtained from the current Floquet analysis at $R = 400$. (a) Amplitude $|\zeta|/\max(|\zeta|)$. (b) Phase $\phi_{(2,0)} = \arg(\zeta)$. (c) Amplitude $|\eta|/\max(|\eta|)$. (d) Phase $\phi_{(1,1)} = \arg(\eta)$.

computations, $\Delta\phi_{in}$ varies in the periodic range of 180° to allow investigation of the effect of the phase difference on the secondary instability and eventually on turbulent transition. The subharmonic phase is shifted with respect to the given fundamental mode. There is no distinction between the phase lead and lag results in the periodicity of 180° for the phase difference.

3. Results

The effect of the modal phase on the growth of the secondary instability (here, the subharmonic mode) is investigated using three approaches, i.e. Floquet analysis, PSE and LES. The baseline case is the subharmonic resonance in the zero-pressure-gradient boundary layer on a flat plate, which was experimentally studied by Kachanov & Levchenko (1984). The current Floquet analysis, validated against the experimental (Kachanov & Levchenko 1984) and the numerical data (Herbert *et al.* 1987) in § 3.1, provides a resonating subharmonic mode for the given basic flow which consists of laminar flow and the fundamental mode (2-D TS wave). Because of the nature of the eigenvalue problem explored in the Floquet analysis, other methods are required for less resonating conditions affected by the modal phase. Here, PSE and LES are used. The phase effect

is first discussed with PSE in § 3.2 and then with LES in § 3.3. A further investigation on the transition location delay affected by the phase and the resonance mechanism from an anti-resonant initial condition is included in § 3.4. Because the fundamental amplitude is one of major parameters affecting the subharmonic resonance, it is speculated that the evolution of the subharmonic mode from the anti-resonant initial condition is also affected by the fundamental amplitude, not the subharmonic amplitude. Such amplitude effects are assessed in § 3.5.

3.1. Validation of instability analysis

The current instability analysis consists of two parts, one for the primary instability (2-D fundamental TS wave) and the other for the secondary instability (3-D subharmonic oblique wave). The eigenvalue problem of each analysis is summarised in table 1 along with the given basic flow. Floquet analysis provides the most unstable mode for the subharmonic oblique wave, yielding the mode shape η and the exponent γ whose positive real value is the spatial growth rate of the subharmonic wave.

The mode shape and the amplitude growth of the subharmonic mode are compared with the experimental data of Kachanov & Levchenko (1984) and the Floquet analysis of Herbert *et al.* (1987), as shown in figure 3. The amplitude growth is obtained, using the integration

$$\frac{A_{(2,0)}(x)}{A_{(2,0)}(x_0)} = \int_{x_0}^x -\text{Im}(\alpha_{(2,0)}) \, ds, \quad (3.1)$$

$$\frac{A_{(1,1)}(x)}{A_{(1,1)}(x_0)} = \int_{x_0}^x \text{Re}(\gamma) \, ds = \int_{x_0}^x -\text{Im}(\alpha_{(1,1)}) \, ds, \quad (3.2)$$

where the initial location x_0 corresponds to $R = 400$ and the initial amplitudes are $A_{(2,0)}(x_0) = 4 \times 10^{-3}$ and $A_{(1,1)}(x_0) = 1.64 \times 10^{-5}$. The two mode shapes are identical to the literature data at $R = 600$ in figures 3(a) and 3(b). The location $R = 600$ is positioned in the subharmonic resonance range shown in figure 3(c). The amplitude growth from the current Floquet analysis matches well with the experimental data of Kachanov & Levchenko (1984) and the Floquet analysis of Herbert *et al.* (1987). According to the discussion of Herbert *et al.* (1987), the subharmonic mode in the experiment (Kachanov & Levchenko 1984) was not fully formed until $R \simeq 540$ because of the proximity to the vibrating ribbon for the disturbance generation. The measurement of Kachanov & Levchenko (1984) showed that the disturbance mode (1, 1) had no definite phase value until $R \simeq 540$ and was deeply buried in background noise. Note that branch I of the neutral curve of the subharmonic mode in linear stability analysis is located near $R = 540$ (see Kachanov & Levchenko 1984, figure 3). It should be mentioned that the spatial growth data of the subharmonic mode (Herbert *et al.* 1987) are used for the comparison here because the transformed data of the temporally growing mode (Herbert 1984) overestimates the growth rate (Herbert *et al.* 1987).

The current Floquet analysis provides only the most resonating condition for the subharmonic mode for the given basic flow. Less resonating conditions, including the anti-resonant condition, can be obtained with the phase variation of the subharmonic oblique wave with the amplitude fixed. PSE and LES computations are explored for the investigation of the phase effect on the subharmonic resonance in the following sections.

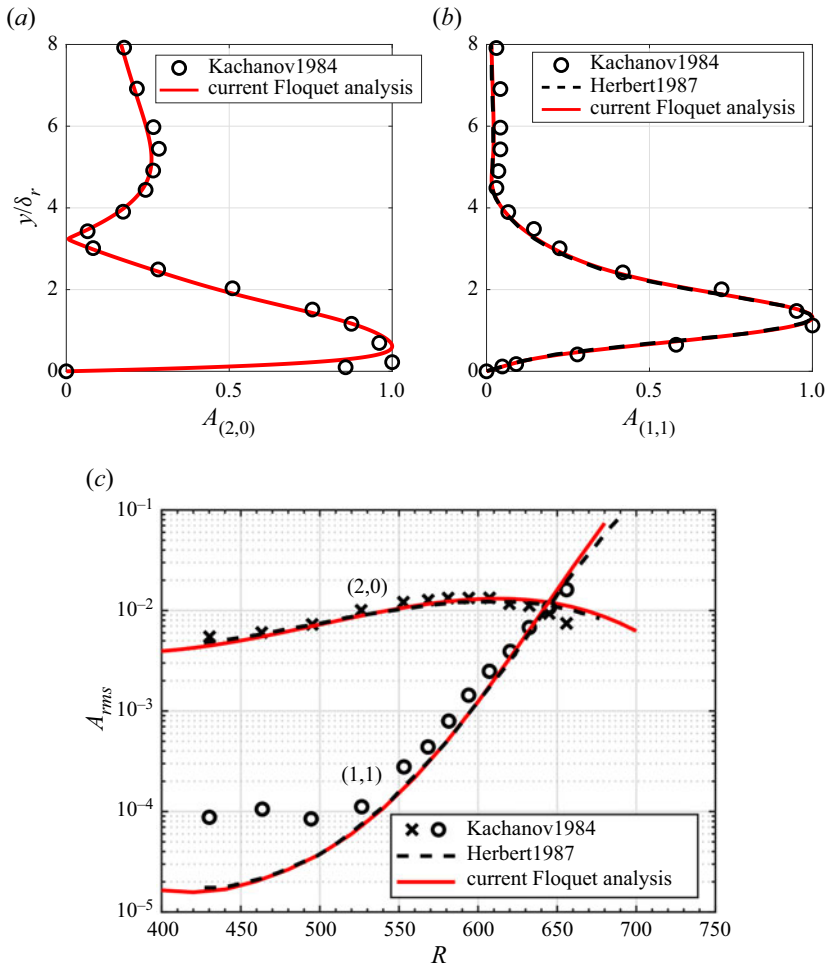


Figure 3. Comparison among the current Floquet analysis, the Floquet analysis of Herbert *et al.* (1987) and the experimental data of Kachanov & Levchenko (1984) for the (a) fundamental and (b) subharmonic modes at $R = 600$ and (c) the amplitude growth of the two modes.

3.2. Phase effects on subharmonic resonance in PSE computations

The PSE method is computationally efficient in investigating nonlinear interactions of instability modes in the transition region. The current PSE method, validated in the subharmonic resonance (Park & Park 2013; Kim *et al.* 2019), is explored here with the baseline inlet condition obtained from the current Floquet analysis. The inlet condition consists of the 2-D fundamental TS and 3-D subharmonic oblique modes. Further details of the baseline inlet condition, including the amplitude of the each mode, are provided in § 2.4.

The current Floquet analysis yields the phase difference between the fundamental and subharmonic modes $\Delta\phi_{in} = 130^\circ$ at the inlet location $R = 400$. Only the phase of the subharmonic mode varies so that the whole periodic range $0 \leq \Delta\phi_{in} \leq 180^\circ$ is simulated here. Other characteristics, including the amplitudes ($A_{(2,0)}$ and $A_{(1,1)}$) and the mode shapes ($\zeta(y)$ and $\eta(y)$), remain the same at the inlet.

Effects of phase difference on boundary-layer transition

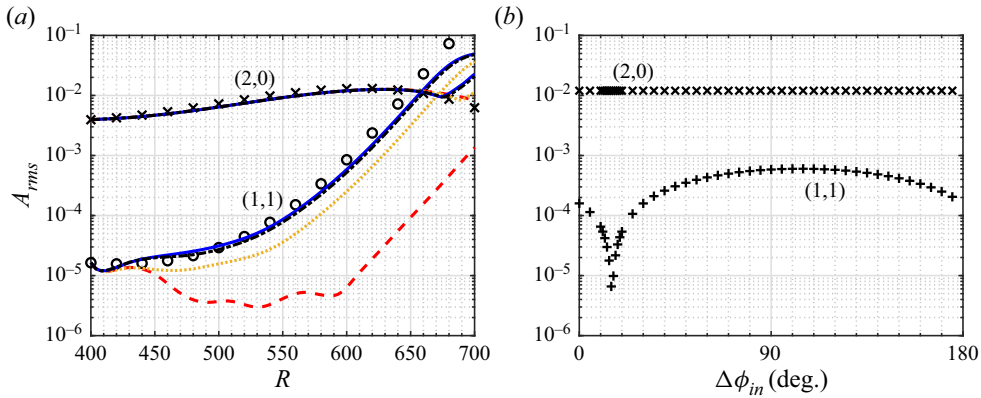


Figure 4. Amplitude of the fundamental and subharmonic modes affected by the initial phase difference in the current simulation. (a) Amplitude growth: \times , Floquet analysis, (2,0); \circ , Floquet analysis, (1,1); dashed dotted line, PSE, $\Delta\phi_{in} = 130^\circ$; blue solid line, PSE, $\Delta\phi_{in} = 105^\circ$; orange dotted line, PSE, $\Delta\phi_{in} = 40^\circ$; red dashed line, PSE, $\Delta\phi_{in} = 15^\circ$. (b) Amplitude at $R = 600$: \times , PSE, (2,0); $+$, PSE, (1,1).

The initial phase difference significantly affects the amplitude evolution of the subharmonic mode as shown in figure 4. A total of 44 initial phase differences are simulated in the current PSE. Four selected phase differences, including the baseline $\Delta\phi_{in} = 130^\circ$, are shown in figure 4(a). A phase shift of 25° from the baseline $\Delta\phi_{in} = 105^\circ$ provides the almost identical evolution of the baseline amplitude for the subharmonic mode. The Floquet analysis data are similar to the PSE data of $\Delta\phi_{in} = 130^\circ$ and $\Delta\phi_{in} = 105^\circ$. The phase shift of 90° from the baseline $\Delta\phi_{in} = 40^\circ$ yields a visual delay in the growth of the subharmonic mode. The case of $\Delta\phi_{in} = 15^\circ$ even damps the subharmonic mode at the beginning until $R \simeq 600$, and the subharmonic mode starts to exponentially grow after $R = 600$. The amplitude of the fundamental mode remains almost the same until $R \simeq 670$ regardless of the initial phase shift of the subharmonic mode.

Figure 4(b) shows the amplitude of the fundamental and subharmonic modes at $R = 600$. The subharmonic mode resonates most when the initial phase difference is $\Delta\phi_{in} = 105^\circ$. The subharmonic resonance is not sensitive to the phase if the phase difference is in the wide range of $60 \lesssim \Delta\phi_{in} \lesssim 150^\circ$ where the amplitude does not change by more than a factor of 1.5. In contrast, the subharmonic amplitude is significantly damped in the narrow range of $5 \lesssim \Delta\phi_{in} \lesssim 25^\circ$, more than a factor of five compared to the case of $\Delta\phi_{in} = 105^\circ$. At the phase valley $\Delta\phi_{in} = 15^\circ$, the subharmonic amplitude is two orders of magnitude lower than that of $\Delta\phi_{in} = 105^\circ$. The least resonating condition is called anti-resonance. The phase difference between maximum resonance and anti-resonance in the current PSE is 90° , as similarly observed in experiments with mild adverse pressure gradients (Borodulin *et al.* 2002).

Floquet analysis yields slightly large amplitude growth for the subharmonic mode, compared with the PSE in the downstream region (see figure 4a). Because the disturbance equations are much simplified in the Floquet analysis, the detailed response of the subharmonic mode with respect to the given basic flow could be different to the PSE counterpart. Additional PSE computations are conducted to investigate whether the assumptions used in the Floquet analysis contribute to the slight difference in the amplitude growth. Three distinct assumptions of the Floquet analysis are individually tested in the additional PSE computations: the parallel assumption of the basic flow, the exclusion of the nonlinear feedback from the subharmonic to fundamental mode and the

exclusion of the mean flow distortion (0, 0) mode. Each individual assumption yields almost identical results to the PSE data shown in [figure 4\(a\)](#). It can be conjectured that a different set of disturbance equations as a whole between the Floquet analysis and PSE may contribute to the subtle difference in the growth in [figure 4\(a\)](#).

The subharmonic resonance (secondary instability) is influenced by the fundamental mode (primary instability) via nonlinear interaction. In contrast, almost no variation of the fundamental amplitude indicates that the feedback effect on the fundamental mode from the subharmonic mode is negligible until the subharmonic mode gains enough strength. In the current stability analysis using the Floquet and PSE computations, the early nonlinear region of the subharmonic resonance ends at approximately $R = 670$, and after that it can be expected that more modes rapidly evolve through higher nonlinear interactions (tertiary, quaternary, and so on).

In the early nonlinear stage, it has been understood that the subharmonic mode resonates via the parametric resonance (Herbert *et al.* 1987; El-Hady 1988; Nayfeh & Masad 1990). Key parameters of the basic flow affecting the subharmonic resonance are the Reynolds number of the laminar flow R , the amplitude $A_{(2,0)}$ and the frequency ω of the fundamental mode and the spanwise wavenumber β of the subharmonic mode. In addition to these parameters, the phase difference between the two modes is also another important parameter, according to the current PSE with various phase differences. Because the subharmonic resonance can be affected by the phase difference only, a complete transition to turbulent flow can also be affected by the phase difference. Because PSE becomes computationally expensive in the late nonlinear stage of the transition, Navier–Stokes equations are solved efficiently with the validated LES approach (Jee *et al.* 2018; Kim *et al.* 2019, 2020; Lim *et al.* 2021) for the final transition to the turbulent flow, which is discussed in the next section.

3.3. Phase effects on subharmonic resonance in LES computations

High-fidelity LES is conducted here in order to study the effect of the phase difference between the two instabilities on both the subharmonic resonance and the complete turbulent transition. A total of nine LES cases are simulated with the inlet phase differences $\Delta\phi_{in} = 5, 7, 10, 11, 15, 20, 25, 105$ and 130° . The PSE discussed in § 3.2 indicates that the subharmonic mode resonates for the given fundamental mode under the wide range of $60 \lesssim \Delta\phi_{in} \lesssim 150^\circ$, hence, the two cases $\Delta\phi_{in} = 105$ and 130° are simulated here. The PSE also suggests that the subharmonic resonance is significantly delayed when $5 \lesssim \Delta\phi_{in} \lesssim 25^\circ$, and the anti-resonant condition is highly sensitive to the initial phase. As a result, seven phases $\Delta\phi_{in} = 5, 7, 10, 11, 15, 20$ and 25° are selected in this narrow phase range. Note that the current LES approach has provided DNS-like fidelity for transitional boundary layers in the authors' previous studies (Kim *et al.* 2019, 2020). The LES statistics are obtained with LES data accumulated over eight periods of the fundamental mode after two flow-through times in the LES domain. The time window for the statistics is larger here compared to the LES validation study of Kim *et al.* (2019) because anti-resonant conditions yield longer-time variations in the flow solution.

The resonant and anti-resonant conditions are compared between the current LES and PSE computations, as shown in [figure 5](#). Two higher modes (3, 1) and (4, 0) are plotted along with the fundamental (2, 0) and subharmonic (1, 1) modes. The PSE is conducted until only $R = 700$ owing to an expected surge in the computational cost for the downstream, late nonlinear transition stage. Instead, LES is conducted continuously in

Effects of phase difference on boundary-layer transition

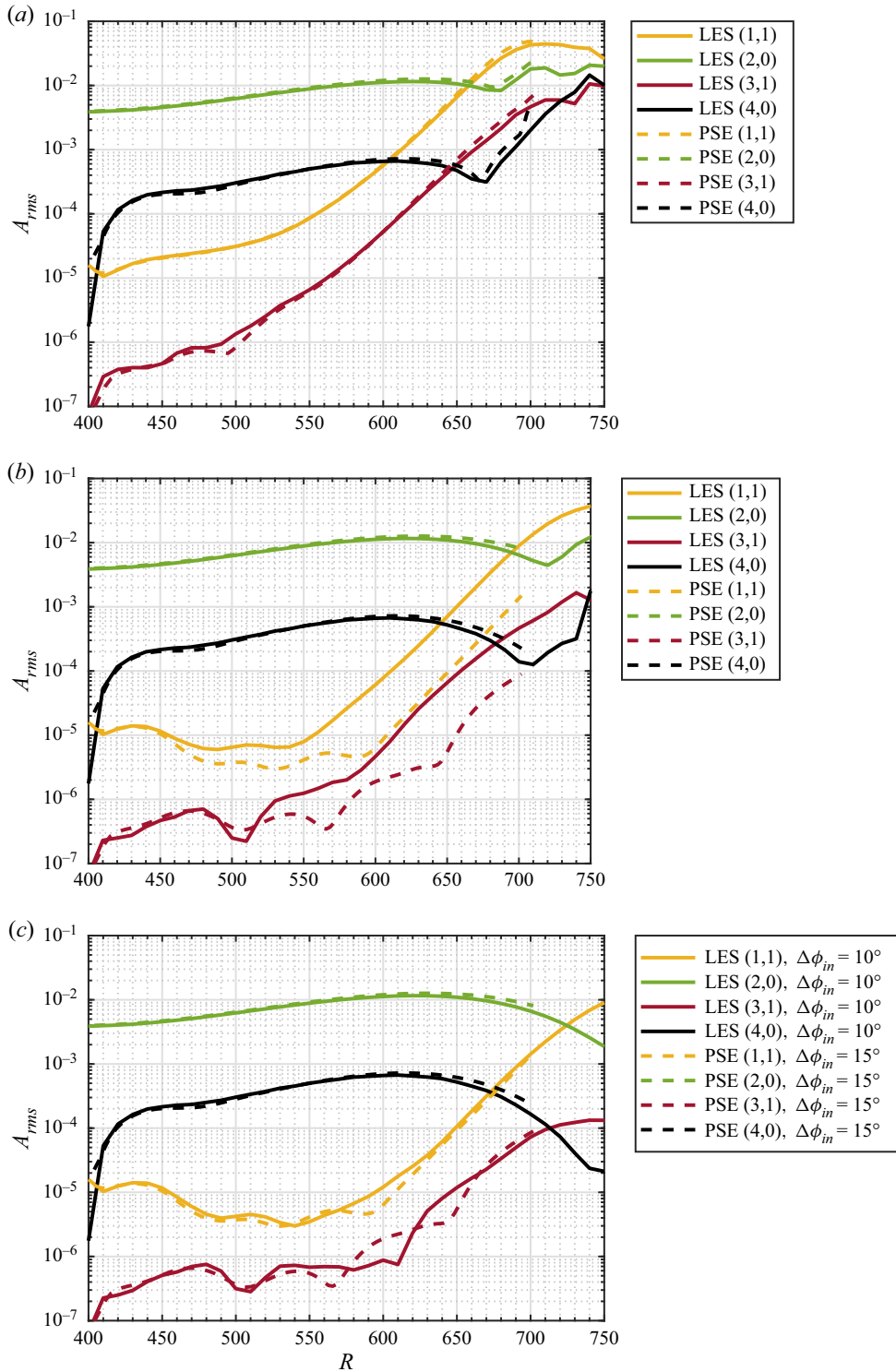


Figure 5. Amplitude growth of instability modes affected by the initial phase differences in the current PSE and LES computations. (a) Amplitude growth with $\Delta\phi_{in} = 105^\circ$. (b) Amplitude growth with $\Delta\phi_{in} = 15^\circ$. (c) Amplitude growth with the anti-resonant phase.

the further downstream up to $R = 1050$. The amplitude growth in the LES computations is shown until $R = 750$ in [figure 5](#).

Both LES and PSE provide almost identical growth of the selected instability modes in the resonant condition (see [figure 5a](#)). The resonant phase $\Delta\phi_{in} = 105^\circ$ yields the oblique modes (1, 1) and (3, 1) which grow exponentially from almost the inlet. Two planar modes (2, 0) and (4, 0) grow gradually until $R \simeq 650$ primarily owing to the linear growth of the fundamental mode (2, 0). The harmonic mode (4, 0) is mainly generated from the nonlinear effect of the fundamental mode, i.e. the nonlinear convective \mathbb{N} terms in (2.2). After $R \simeq 670$, the transition undergoes a highly nonlinear stage, and all the modes grow exponentially in the current simulation.

In [figure 5\(b\)](#), the initial phase difference $\Delta\phi_{in} = 15^\circ$ is simulated in both LES and PSE. Both LES and PSE provide delayed subharmonic resonance. However, the subharmonic mode begins to resonate with the fundamental mode after $R \simeq 550$ in LES, whereas $R \simeq 600$ in PSE. In the current LES computations, $\Delta\phi_{in} = 10^\circ$ yields the least resonating condition for the subharmonic mode (anti-resonance), and the instability growth is very similar to the anti-resonant condition of PSE, as shown in [figure 5\(c\)](#). The fundamental mode decays after $R \simeq 650$ owing to the insufficient growth of the subharmonic mode until $R = 750$. DNS computations (not shown here) in the anti-resonant condition also provide the almost identical results of the amplitude growth compared with LES, so the difference between LES and PSE for the anti-resonant phase may not come from the sub-grid-scale model which provides a negligible eddy viscosity until $R = 700$.

The current LES and PSE computations indicate that the anti-resonance phenomena is highly sensitive to the flow condition as shown in [figure 6](#) where the amplitude of the fundamental and subharmonic modes at $R = 600$ is plotted with the variation of the initial phase difference between the two modes. The anti-resonant phase is located in the narrow phase valley where the subharmonic amplitude varies by approximately a factor of ten only with the phase shift of 10° . The anti-resonant phase is slightly different between LES and PSE; $\Delta\phi_{in} = 10^\circ$ in LES and $\Delta\phi_{in} = 15^\circ$ in PSE. It is conjectured that the anti-resonance phenomena is sensitive to not only the initial phase difference but also the detailed flow solution of each computation. Because the full Navier–Stokes equations (2.9) in LES are not identical to those solved in PSE, a subtle difference between LES and PSE computations can cause a slight difference for the anti-resonant phase.

The phase effect on the subharmonic resonance eventually leads to a significant difference in the transition-to-turbulence location, as shown in [figure 7](#). The resonant condition results in staggered Λ -shape vortical structures at approximately $R = 700$ which is the footprint of the subharmonic resonance observed in previous experiments (Corke & Mangano 1989; Borodulin, Kachanov & Roschektayev 2011; Würz *et al.* 2012b) and high-fidelity computations (Sayadi, Hamman & Moin 2013; Jee *et al.* 2018; Kim *et al.* 2019, 2020). Fully turbulent flow starts roughly after $R = 750$ in the resonant condition. In contrast, the anti-resonant condition leads to significantly delayed transition. Staggered Λ -shape vortical structures appear in the long range $750 \lesssim R \lesssim 950$ with prolonged structures near the end of the transition. The vortical structures are elongated in the streamwise direction probably because of the weak nonlinear interaction among low-amplitude instabilities expected; see [figure 5\(c\)](#).

The skin friction C_f in [figure 8](#) indicates the transition region affected by the initial phase difference. The resonant conditions ($\Delta\phi_{in} = 105$ and 130°) yield the deviation of C_f from the laminar data at approximately $R = 690$ and the approach to turbulent C_f at approximately $R = 750$. In contrast, the anti-resonant condition with $\Delta\phi_{in} = 10^\circ$ leads to C_f deviation from the laminar at approximately $R = 820$ and the turbulent C_f near

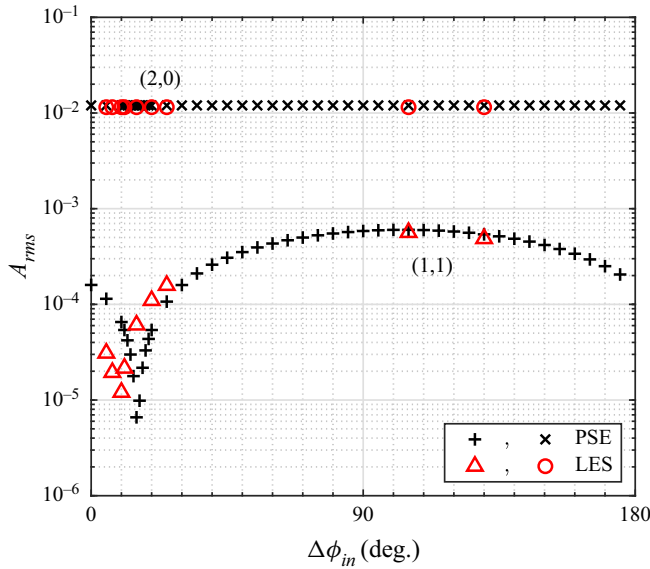


Figure 6. Amplitude of the fundamental and subharmonic modes at $R = 600$ affected by the initial phase difference in the current computations.

$R = 1000$. The prolonged vortical structures in figure 7(b) are associated with the long transition region.

Current LES computations indicate that the initial phase difference by itself can control the transition location, which was not disclosed in the literature. The anti-resonant phase delays the turbulent transition location by $\Delta R \simeq 1000 - 750 = 250$ which corresponds to $\Delta Re_x \simeq 4.4 \times 10^5$, an approximately 80% increase in the transition Reynolds number from the resonant condition. The phase difference between the fundamental and subharmonic modes was modulated with an array of microphones in previous experiments with non-zero pressure gradient (Borodulin *et al.* 2002; Würz *et al.* 2012a). Although complete transition to turbulent flow was not achieved in the experiments of Borodulin *et al.* (2002) and Würz *et al.* (2012a), the nonlinear interaction was significantly delayed with the anti-resonant phase. The current investigation and the experimental approach in controlling the phase suggest that turbulent transition can be controlled with the phase modulation of a major instability mode (here the subharmonic mode).

3.4. Discussion on resonance and anti-resonance

Resonance and anti-resonance phenomenon of the secondary instability (subharmonic mode) are further discussed here with the evolution of the phase difference between the fundamental and subharmonic modes. A total of 44 initial phase differences are simulated in the current PSE (see figure 4b), and the evolution of four selected phases $\Delta\phi_{in} = 15, 40, 105$ and 130° are shown in figure 9. The Floquet analysis is also compared with the PSE data because the Floquet analysis provides the phase-locked condition. Initial phase differences near the Floquet $\Delta\phi_{in}$ follow the Floquet phase evolution in the current PSE with a slight deviation at the beginning. As the initial phase difference deviates further from the resonant phase, the phase evolution requires more distance to approach the Floquet phase difference. It takes approximately $\Delta R = 200$ for the anti-resonant condition of the initial phase $\Delta\phi_{in} = 15^\circ$ to catch up with the subharmonic resonance,

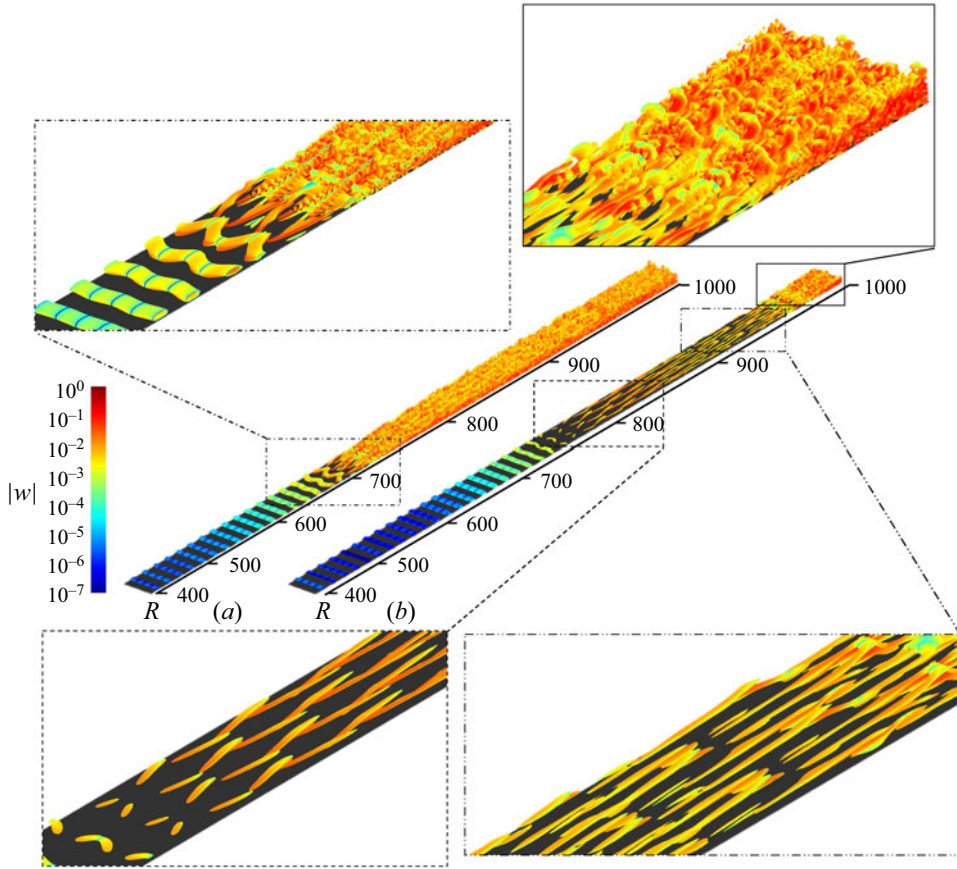


Figure 7. Vortical structures in the LES computations with the resonant phase $\Delta\phi_{in} = 105^\circ$ (a) and the anti-resonant phase $\Delta\phi_{in} = 10^\circ$ (b). The iso-surface of the Q-criteria $Q = 3\tilde{U}_\infty^2/\bar{x}^2$ ($R = 400$) is used for the visualisation with the colour contour of the magnitude of the spanwise velocity $|w|$.

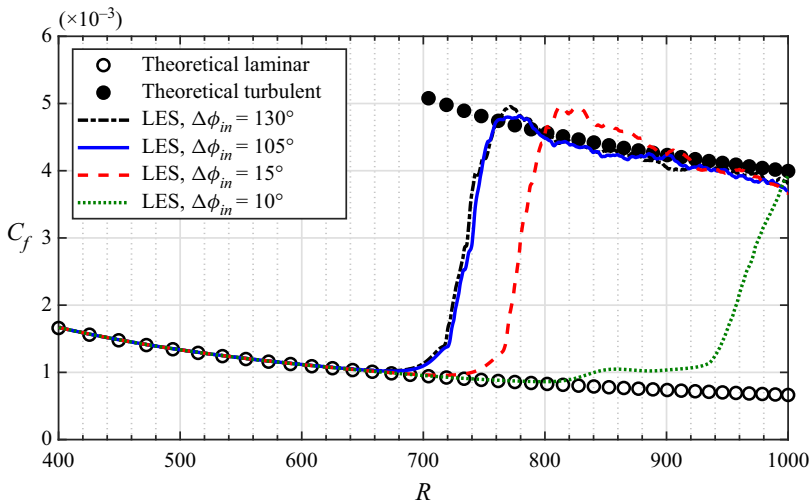


Figure 8. Skin friction C_f in the current LES computations with various initial phase difference $\Delta\phi_{in}$ compared with theoretical data.

Effects of phase difference on boundary-layer transition

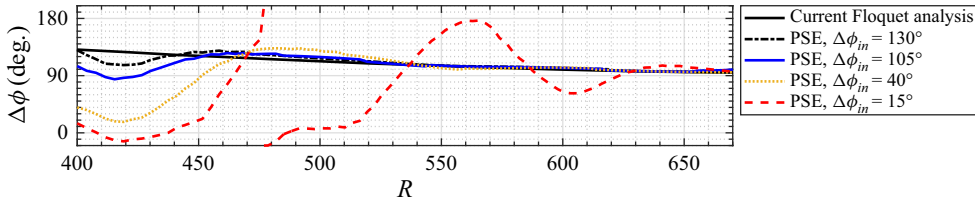


Figure 9. Evolution of the phase difference between the fundamental 2-D and subharmonic 3-D modes in the current PSE and Floquet analysis with the four selected initial phases.

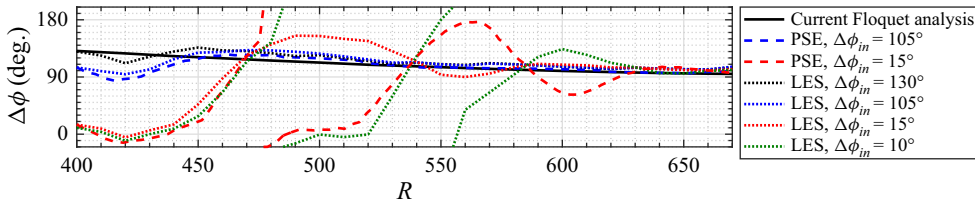


Figure 10. Evolution of the phase difference between the fundamental 2-D and subharmonic 3-D modes in the current PSE, LES and Floquet analysis with the four selected initial phases.

which is consistent with the exponential growth of the subharmonic mode after $R \simeq 600$ in figure 4(a).

The phase evolution is also confirmed in the LES computations as shown in figure 10. Two resonant initial phase differences ($\Delta\phi_{in} = 105$ and 130°) and two anti-resonant phase differences ($\Delta\phi_{in} = 10$ and 15°) are selected for the LES data sets. Two selected PSE cases are also plotted for comparison. In the resonant conditions, the phase difference quickly converges to the Floquet phase difference. For the anti-resonant condition of $\Delta\phi_{in} = 10^\circ$ in LES, the phase difference approaches the Floquet data after $R = 600$, similarly observed in the PSE anti-resonance of $\Delta\phi_{in} = 15^\circ$. Note that the anti-resonance phenomena is sensitive to detailed numerical solution, so the difference of 5° seems acceptable, as discussed in § 3.3.

In both PSE and LES, regardless of the initial phase differences, $\Delta\phi$ converges to the resonant phase difference approximately 90° in the downstream. Similar evolution of the phase difference between two major instability modes (normally primary and secondary instability modes) has been observed in experiments (Borodulin *et al.* 2002; Würz *et al.* 2012a). Borodulin *et al.* (2002) noticed a similar convergence to 90° for the phase difference in an adverse-pressure-gradient boundary-layer flow on a flat plate (see Borodulin *et al.* 2002, figure 26). The narrow phase range for the anti-resonant condition was also observed in the experiment (see Borodulin *et al.* 2002, figure 25). Würz *et al.* (2012a) also measured the evolution of the phase difference starting from the anti-resonance to the resonance in a boundary layer on a laminar airfoil.

The mechanism of the phase evolution is related to the phase synchronisation of the subharmonic mode for the parametric resonance. A simple dynamic system expressed in Mathieu's equation, which describes a sinusoidal parametric excitation (Kovacic, Rand & Sah 2018), requires the phase synchronisation for the parametric resonance. An initial phase shift of the subharmonic mode eventually approaches to the phase synchronisation (Kim 2020), and the transient interval is associated with the initial phase shift. Kim (2020) obtained two opposite local solutions, one for exponential growth (resonance) and another for exponential damping (anti-resonance) in Mathieu's equation. An arbitrary

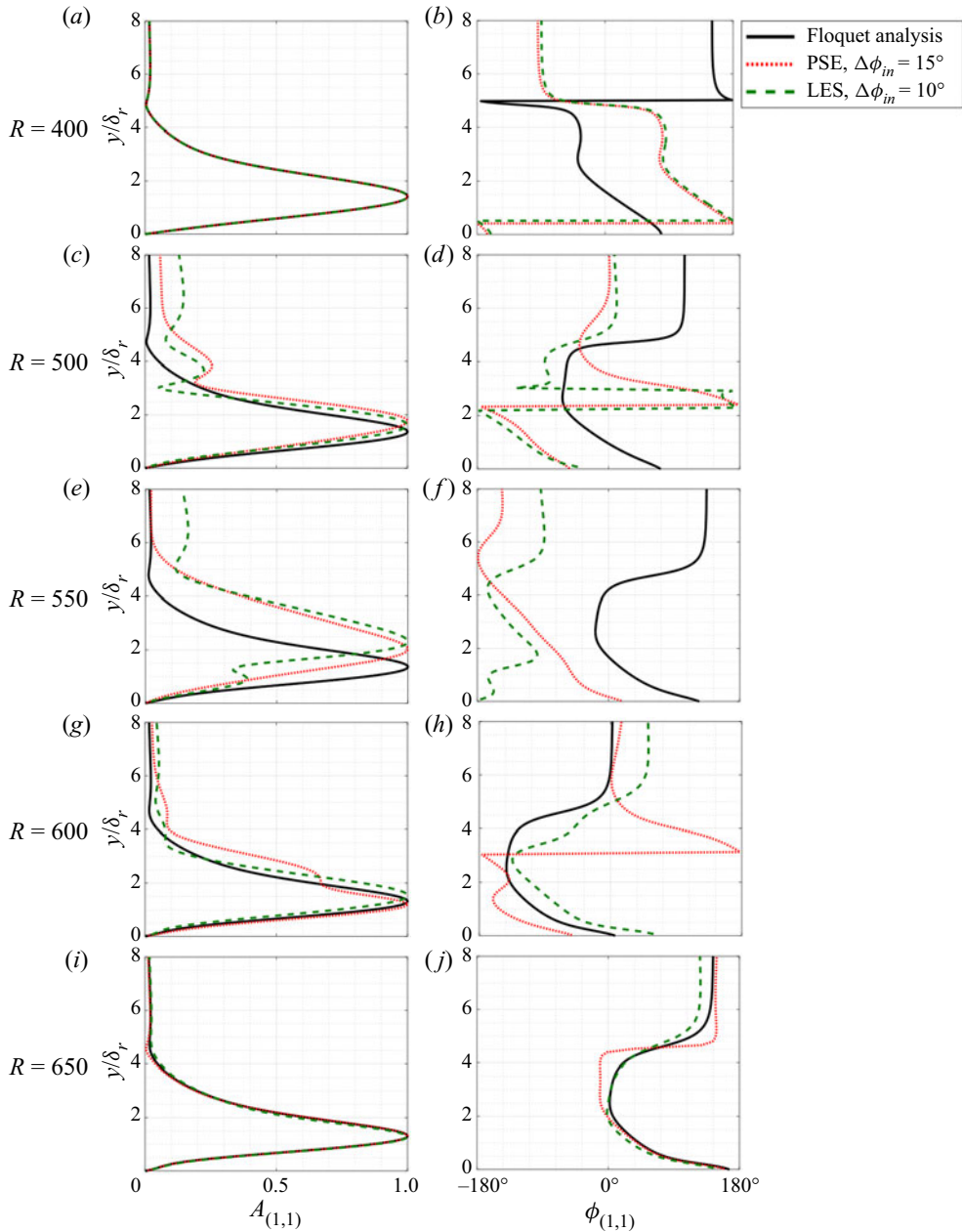


Figure 11. Comparison of the modal shapes between the current Floquet analysis and PSE computations for anti-resonant conditions. The amplitude is scaled by its own maximum in each case.

initial condition can be decomposed into these two solutions. Obviously, the resonant component grows exponentially and dominates the subharmonic mode, which results in the phase evolution to the phase synchronisation. A similar discussion can be found in an experimental observation of phase evolution (Borodulin *et al.* 2002; Würz *et al.* 2012a).

Initial phase differences in the anti-resonant condition change the mode shape of the subharmonic mode during the transient region towards the phase synchronisation,

as shown in [figure 11](#). In the initial damping region $400 < R < 600$ of the anti-resonant condition, the subharmonic mode undergoes a severe distortion. As the phase difference approaches to the resonant phase predicted by the Floquet analysis at approximately $R = 600$ (i.e. the phase synchronisation), the subharmonic mode eventually recovers to the resonant shape. In contrast, the resonant condition maintains the initial resonant modal shape as shown in [figure 12](#). Note that the resonant condition is insensitive to the phase shift if the phase difference is in the wide range of $60 \lesssim \Delta\phi_{in} \lesssim 150^\circ$, which has been discussed with [figure 4\(b\)](#).

The evolution of the temporal oscillation of the fundamental and subharmonic modes shown in [figure 13](#) indicates the variation of the phase speed depending on the initial phase difference $\Delta\phi_{in}$. The subharmonic oscillation relative to the fundamental oscillation at $y_{(1,1),max}$ is plotted in [figure 13](#). The subharmonic mode, initially resonating with the fundamental mode, yields almost no variation in the temporal oscillation, which indicates that the phase speed is synchronised in the overall transition process. In contrast, the anti-resonant initial condition causes the temporal oscillation of the subharmonic mode to continuously shift in the phase until $R \simeq 630$. After $R > 630$, the phase speed of the subharmonic mode remains the same and is synchronised with the phase speed of the fundamental mode, i.e. in the phase synchronisation condition.

3.5. *Effect of amplitude on anti-resonance and phase synchronisation*

It is well known that the subharmonic resonance is affected by major parameters including the amplitude of the fundamental mode. However, amplitude effects on the evolution of the subharmonic mode, initially in the anti-resonant condition, have not been thoroughly investigated. Particularly, the effect on the phase synchronisation location has not been studied. As a consequence, additional computations with various amplitudes of the fundamental and subharmonic modes are carried out here for the assessment of the amplitude effect on anti-resonance and phase synchronisation. The additional computations are listed in [table 2](#). Due to the computational cost, LES is used for selected cases.

The effect of the initial subharmonic amplitude on anti-resonance is shown in [figure 14\(a\)](#). The amplitude evolution of the subharmonic mode is vertically shifted with the initial amplitude of the subharmonic mode itself (see [figure 14\(a\)](#)). The phase synchronisation location at approximately $R = 630$ remains the same in the LES and PSE computations (see [figure 14\(b\)](#)), regardless of the initial amplitude of the subharmonic mode in the current study. The subharmonic initial amplitude is sufficiently small compared with the fundamental that the subharmonic amplitude effect on anti-resonance and phase synchronisation is negligible. The growth rates after the phase synchronisation shown in [figure 14\(a\)](#) also confirm that the subharmonic resonance is not significantly affected by the subharmonic amplitude itself. The PSE data show a slight different evolution of the phase difference at approximately $R = 600$ compared with the LES data, as already discussed in § 3.3 with [figure 10](#).

The effect of the initial fundamental amplitude on anti-resonance is shown in [figure 15](#). The higher initial fundamental amplitude induces larger growth of the subharmonic mode (see [figure 15\(a\)](#)) and earlier phase synchronisation (see [figure 15\(b\)](#)). The subharmonic amplitude quickly grows double exponentially with the highest fundamental amplitude $2 \times A_{(2,0)}$ owing to the strong driving force of the large fundamental mode. The phase synchronisation occurs at approximately $R = 500$ with the highest fundamental amplitude in both LES and PSE. The subharmonic mode decays initially in all the cases in [figure 15](#)

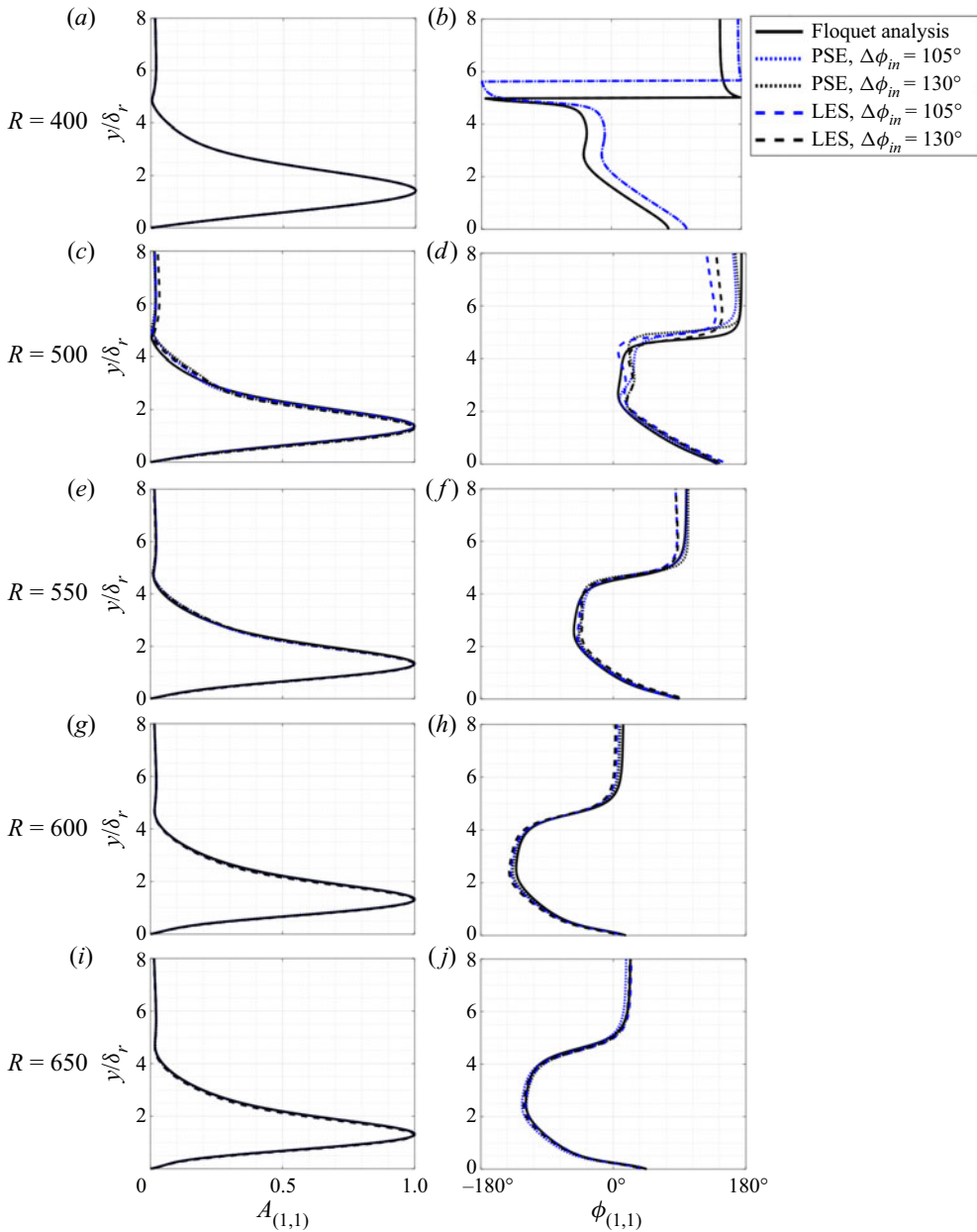


Figure 12. Comparison of the modal shapes between the current Floquet analysis and PSE computations for resonant conditions. The amplitude is scaled by its own maximum in each case.

because of the anti-resonant condition. The decaying rate also depends on the initial amplitude of the fundamental mode, the higher fundamental amplitude leads to more reduction at approximately $R = 450$ in the subharmonic amplitude. The low amplitude of the fundamental mode in the case of $0.1 \times A_{(2,0)}(x_0)$ cannot trigger the subharmonic resonance, and both the fundamental and subharmonic modes decay at approximately $R = 620$ in the current PSE computation.

Effects of phase difference on boundary-layer transition

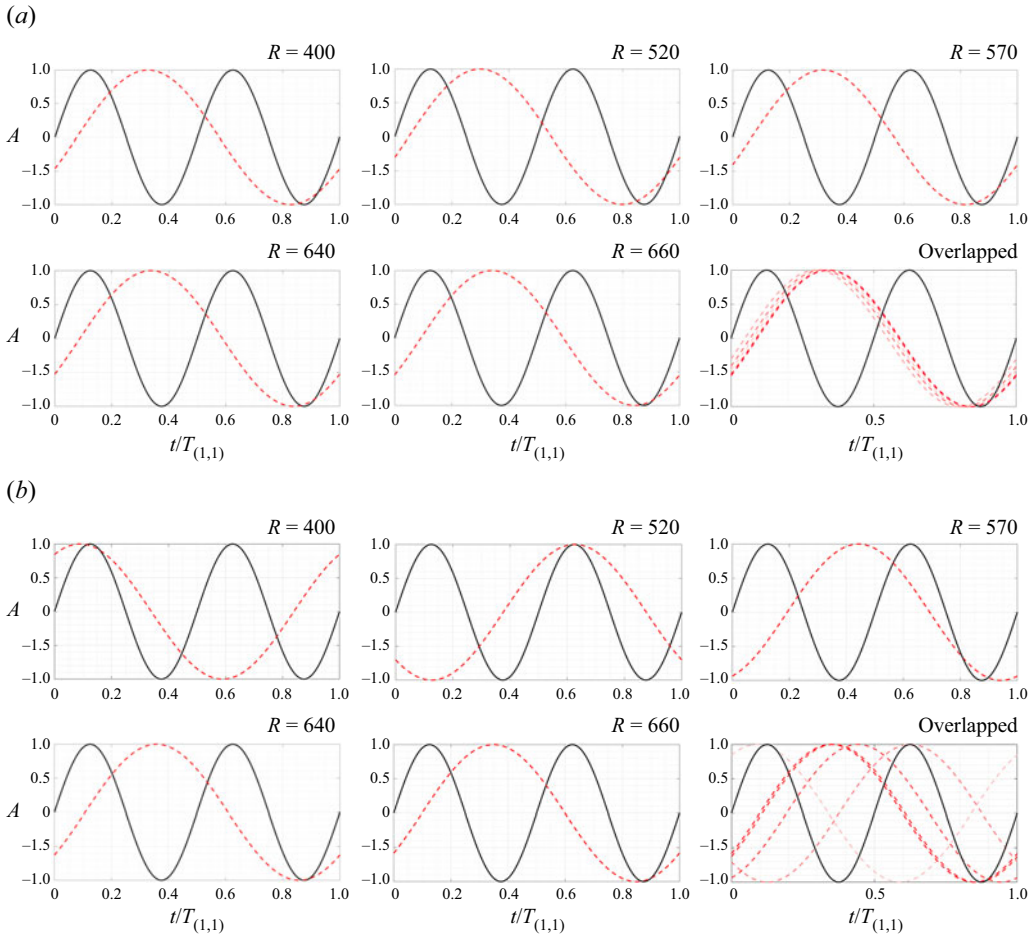


Figure 13. Temporal oscillation of the fundamental and subharmonic modes during the period of the subharmonic mode $T_{(1,1)}$ at selected streamwise locations. The LES computations are used: red dashed line, $(1, 1)$; black solid line, $(2, 0)$. Each mode amplitude is scaled with its own maximum. (a) Initially resonant condition, $\Delta\phi_{in} = 105^\circ$. (b) Initially anti-resonant condition, $\Delta\phi_{in} = 10^\circ$.

Initial amplitudes for each case	PSE	LES
$10 \times A_{(1,1)}(x_0)$ and $A_{(2,0)}(x_0)$	○	○
$0.1 \times A_{(1,1)}(x_0)$ and $A_{(2,0)}(x_0)$	○	○
$A_{(1,1)}(x_0)$ and $2 \times A_{(2,0)}(x_0)$	○	○
$A_{(1,1)}(x_0)$ and $0.5 \times A_{(2,0)}(x_0)$	○	—
$A_{(1,1)}(x_0)$ and $0.1 \times A_{(2,0)}(x_0)$	○	—

Table 2. Computational cases with various initial amplitudes for the current study of amplitude effects on anti-resonance and phase synchronisation.

Interestingly, the case of $A_{(2,0)}$ yields phase synchronisation much delayed compared with the case of $0.5 \times A_{(2,0)}$. This is presumably associated with the large distortion of the subharmonic mode in the case of $A_{(2,0)}$ compared with the case of $0.5 \times A_{(2,0)}$ in the region of $450 < R < 600$ as shown in figure 16. It is speculated that the large distortion of

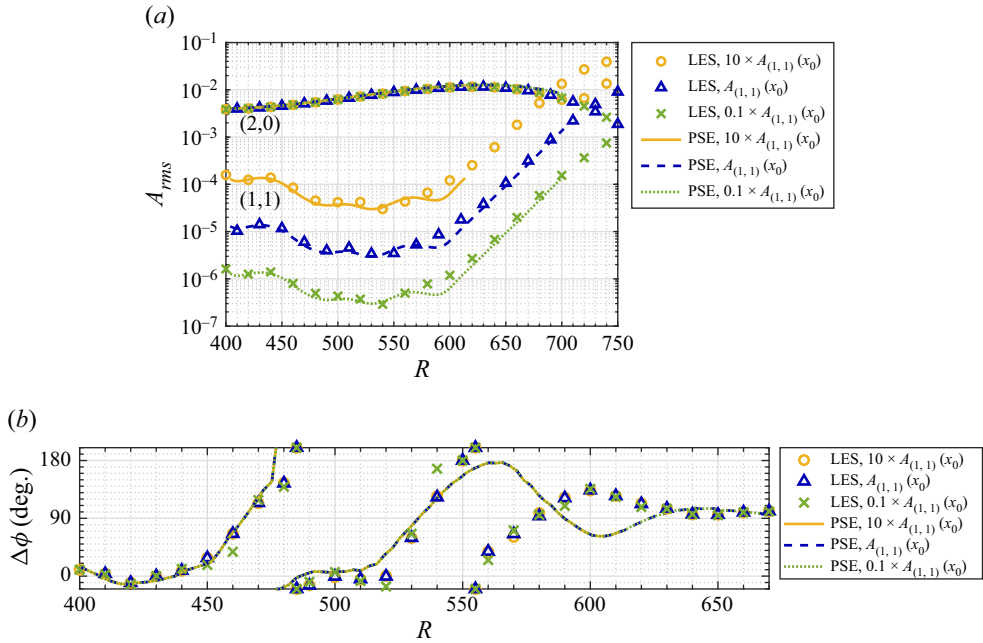


Figure 14. LES and PSE computations with various initial amplitudes of the subharmonic mode $A_{(1,1)}(x_0)$ and anti-resonant initial phase differences. (a) Amplitude growth. (b) Evolution of phase difference.

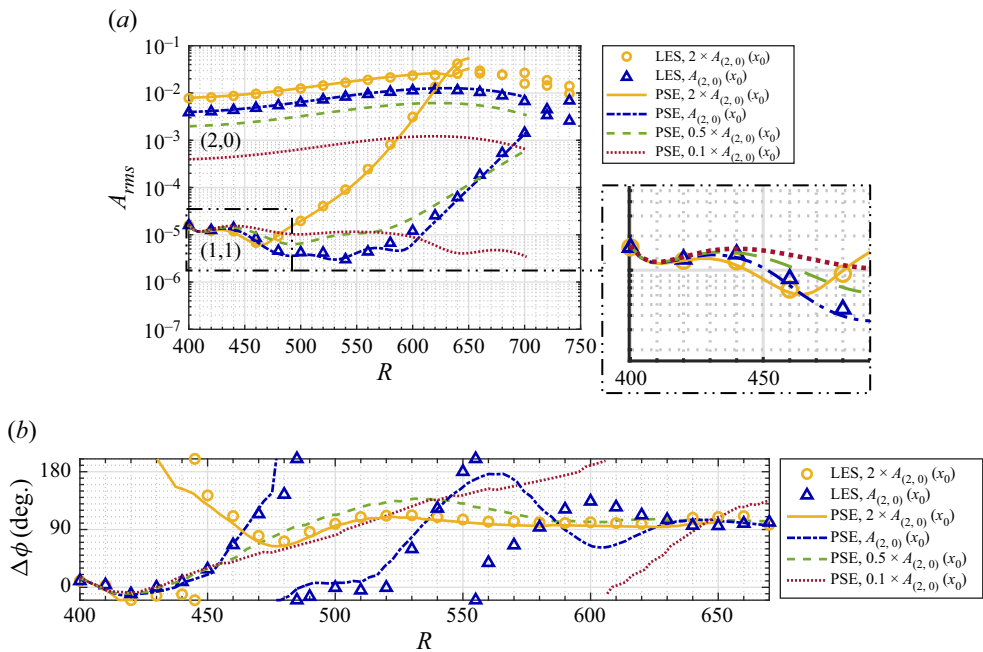


Figure 15. LES and PSE computations with various initial amplitudes of the fundamental mode $A_{(2,0)}(x_0)$ and anti-resonant initial phase differences. (a) Amplitude growth. (b) Evolution of phase difference.

Effects of phase difference on boundary-layer transition

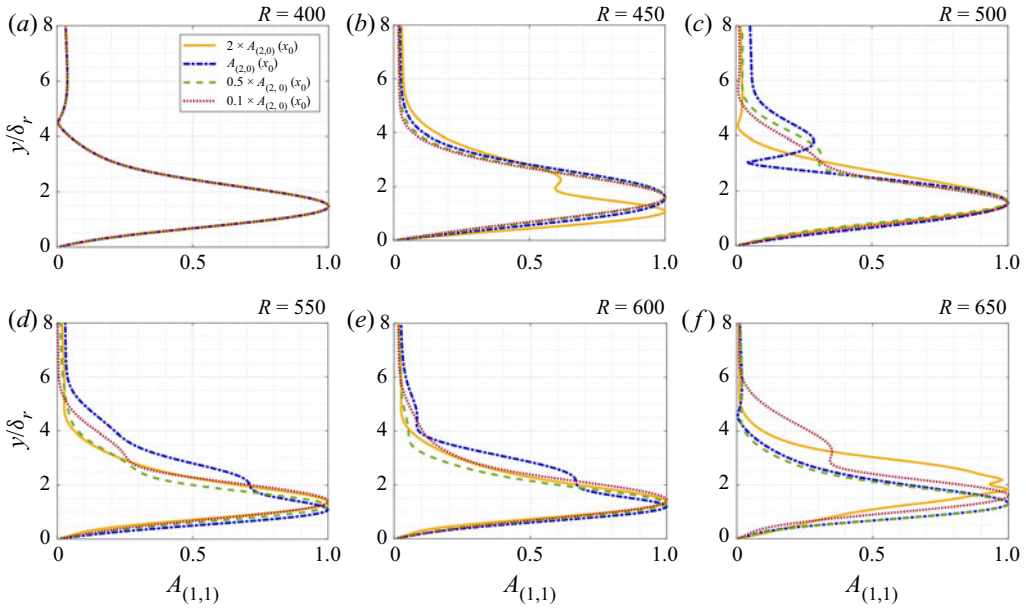


Figure 16. Evolution of the subharmonic mode shape from the PSE computations with various initial amplitudes of the fundamental mode and anti-resonant initial phase difference. The amplitude is scaled by its own maximum in each case.

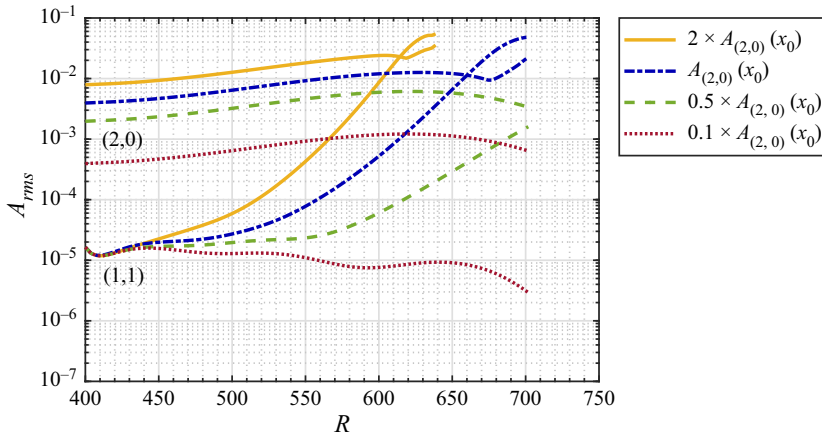


Figure 17. PSE computations with various initial amplitudes of the fundamental mode and initially resonant phase difference.

the mode shape in the case of $A_{(2,0)}$ causes a greater distance to recover, which may cause the amplitude to dwindle until approximately $R = 600$ in figure 15(a).

The effect of the initial fundamental amplitude on the subharmonic resonance with the resonating initial condition is shown in figure 17. Note that the PSE with the highest initial amplitude ends earlier compared with the other cases because these major modes (2, 0) and (1, 1) are already at 1% of the free-stream velocity. The behaviour of the subharmonic mode affected by the fundamental amplitude is expected owing to the nature of the parametric resonance.

4. Conclusions

A thorough investigation has been conducted into the phase effect on the growth of a secondary instability in the early nonlinear transition region and its final impact on the turbulent transition location. Numerical methods with various levels of fidelity were systematically explored. The fundamental 2-D TS wave and subharmonic oblique wave were chosen for the primary and corresponding secondary instability, respectively.

Floquet analysis provides a resonating subharmonic mode for a given basic flow composed of steady laminar flow and the fundamental TS wave with the assumption of locally parallel basic flow and a one-way nonlinear effect from the basic flow to the subharmonic mode. The current Floquet analysis was validated against the pioneering analysis of Herbert *et al.* (1987) and the experimental data of Kachanov & Levchenko (1984) for the same flow condition. In such an early nonlinear stage in the laminar region, local Floquet analysis is efficient for obtaining the subharmonic mode resonating to the given basic flow.

Because the current Floquet analysis is limited to a resonating condition, PSE was used for the new parametric study on the effect of the phase on the subharmonic resonance. A total of 44 phase differences between the fundamental and subharmonic modes were studied by shifting the subharmonic phase with respect to the given fundamental TS wave while maintaining the initial amplitude of both the waves at the PSE inlet. The current PSE indicates that the subharmonic resonance is insensitive to the phase difference as long as the phase shift is less than approximately 45° from the most resonating phase condition. In contrast to the resonance phenomena, the anti-resonant condition damps the subharmonic growth at the beginning and delays the resonance significantly. The anti-resonant condition is sensitive to the phase difference here, only 5° difference can cause the subharmonic amplitude to vary with a factor of 10 downstream near $R = 600$ in the current simulation.

To carry through complete simulations to fully turbulent flows, LES was used for nine selected phase differences (two in the resonant condition and seven near the anti-resonance). The current LES provides the subharmonic resonance observed in the Floquet and PSE analyses in the early nonlinear region, indicating that LES is essentially DNS before highly nonlinear interactions occur. Comparisons between PSE and LES were also made in less-resonating conditions, and the comparison is acceptable even in the anti-resonant condition. A slight difference, approximately 5° in the anti-resonant phase between PSE and LES, is presumably related to the sensitive nature of the anti-resonance phenomena to detailed flow solutions. The turbulent transition is significantly delayed when the subharmonic resonance is mostly suppressed in the anti-resonant condition. The variation of the transitional Reynolds number can be drastic as $\Delta Re_{x,tr} \simeq 4.4 \times 10^5$, when the phase shifts from the resonant to anti-resonant condition. Although a realistic transition control technique with the phase modulation requires further investigation, a few experimental approaches with an array of microphones in Borodulin *et al.* (2002) and Würz *et al.* (2012a) indicate the control potential.

The resonance and anti-resonance phenomenon were further discussed with the evolution of the phase difference. In a resonating condition, the phase difference quickly follows the phase evolution of the Floquet analysis even though the initial phase is moderately deviated from the Floquet phase. In the anti-resonant condition, it takes a significant distance for the subharmonic mode to catch up on the phase evolution of the Floquet analysis. The mechanism of the phase evolution is associated with the phase synchronisation of the subharmonic mode for the parametric resonance. A similar phase evolution towards the resonant phase has been noticed even in a simple nonlinear dynamic system governed by Mathieu's equation (Kim 2020) and experimental measurements

under non-zero pressure gradients (Borodulin *et al.* 2002; Würz *et al.* 2012a). In the anti-resonant condition, the subharmonic mode shape deviates from the resonating shape at the beginning as the subharmonic amplitude damps, and then it returns to the resonating shape as phase synchronisation occurs.

Because an anti-resonant condition can lead to a significant transition delay, it was imperative to investigate parameters affecting the anti-resonance. Previous studies focused on the parametric resonance of the subharmonic mode in resonant conditions, not anti-resonance. In the current study, amplitude effects on anti-resonance and phase synchronisation were investigated using both the PSE and LES computations. The initial amplitude of the subharmonic mode does not significantly change the evolution of the subharmonic mode in anti-resonant conditions, as long as the subharmonic amplitude is sufficiently small enough not to interfere the one-way influence of the fundamental to subharmonic modes. In contrast, the initial amplitude of the fundamental mode strongly affects the evolution of the subharmonic mode even in anti-resonance and eventually the phase synchronisation location for the subharmonic resonance, the higher fundamental amplitude causes earlier recovery of the subharmonic mode from a desynchronised to a synchronised phase.

Funding. This work was supported by the National Research Foundation of Korea (NRF) grant funded by the Korea government (MSIT) (Project No. NRF-2021R1A2C1006193) and Space Core Technology Development Program (No. NRF-2017M1A3A3A02016810). Computational resources were supported by the KISTI National Supercomputing Center (Project Numbers: KSC-2020-CRE-0057 and KSC-2018-CRE-0113) with technical support.

Declaration of interests. The authors report no conflict of interest.

Author ORCIDs.

 Solkeun Jee <https://orcid.org/0000-0001-7765-6065>.

Appendix A. Primary and secondary instability (Floquet) analyses

Equations for the primary instability are obtained for the fundamental TS wave, substituting (2.3) and (2.4) into (2.2), and eliminating non-parallel terms, as provided in the Appendix of El-Hady (1988),

$$\dot{\zeta}_1 = \zeta_2, \tag{A1a}$$

$$\dot{\zeta}_2 = \left\{ \alpha^2 + iR_o(\alpha U_L - \omega) \right\} \zeta_1 + R_o \dot{U}_L \zeta_3 + i\alpha R_o \zeta_4, \tag{A1b}$$

$$\dot{\zeta}_3 = -i\alpha \zeta_1, \tag{A1c}$$

$$\dot{\zeta}_4 = -\frac{i\alpha \zeta_2}{R_o} - \left\{ \frac{\alpha^2}{R_o} + i(\alpha U_L - \omega) \right\} \zeta_3, \tag{A1d}$$

where $\dot{\zeta} = d\zeta/dy$. The set of the first-order differential equations with the boundary conditions given in (A2) yields an eigenvalue problem for the eigenvalue α and the eigenfunctions ζ .

$$\zeta_1 = \zeta_3 = 0 \quad \text{at } y = 0, \tag{A2a}$$

$$\zeta_1, \zeta_3 \rightarrow 0 \quad \text{as } y \rightarrow \infty. \tag{A2b}$$

Substituting (2.5) and (2.6) for the basic flow and the disturbance in (2.2), respectively, with $\{u, v, w, p\}$ being replaced with $\{u, v, w, p\}_{1/2}$, and equating the coefficients of

$\exp(\pm i\theta/2)$ on both sides, the following set of first-order ordinary differential equations for the secondary instability is obtained.

$$\dot{\eta}_1 = \eta_2, \tag{A3a}$$

$$\begin{aligned} \dot{\eta}_2 = & \Gamma\eta_1 + R_o\dot{U}_L\eta_3 + R_o(\gamma + i\alpha_{1/2})\eta_4 \\ & + AR_o(\gamma + i\alpha_{1/2})\zeta_1\eta_7 + AR_o\zeta_3\eta_8 + AR_o\zeta_2\eta_9, \end{aligned} \tag{A3b}$$

$$\dot{\eta}_3 = -(\gamma + i\alpha_{1/2})\eta_1 - \beta\eta_5, \tag{A3c}$$

$$\begin{aligned} \dot{\eta}_4 = & -\frac{1}{R_o}[(\gamma + i\alpha_{1/2})\eta_2 + \Gamma\eta_3 + \beta\eta_6] \\ & + A(\gamma - i3\alpha_{1/2})\zeta_3\eta_7 - A[\gamma - i(\alpha + \alpha_{1/2})]\zeta_1\eta_9 + A\beta\zeta_3\eta_{11}, \end{aligned} \tag{A3d}$$

$$\dot{\eta}_5 = \eta_6, \tag{A3e}$$

$$\dot{\eta}_6 = -\beta R_o\eta_4 + \Gamma\eta_5 + AR_o(\gamma - i\alpha_{1/2})\zeta_1\eta_{11} + AR_o\zeta_3\eta_{12}, \tag{A3f}$$

$$\dot{\eta}_7 = \eta_8, \tag{A3g}$$

$$\begin{aligned} \dot{\eta}_8 = & \Gamma\eta_7 + R_o\dot{U}_L\eta_9 + R_o(\gamma - i\alpha_{1/2})\eta_{10} \\ & + AR_o(\gamma - i\alpha_{1/2})\zeta_1^*\eta_1 + AR_o\zeta_3^*\eta_2 + AR_o\zeta_2^*\eta_3, \end{aligned} \tag{A3h}$$

$$\dot{\eta}_9 = -(\gamma - i\alpha_{1/2})\eta_7 - \beta\eta_{11}, \tag{A3i}$$

$$\begin{aligned} \dot{\eta}_{10} = & -\frac{1}{R_o}[(\gamma - i\alpha_{1/2})\eta_8 + \Gamma^*\eta_9 + \beta\eta_{11}] \\ & + A(\gamma + i3\alpha_{1/2})\zeta_3^*\eta_1 - A[\gamma + i(\alpha^* + \alpha_{1/2})]\zeta_1^*\eta_3 + A\beta\zeta_3^*\eta_5, \end{aligned} \tag{A3j}$$

$$\dot{\eta}_{11} = \eta_{12}, \tag{A3k}$$

$$\dot{\eta}_{12} = -\beta R_o\eta_{10} + \Gamma^*\eta_{11} + AR_o(\gamma + i\alpha_{1/2})\zeta_1^*\eta_5 + AR_o\zeta_3^*\eta_6, \tag{A3l}$$

where $\Gamma = \alpha_{1/2}^2 + \beta^2 - \gamma^2 - 2i\alpha_{1/2}\gamma + R_o[\gamma U_L + i(\alpha_{1/2}U_L - \omega_{1/2})]$ and β is the spanwise wavenumber for the subharmonic wave. Note that the presence of the fundamental TS wave in the basic flow provides the nonlinear interaction between the fundamental and subharmonic modes through all the terms including U and V in (2.2) (even the square bracket terms). The nonlinear interaction is one-way in the current analysis because only the subharmonic oblique wave is influenced by the fundamental TS wave, not vice versa. In the derivation from (2.2) to (A3), higher subharmonic modes such as $\exp(i3\theta/2)$ are ignored.

Note that the current formulation in (2.6) is an extended version of Nayfeh & Masad (1990, (33)) and El-Hady (1988, (14)) in order to cooperate the complex exponent γ later, whereas the real γ is assumed in Nayfeh & Masad (1990) and El-Hady (1988). Although the current Floquet analysis is able to handle the complex γ , the subharmonic oblique wave perfectly synchronised with the fundamental TS wave, i.e. the real γ , is of interest here. The physical meaning of the function η is given in table 3 where γ is real.

The set of 12 differential equations (A3) with boundary conditions given in (A4) yields an eigenvalue problem for the eigenvalue γ and the eigenfunction η ,

$$\eta_1 = \eta_3 = \eta_5 = \eta_7 = \eta_9 = \eta_{11} = 0, \quad \text{at } y = 0, \tag{A4a}$$

$$\eta_1, \eta_3, \eta_5, \eta_7, \eta_9, \eta_{11} \rightarrow 0, \quad \text{as } y \rightarrow \infty. \tag{A4b}$$

The Blasius solution is used for the laminar flow $U_L(y)$. Although the Blasius solution is not strictly parallel (i.e. $V \neq 0$ and $\partial U_L/\partial x \neq 0$), the assumption of locally parallel flow

Function	Physical Meaning	Function	When $\gamma = \text{Re}(\gamma)$
η_1	modal shape of $u_{1/2}$	η_7	η_1^*
η_2	modal shape of $\dot{u}_{1/2}$	η_8	η_2^*
η_3	modal shape of $v_{1/2}$	η_9	η_3^*
η_4	modal shape of $p_{1/2}$	η_{10}	η_4^*
η_5	modal shape of $w_{1/2}$	η_{11}	η_5^*
η_6	modal shape of $\dot{w}_{1/2}$	η_{12}	η_6^*

Table 3. Physical meaning of function η for indices 1–6 and the relevant additional function when γ is real.

is used for the analysis of both the primary instability (A1) and the secondary subharmonic instability (A3), following the previous approach in Herbert (1984), Herbert *et al.* (1987), Nayfeh & Masad (1990) and El-Hady (1988).

The total number of the grid points is 512 in the wall-normal distance of $200\tilde{\delta}_r$, with approximately 300 points inside the boundary-layer thickness $5\tilde{\delta}_r$, and the first wall-normal grid size is $7 \times 10^{-3}\tilde{\delta}_r$. The current wall-normal mesh points are obtained using the mapping from a semi-infinite to a finite domain suggested in Schmid & Henningson (2001, Appendix A.4) as described in (A5).

$$\left. \begin{aligned} y_j &= c_1 \frac{1 + h_j}{c_2 - h_j}, \quad h_j = \frac{2j - N}{N}, \quad j = 0, 1, \dots, N, \quad N = 512, \\ y_0 &= 0, \quad y_{N/2} = \frac{c_1}{c_2} = 3.5, \quad y_N = \frac{c_1}{c_2 - 1} = 200, \quad c_1 = \frac{700}{193}, \quad c_2 = \frac{196.5}{193} \end{aligned} \right\} \quad (\text{A5})$$

Using the Matlab built-in function *polyeig*, the eigenvalue problem with (A1) and (A2) is solved for the 2-D TS wave. The same function is used for the Floquet analysis (A3) with the boundary condition (A4) to obtain the subharmonic characteristic exponent γ along with the eigenfunctions η . The function *polyeig* solves the polynomial eigenvalue problem $(\mathbf{A}_0 + \mathbf{A}_1\lambda + \dots + \mathbf{A}_n\lambda^n)\mathbf{b} = 0$ where λ is the eigenvalue, \mathbf{b} is the eigenvector and \mathbf{A} is the given square coefficient matrix (see Higham & Higham 2016, Ch. 9.8). For the current quadratic eigenvalue problems, $n = 2$.

REFERENCES

BERTOLOTTI, F.P., HERBERT, T. & SPALART, P.R. 1992 Linear and nonlinear stability of the Blasius boundary layer. *J. Fluid Mech.* **242**, 441–474.
 BORODULIN, V.I., KACHANOV, Y.S. & KOPTSEV, D.B. 2002 Experimental study of resonant interactions of instability waves in a self-similar boundary layer with an adverse pressure gradient: I. Tuned resonances. *J. Turbul.* **3**, N62.
 BORODULIN, V.I., KACHANOV, Y.S. & ROSCHEKTAYEV, A.P. 2011 Experimental detection of deterministic turbulence. *J. Turbul.* **12**, N23.
 CHANG, C.-L., MALIK, M.R., ERLEBACHER, G. & HUSSAINI, M.Y. 1993 Linear and nonlinear PSE for compressible boundary layers. Technical Report NASA-CR-191537.
 CORKE, T.C. & MANGANO, R.A. 1989 Resonant growth of three-dimensional modes in transitioning Blasius boundary layers. *J. Fluid Mech.* **209**, 93–150.
 CRAIK, A.D.D. 1971 Non-linear resonant instability in boundary layers. *J. Fluid Mech.* **50** (2), 393–413.
 DURBIN, P. & WU, X. 2007 Transition beneath vortical disturbances. *Annu. Rev. Fluid Mech.* **39** (1), 107–128.
 EL-HADY, N.M. 1988 Secondary subharmonic instability of boundary layers with pressure gradient and suction. Technical Report NASA-CR-4112.

- GAO, B., PARK, D. & PARK, S.O. 2011 Stability analysis of a boundary layer over a hump using parabolized stability equations. *Fluid Dyn. Res.* **43** (5), 055503.
- HERBERT, T. 1984 Analysis of the subharmonic route to transition in boundary layers. In *AIAA 22nd Aerospace Sciences Meeting*, January 09–12, Reno, NV. <https://arc.aiaa.org/doi/pdf/10.2514/6.1984-9>.
- HERBERT, T. 1988 Secondary instability of boundary layers. *Annu. Rev. Fluid Mech.* **20** (1), 487–526.
- HERBERT, T., BERTOLOTI, F.P. & SANTOS, G.R. 1987 Floquet analysis of secondary instability in shear flows. In *Stability of Time Dependent and Spatially Varying Flows* (ed. D.L. Dwoyer & M.Y. Hussaini), pp. 43–57. Springer.
- HIGHAM, D.J. & HIGHAM, N.J. 2016 *MATLAB Guide*, 3rd edn. SIAM. <https://epubs.siam.org/doi/pdf/10.1137/1.9781611974669.ch9>.
- ISSA, R.I. 1986 Solution of the implicitly discretised fluid flow equations by operator-splitting. *J. Comput. Phys.* **62** (1), 40–65.
- JEE, S., JOO, J. & LIN, R.-S. 2018 Toward cost-effective boundary layer transition computations with large-eddy simulation. *Trans. ASME J. Fluids Engng* **140** (11), 111201.
- JOSLIN, R.D., STRETT, C.L. & CHANG, C.-L. 1993 Spatial direct numerical simulation of boundary-layer transition mechanisms: validation of PSE theory. *Theor. Comput. Fluid Dyn.* **4** (6), 271–288.
- KACHANOV, Y.S. 1994 Physical mechanisms of laminar-boundary-layer transition. *Annu. Rev. Fluid Mech.* **26** (1), 411–482.
- KACHANOV, Y.S. & LEVCHENKO, V.Y. 1984 The resonant interaction of disturbances at laminar-turbulent transition in a boundary layer. *J. Fluid Mech.* **138**, 209–247.
- KIM, S. 2020 Effect of phase difference between instability modes on boundary layer transition. Master's thesis, Gwangju Institute of Science and Technology, Gwangju, Korea.
- KIM, M., LIM, J., KIM, S., JEE, S. & PARK, D. 2020 Assessment of the wall-adapting local eddy-viscosity model in transitional boundary layer. *Comput. Meth. Appl. Mech. Engng* **371**, 113287.
- KIM, M., LIM, J., KIM, S., JEE, S., PARK, J. & PARK, D. 2019 Large-eddy simulation with parabolized stability equations for turbulent transition using OpenFOAM. *Comput. Fluids* **189**, 108–117.
- KLEBANOFF, P.S., TIDSTROM, K.D. & SARGENT, L.M. 1962 The three-dimensional nature of boundary-layer instability. *J. Fluid Mech.* **12** (1), 1–34.
- KOVACIC, I., RAND, R. & SAH, S.M. 2018 Mathieu's equation and its generalizations: overview of stability charts and their features. *Appl. Mech. Rev.* **70** (2), 020802.
- LIM, J., KIM, M., KIM, S., JEE, S. & PARK, D. 2021 Cost-effective and high-fidelity method for turbulent transition in compressible boundary layer. *Aerosp. Sci. Technol.* **108**, 106367.
- MORKOVIN, M.V. 1969 On the many faces of transition. In *Viscous Drag Reduction* (ed. C. Sinclair Wells), pp. 1–31. Springer.
- NAYFEH, A.H. & MASAD, J.A. 1990 Recent advances in secondary instabilities in boundary layers. *Comput. Syst. Engng* **1** (2), 401–414.
- NICOUD, F. & DUCROS, F. 1999 Subgrid-scale stress modelling based on the square of the velocity gradient tensor. *Flow Turbul. Combust.* **62** (3), 183–200.
- PARK, D. & PARK, S.O. 2013 Linear and non-linear stability analysis of incompressible boundary layer over a two-dimensional hump. *Comput. Fluids* **73**, 80–96.
- PARK, D. & PARK, S.O. 2016 Study of effect of a smooth hump on hypersonic boundary layer instability. *Theor. Comput. Fluid Dyn.* **30** (6), 543–563.
- PARK, D., PARK, J., KIM, M., LIM, J., KIM, S. & JEE, S. 2021 Influence of initial phase on subharmonic resonance in an incompressible boundary layer. *Phys. Fluids* **33** (4), 044101.
- SARIC, W.S., REED, H.L. & WHITE, E.B. 2003 Stability and transition of three-dimensional boundary layers. *Annu. Rev. Fluid Mech.* **35** (1), 413–440.
- SAYADI, T., HAMMAN, C.W. & MOIN, P. 2013 Direct numerical simulation of complete H-type and K-type transitions with implications for the dynamics of turbulent boundary layers. *J. Fluid Mech.* **724**, 480–509.
- SCHMID, P.J. 2007 Nonmodal stability theory. *Annu. Rev. Fluid Mech.* **39** (1), 129–162.
- SCHMID, P.J. & HENNINGSON, D.S. 2001 *Stability and Transition in Shear Flows*. Springer.
- WÜRZ, W., SARTORIUS, D., KLOKER, M., BORODULIN, V.I., KACHANOV, Y.S. & SMORODSKY, B.V. 2012a Nonlinear instabilities of a non-self-similar boundary layer on an airfoil: experiments, DNS, and theory. *Eur. J. Mech. B/Fluids* **31**, 102–128.
- WÜRZ, W., SARTORIUS, D., KLOKER, M., BORODULIN, V.I., KACHANOV, Y.S. & SMORODSKY, B.V. 2012b Detuned resonances of Tollmien–Schlichting waves in an airfoil boundary layer: experiment, theory, and direct numerical simulation. *Phys. Fluids* **24** (9), 094103.
- WU, X. 2019 Nonlinear theories for shear flow instabilities: physical insights and practical implications. *Annu. Rev. Fluid Mech.* **51** (1), 451–485.
- XU, H., LOMBARD, J.W. & SHERWIN, S.J. 2017 Influence of localised smooth steps on the instability of a boundary layer. *J. Fluid Mech.* **817**, 138–170.