## A decision model for making decisions under epistemic uncertainty and its application to select materials

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#### Abstract

This study deals with both a decision model for making decisions under epistemic uncertainty and how to use it for selecting optimal materials under the same uncertainty. In particular, the proposed decision model employs a set of possibilistic objective functions defined by fuzzy numbers to handle a set of conflicting criteria. In addition, the model can calculate the compliance of a piece of decision-relevant (imprecise) information with a given objective function. Moreover, the model is capable to aggregate the calculated compliances for the sake of ranking a given set of alternatives against the set of conflicting criteria. The problem of selecting materials for making the body of a vehicle is considered as an example. In this problem, the indices for selecting the materials are unknown because the specifications regarding the vehicle body are not given. In addition, the data relevant to material properties entails a great deal of imprecision. The presented decision model can quantify the above-mentioned epistemic uncertainty in a lucid manner and generate a list of optimal materials.

Keywords: Decision Making; Engineering Design; Epistemic Uncertainty; Material Selection

## 1. INTRODUCTION

The notion of uncertainty has earned a great deal of attention from researchers belonging to various academic disciplines. Uncertainty is often understood (semantics) by classifying it into different categories, for example, aleatory uncertainty, epistemic uncertainty, irreducible uncertainty, reducible uncertainty, and inference uncertainty (Booker & Ross, 2011; Ross et al., 2013). In general, aleatory uncertainty refers to uncertainty due to random variability or stochastic processes. Epistemic uncertainty refers to uncertainty due to lack of knowledge or imprecision associated with the data and information. Irreducible uncertainty refers to uncertainty due to natural variability that can be quantified but cannot be reduced. Reducible uncertainty refers to uncertainty that can be reduced by acquiring more information. Inference uncertainty refers to predicting the future from the past, inferring the population behavior from a sample, and inferring the system behavior from its subsystems. To compute uncertainty in a formal manner (syntax), numerous theories have been developed, for example (to name a few), probability theory (Dempster, 1968, 2008), imprecise

298

probability theory (Walley, 1991, 2000), evidence theory (Shafer, 1976; Klir, 1990), possibility theory (Zadeh, 1978; Dubois & Prade, 1988), and random interval theory (Joslyn & Booker, 2004). In certain cases, the theories are based on different categories of uncertainty. For example, the probability theory deals mainly with the aleatory uncertainty, whereas the possibility theory deals mainly with the epistemic uncertainty. Certain theories can deal with multiple categories of uncertainty; for example, imprecise probability theory can deal with aleatory uncertainty and the epistemic uncertainty associated with the probabilities of events. Nevertheless, the uncertainty of a category can be interpreted in terms of the uncertainty of a different category (Klir, 1999; Dubois et al., 2004; Sharif Ullah & Shamsuzzaman, 2013). This means that the aleatory uncertainty, epistemic uncertainty, and any other uncertainty are different from each other in the sense of semantics, but all these uncertainties are somewhat same in the computational sense, and thereby, they can be integrated while developing systems for making decisions under uncertainty regardless of its category.

Similar to numerous academic communities, the engineering design community has also recognized the above-mentioned theorization (syntax) and categorization (semantics) of uncertainty, and developed numerous models and tools for making design decisions under uncertainty (Antonsson

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& Otto, 1995; Huang & Jiang, 2002; Nikolaidis et al., 2003, 2004; Youn & Choi, 2004; Gurnani & Lewis, 2005; Ullah, 2005a, 2005b; Ullah & Harib, 2008; Achiche & Ahmed-Kristensen, 2011; Sharif Ullah & Tamaki, 2011; Sharif Ullah et al., 2012; Matsumura & Haftka, 2013; Sharif Ullah & Shamsuzzaman 2013; Jiang et al., 2015; Rezaee et al., 2015). The methods and tools for dealing with uncertainty bring benefits for both approaches of engineering design, namely, solution-based design and problem-based design. In particular, the aleatory uncertainty-based measures (e.g., probability distributions and Bayesian inferences) are useful for the solution-based design, where the robustness or reliability of a given design solution is enhanced, without making any drastic changes in the geometric and material specifications of the given design solution. In the case of problem-based design, the geometric and material specifications are not clearly defined or known; rather, numerous problems are introduced and solved (determining customer needs, concept selection, and materials selection) by using the epistemic uncertainty-based measures (e.g., possibility measures and fuzzy numbers). The goal here is to transform a problembased design to a solution-based design. Some authors have integrated both aleatory uncertainty and epistemic uncertainty based measures to make the design decision-making process an even more robust and user-friendly process (e.g., see the works of Nikolaidis et al., 2003; Sharif Ullah & Tamaki, 2011; Sharif Ullah & Shamsuzzaman, 2013).

However, materials have been considered a key factor for managing the complexity while designing engineering products (McDowell et al., 2010). In addition, to achieve a sustainable future, the reduction and diversification of material usages (i.e., materials efficiency) are considered more effec-

tive than other measures (e.g., energy efficiency; Allwood et al., 2011; Ullah et al., 2013; Sharif Ullah et al., 2014). This is even more relevant for the products called vehicles. Mayyas et al. (Mayyas, Mayyas, et al., 2012; Mayyas, Qattawi, et al., 2012) and Poulikidou et al. (2015) have shown that the environmental impact of a vehicle depends heavily on the materials used in different parts of a vehicle. Therefore, if a designer has a clear idea about the appropriateness of a set of materials for making the parts of a vehicle at the early stage of the design process, then it would be easy for the designer to control the complexity of the subsequent design activities (McDowell et al., 2010; Omar, 2011). While assessing the appropriateness of a set of materials for making the parts of a vehicle, it is likely to be the case that the designer encounters a certain degree of epistemic uncertainty, as schematically illustrated in Figure 1.

As seen from Figure 1, if a designer prefers to select the optimal materials for making the body of a vehicle at a very early stage of the design process, he or she makes this decision without knowing the exact physical configuration of the body. As such, the material indices (Ashby, 2005, pp. 509– 512) to be used for comparing the materials are unknown. It is worth mentioning that the outline of a vehicle body depends on customer requirements (Sharif Ullah et al., 2016), and the outline is refined to get the final configuration using numerous engineering analyses where the materials must be known beforehand (Omar, 2011). In addition, we need to handle conflicting objectives while selecting materials. For example, if a designer prefers to maximize the structural integrity, then it may create a conflict with the environmental impact, as schematically illustrated in Figure 1. As such, how to define and manage these conflicting objectives is an



Fig. 1. A scenario of epistemic uncertainty.

important issue that must be tackled under the above-mentioned epistemic uncertainty (i.e., under the situation where the material indices are unknown). Moreover, the designer may encounter heterogeneous and imprecise decision-relevant information. For example, the information regarding some material attributes (or properties) can be given by some numerical ranges, information regarding some other materials properties can be given by probability distributions, and information regarding some other material properties can be given by fuzzy numbers, as schematically illustrated in Figure 1. It highly unlikely that all the materials-relevant information are available as crisp numerical values, as it is considered in other studies (Mayyas, Mayyas, et al., 2012; Mayyas, Qattawi, et al., 2012; Poulikidou et al., 2015).

Therefore, the goal of this study is to develop a novel decision model to select the best alternatives. The proposed model is designed to handle epistemic uncertainty and conflicting objectives simultaneously. In order to show the effectiveness of our model, we present a material selection case study, where we do not have complete information about alternative materials and design specifications. We have organized the remainder of this article as follows: Section 2 describes the mathematical entities that are needed for performing the required mathematical operations. Section 3 describes how to determine the numerical scales for defining the objective functions using some fuzzy numbers. Section 4 describes a procedure to induce a triangular fuzzy number from numerical data as it is useful in making decision when the probability distribution underlying a set of data is unknown or given. Section 5 describes the proposed decision model that consists of four major steps, namely, decision formulation, information gathering, compliance calculation, and aggregation. Section 6 presents the results and discusses their implications. In particular, Section 6 presents the results of a material selection problem using the proposed decision model where a large number of alloys of aluminum, magnesium, and titanium are evaluated. Finally, Section 7 provides the concluding remarks of this study and avenues for future research.

## 2. MATHEMATICAL SETTINGS

As mentioned in the previous section, one of the objectives of this study is to develop a novel decision model that helps make a decision under epistemic uncertainty. To achieve this, the decision model must be able to handle heterogeneous forms of information (Fig. 1). Now, as far as the uncertainty is concerned, there are two broad categories of information, namely, crisp information and granular information (Zadeh, 2005; Khozaimy et al., 2011). A piece of crisp information refers to a sharp numerical value (e.g., density is 10 kg/m<sup>3</sup>). The other category of information, granular information, refers to a set of numerical values and has numerous forms. The simplest form of granular information is called crisp granular information that refers to a numerical range (e.g., density is 10, 15] kg/m<sup>3</sup>). Probability granular information refers to a piece of information given by a probability distribution (e.g.,

density is normally distributed with mean 12 kg/m<sup>3</sup> and standard deviation 1 kg/m<sup>3</sup>). Fuzzy granular information refers to linguistically defined pieces of information that are often modeled by the fuzzy sets or numbers (e.g., density is "low" where low is defined by a triangular fuzzy number with core 12 kg/m<sup>3</sup> and support [8, 20] kg/m<sup>3</sup>). The terms called triangular fuzzy number, core, and support will be discussed in a moment. There are other complex forms of granular information, for example, fuzzy-probability granular information (density is most likely normally distributed with mean 10 kg/m<sup>3</sup> and standard deviation 1 kg/m<sup>3</sup>). If the probability distribution is unknown, one can model a piece of information using a fuzzy number or possibility distribution (Dubois et al., 2004; Sharif Ullah & Shamsuzzaman, 2013). This means that a fuzzy number is a general form of granular information that subsumes other forms of information.

Therefore, the proposed decision model must be able to model both crisp information and various forms of granular information. To formally compute the crisp information and various forms of granular information in an integrated manner, certain mathematical entities are needed. The remainder of this section describes the needed mathematical entities, namely, fuzzy numbers, triangular fuzzy numbers, maximization/minimization fuzzy numbers, and the degree of compliance.

### 2.1. Fuzzy number

A fuzzy number *F* is a function *F*:  $\Re \to [0, 1]$ , and it must be normal, compactly supported, convex, and upper semicontinuous (Zadeh, 1975; Dubois & Prade, 1978; Dijkman et al., 1983). It is normal means that there is, at least, one real number  $f_0$  for which  $F(f_0) = 1$ . It is compactly supported means that the set  $\{f \in \Re \mid F(f) > 0\}$  is bounded. It is convex means that if  $f_1 \le f_2 \le f_3$ , then min( $F(f_1), F(f_3)$ )  $\le F(f_2)$  for all  $f_1, f_2$ ,  $f_3 \in \Re$ . It is upper semicontinuous means that the set  $\{f \mid$  $F(f) \ge \alpha\}$  is closed for each  $\alpha \in [0, 1]$ . The points corresponding to F(.) = 1 constitute an interval called core. The closed interval  $S = [a, b] \in \Re$  beyond which the fuzzy number F(.) = 0 is called support. As such,  $F(a) = 0 \land F(a + \varepsilon) > 0$ and  $F(b - \varepsilon) > 0 \land F(b) = 0$ , where  $\varepsilon$  is a very small positive number.

### 2.2. Triangular fuzzy number

A triangular fuzzy number *T* is a fuzzy number that has a triangularly shaped membership function represented as follows:

$$T(x) = \max\left\{0, \min\left(\left(\frac{x-a}{c-a}\right), \left(\frac{b-x}{b-c}\right)\right)\right\}.$$
 (1)

In Eq. (1),  $x \in \Re$ ,  $a < c < b \in \Re$ . As such, the support of the triangular fuzzy number *T* is [a, b]. The core of *T* is *c* because T(x = c) = 1. The function (x-a)/(c-a) is called the left function and the function (b-x)/(b-c) is called the right function. The alpha-cuts of a triangular fuzzy number are the



Fig. 2. Examples of triangular, maximization, and minimization fuzzy numbers.

intervals  $[a + (c-a)\alpha, b - (b-c)\alpha]$ ,  $\forall \alpha \in (0, 1)$ . The concept of alpha-cut is useful when one needs an interval or a set of intervals from a given triangular fuzzy number. In this sense, all alpha-cuts belong to the support [a, b]; that is, the support is the largest alpha-cut. Figure 2a shows, for example, a triangular fuzzy number T where a = 10, b = 50, and c = 20.

### 2.3. Maximization fuzzy number

A maximization fuzzy number denoted as *MX* is also a fuzzy number. It defines a possibilistic objective function for maximizing a quantity. The expression of *MX* is as follows:

$$MX(x) = \begin{cases} \max\left\{0, \frac{x-a}{b-a}\right\} & x \le b\\ 0 & \text{otherwise} \end{cases}.$$
 (2)

As such, the core of MX is equal to b and the support is equal to [a, b]. MX linearly increases with the increase in xin the interval of its support. Figure 2b shows, for example, an MX where a = 10 and b = 30. As MX is for maximizing a quantity, setting its support [a, b] is a critical issue. This issue is described in Section 3.

### 2.4. Minimization fuzzy number

A minimization fuzzy number denoted as MI is also a fuzzy number. It defines a possibilistic objective function for minimizing a quantity. The expression of MI is as follows:

$$MX(x) = \begin{cases} \max\left\{0, \frac{b-x}{b-a}\right\} & x \ge a\\ 0 & \text{otherwise} \end{cases}$$
(3)

As such, the core of MI is equal to a and the support is equal to [a, b]. MI linearly decreases with the increase in xin the interval of its support. Figure 2c shows, for example, an MI where a = 10 and b = 40. As MI is for minimizing a quantity, setting its support [a, b] is a critical issue, similar to MX. This issue is also described in Section 3.

## 2.5. Degree of compliance of a crisp value

Let *d* be a point in the support of *MX* or *MI*; that is,  $d \in [a, b]$ . Its degree of compliance with *MX* or *MI*, denoted as  $CC_{MX}$  or  $CC_{MI}$ , respectively, is its membership value or degree of belief (DOB). Thus, Eqs. (4) and (5) can be used to express them:

$$CC_{MX} = MX(d) = \frac{d-a}{b-a},$$
(4)

$$CC_{MI} = MI(d) = \frac{b-d}{b-a}.$$
(5)

For example, consider that [a, b] = [10, 30] for both MX and MI. As such, if d = 15, then  $CC_{MX} = 0.25$  and  $CC_{MI} = 0.75$ . Needless to say, the nature of  $CC_{MX}$  or  $CC_{MI}$  resembles the nature of MX or MI, respectively. The higher the value of  $CC_{MX}$  or  $CC_{MI}$ , the better the d from the viewpoint of maximization or minimization, respectively.

## 2.6. Degree of compliance of a crisp granular information

Let P = [p, q] be an interval in the support [a, b] of MX or MI; that is,  $p \ge a \land q \le b$ , as schematically illustrated in Figure 3a–b. The compliance of P with respect to MX or MI denoted as  $RC_{MX}$  or  $RC_{MI}$ , respectively, is the average membership value of P with respect to MX or MI (Ullah, 2008; Rashid et al., 2011; Shamasuzzaman et al., 2013). Therefore, Eqs. (6) and (7) can be used to express them:

$$RC_{MX} = \frac{\int_{p} MX(x)dx}{|q-p|} = \frac{MX(p) + MX(q)}{2} = \frac{(p+q) - 2a}{2(b-a)}, \quad (6)$$



Fig. 3. Compliances of a range with respect to maximization and minimization fuzzy numbers.

$$RC_{MI} = \frac{\int_{p} MI(x)dx}{|q-p|} = \frac{MI(p) + MI(q)}{2} = \frac{2b - (p+q)}{2(b-a)}.$$
 (7)

As such,  $RC_{MX}$  and  $RC_{MI}$  take a value in the interval [0, 1]. The plot shown in Figure 3c for two arbitrary cases shows the typical nature of  $RC_{MX}$ . Case 1 corresponds to p = 12 + s, q =15 + s, s = 0, 0.5, ..., 15. The other case corresponds to p =12 + u, q = 20 + u, u = 0, 0.5, ..., 10. The range corresponding to the first case is relatively slim, whereas the other is relatively fat. In both cases,  $RC_{MX}$  linearly increases when it approaches the upper limit of maximization (i.e., b = 30).  $RC_{MX}$  becomes unit if it is a point equal to the core of MX(i.e., p = q = b).  $RC_{MX}$  becomes zero if it is a point equal to a, (i.e., p = q = a). Otherwise,  $RC_{MX} < 1$  (see Fig. 3c). The higher the value of  $RC_{MX}$ , the better the P from the viewpoint of maximization.

In contrast, the plot shown in Figure 3d for two arbitrary cases shows the typical nature of  $RC_{MI}$ . Case 1 corresponds to p = 12 + s, q = 15 + s, s = 0, 0.5,  $\ldots$ , 15. The other case corresponds to p = 12 + u, q = 20 + u, u = 0, 0.5,  $\ldots$ , 10. The range that corresponds to the first case is relatively slim, whereas the other is relatively fat, similar to that in  $RC_{MX}$ . In both cases,  $RC_{MI}$  linearly decreases when it approaches the lower limit of minimization (i.e., a = 10).  $RC_{MI}$  is unit if it is a point equal to the core of MI (i.e., p = q = a).  $RC_{MI}$  is zero if it is a point equal to b, (i.e., p = q = b). Otherwise,  $RC_{MI} < 1$  (see Fig. 3d). The higher the value of  $RC_{MI}$ , the better the P from the viewpoint of minimization.

# 2.7. Degree of compliance of a triangular fuzzy number

This subsection employs the notion of triangular fuzzy number as defined in Eq. (1) but expresses it using a different set of notations so that one can differentiate it from other triangular fuzzy numbers.

Let  $t_1$ ,  $t_2$ , and  $t_3$  be three points in the ascending order on the real-line; that is,  $t_1 \le t_2 \le t_3 \in \mathbb{R}$ . Let the interval  $[t_1, t_3]$  and the point  $t_2$  be the support and core, respectively, of a triangular fuzzy number denoted as *D*. As such, the following expression holds:

$$D(x) = \max\left\{0, \min\left(\left(\frac{x-t_1}{t_2-t_1}\right), \left(\frac{t_3-x}{t_3-t_2}\right)\right)\right\}.$$
 (8)

Recall the maximization fuzzy number *MX* defined in Equation (2) and its support [*a*, *b*]. Assume that the support of *D* belongs to the support of *MX*; that is,  $a \le t_1$  and  $b \ge t_3$ . This assumption is illustrated in Figure 4a, where the points of intersections of *D* and *MX* are  $V_{MX}(V_{MXx}, V_{MXy})$  and  $W_{MX}(W_{MXx}, W_{MXy})$ , and are given as

$$V_{MXx} = \frac{bt_1 - at_2}{(b - a) - (t_2 - t_1)},$$
  

$$V_{MXy} = \frac{t_1 - a}{(b - a) - (t_2 - t_1)},$$
(9)



(a) Interaction between the triangular and maximization fuzzy numbers



Fig. 4. Compliance of a triangular fuzzy number with respect to a maximization fuzzy number.

$$W_{MXx} = \frac{bt_3 - at_2}{(b - a) + (t_3 - t_2)},$$
  

$$W_{MXy} = \frac{t_3 - a}{(b - a) + (t_3 - t_2)}.$$
(10)

Let the area under the function  $\min(D(x), MX(x))$  be  $A_{MX}$ . As a result, the following expression holds:

$$A_{MX} = \int_{t_1}^{t_3} \min(D(x), MX(x)) dx$$
  
=  $\frac{V_{MXy}(W_{MXx} - t_1) + W_{MXy}(t_3 - V_{MXx})}{2}.$  (11)

The maximum possible  $A_{MX}$  is  $\frac{1}{2}(t_3 - t_1)$ , which occurs if  $t_1 = a$  and  $t_2 = t_3 = b$ , that is, if *D* takes the shape of *MX*. Therefore, if  $A_{MX}$  is normalized by the abovementioned maximum possible area, then the resulting quantity denoted as  $TC_{MX}$  measures the degree of compliance of *D* with respect to *MX* in the interval [0, 1]. Equation (12) is used to express this relationship:

$$TC_{MX} = \frac{A_{MX}}{\frac{1}{2}(t_3 - t_1)} = \frac{V_{MXy}(W_{MXx} - t_1) + W_{MXy}(t_3 - V_{MXx})}{(t_3 - t_1)}.$$
(12)

A typical nature of  $TC_{MX}$  is shown in Figure 4b for two arbitrary cases. Case 1 corresponds to  $t_1 = 10 + s$ ,  $t_2 = 12 + s$ ,

 $t_3 = 15 + s, s = 0, 0.5, ..., 15$ . The other case corresponds to  $t_1 = 10 + u, t_2 = 15 + u, t_3 = 20 + u, u = 0, 0.5, ..., 10$ . The triangular fuzzy number corresponding to the first case is relatively slim, whereas the other one is relatively fat. In both cases, an exponential increase in the value of  $TC_{MX}$  is observed, if the triangular fuzzy numbers approach the upper limit of maximization (i.e., b = 30).  $TC_{MX}$  becomes unit if D takes the shape of MX (i.e.,  $t_1 = a, t_2 = t_3 = b$ ). Otherwise,  $TC_{MX} < 1$  (see Fig. 4b). The more the D resembles MX, the higher is the value of  $TC_{MX}$  is, the better is the D from the viewpoint of maximization.

Recall the minimization fuzzy number *MI* defined by Eq. (3) and its support [*a*, *b*]. We assume that the support of *D* belongs to the support of *MI*; that is,  $a \le t_1$  and  $b \ge t_3$ . This assumption is illustrated in Figure 5a, where the points of intersections between *D* and *MI* are  $V_{MI}(V_{MIx}, V_{MIy})$  and  $W_{MI}(W_{MIx}, W_{MIy})$ , and are given, as follows:

$$V_{MIx} = \frac{bt_2 - at_1}{(b - a) + (t_2 - t_1)},$$
  
$$V_{MIy} = \frac{b - t_1}{(b - a) + (t_2 - t_1)},$$
(13)

$$W_{MLx} = \frac{bt_2 - at_3}{(b-a) - (t_3 - t_2)},$$
  

$$W_{MLy} = \frac{b - t_3}{(b-a) - (t_3 - t_2)}.$$
(14)



(a) Interaction between a triangular and a minimization fuzzy number



Fig. 5. Compliance of a triangular fuzzy number with respect to a minimization fuzzy number.

Let the area under the function  $\min(D(x), MI(x))$  be  $A_{MI}$ . As a result, the following expression holds:

$$A_{MI} = \int_{t_1}^{t_3} \min(D(x), MI(x)) dx$$
$$= \frac{V_{MIy}(W_{MIx} - t_1) + W_{MIy}(t_3 - V_{MIx})}{2}.$$
 (15)

The maximum possible  $A_{MI}$  is  $\frac{1}{2}(t_3 - t_1)$ , which occurs when  $t_1 = t_2 = a$  and  $t_3 = b$ , that is, when *D* takes the shape of *MI*. Therefore, if  $A_{MI}$  is normalized by the abovementioned maximum possible area, then the resulting quantity denoted as  $TC_{MI}$  measures the degree of compliance of *D* with respect to *MI* in the interval [0, 1]. The expression of  $TC_{MI}$  can be expressed as follows:

$$TC_{MI} = \frac{A_{MI}}{\frac{1}{2}(t_3 - t_1)} = \frac{V_{MIy}(W_{MIx} - t_1) + W_{MIy}(t_3 - V_{MIx})}{(t_3 - t_1)}.$$
 (16)

The typical nature of  $TC_{MI}$  is shown in Figure 5b for two different cases. Case 1 corresponds to  $t_1 = 10 + s$ ,  $t_2 = 12 + s$ ,  $t_3 = 15 + s$ , s = 0, 0.5, ..., 15. The other case corresponds to  $t_1 = 10 + u$ ,  $t_2 = 15 + u$ ,  $t_3 = 20 + u$ , u = 0, 0.5, ..., 10. The triangular fuzzy number corresponding to the first case is relatively slim compared to that of the other case. In both cases,  $TC_{MI}$  linearly increases if the triangular fuzzy number approaches the upper limit of maximization (i.e., b = 30). It is worth mentioning that  $TC_{MI}$  becomes unit if D takes the shape of MI (i.e.,  $t_1 = a$ ,  $t_2 = t_3 = b$ ). Otherwise,  $TC_{MI} < 1$  (see Fig. 5b). The higher the value of  $TC_{MI}$ , the better the D from the viewpoint of minimization.

### **3. DETERMINING THE SUPPORTS**

To define the maximization or minimization fuzzy number denoted as *MX* or *MI*, as described in the previous section, the support [*a*, *b*] must be known beforehand. Despite the remarkable progress of fuzzy-number-based knowledge-based systems, it remains true that no unique, best-of-the-world solution exists for setting a support of a fuzzy number unless it is induced using a set of numerical data (see Section 4). Keeping this in mind, this section describes four types of supports, namely, *deterministic*, *local, semiglobal*, and *global* supports, for defining *MX* or *MI*. These supports are described below using numerical examples.

Consider the support called deterministic support. Deterministic support means a support that is known to all without any controversy. For example, consider the parameter called recycle fraction. It is customary to express the recycle fraction using a number taken from the interval [0, 1]. This means that if one defines MX or MI for maximizing or minimizing the recycle fraction, respectively, then the support [a, b] is equal to [0, 1]; that is, [a, b] = [0, 1]. The same argument holds for numerous physical quantities. It is worth mentioning that the compliances described in the previous section also underlie a deter-

ministic support that is equal to [0, 1]. If one is interested in seeing whether the compliances of an alternative for a set of criteria are being maximized, he or she obviously chooses an MX for compliance maximization. In this case, the MX underlies a support equal to [0, 1] because the values of the compliances always lie in the interval [0, 1] no matter the type of compliance (crisp, range, and fuzzy), as described in the previous section.

However, the local, semiglobal, and global supports are somewhat subjective and, thereby, depend on the user's judgment or the available numerical data. For example, consider the following scenario. Engineering materials are divided into seven classes, namely, wood and wooden products, foams, rubbers, polymers, composites, ceramics, and metals and alloys. Assume that one is interested in maximizing or minimizing the density of material. According to (Ashby, 2005, pp. 520–521) the density (Mg/m<sup>3</sup>) of wood and wooden products, foams, rubbers, polymers, composites, ceramics, and metals and alloys lies in the interval [0.6, 1.05], [0.016, 0.47], [0.92, 0.955], [0.89, 1.58], [1.5, 2.9], [1.9, 15.9], and [1.74, 8.94], respectively.

Now, if one considers a class of materials, for example, metals and alloys, as the alternatives, and wants to evaluate the materials in the class using density as one of the criteria, then an interval [1.74, 8.94], or even a larger one (e.g., [1, 10]), becomes the support of MX or MI because the suggested support subsumes the intervals representing the density of all materials belonging to the considered class according to the supplied data. This kind of support is called the local support in the sense the support focuses alternatives that belong to a single class.

In contrast, if one considers two classes of materials, for example, polymers and ceramics, as the alternatives, and wants to evaluate the materials of both classes using density as one of the criteria, then an interval [0.89, 15.9], or even a larger one (e.g., [0.5, 20]), becomes the support of *MX* or *MI* because the suggested support subsumes [0.89, 1.58] and [1.9, 15.9], that is, the intervals underlying the two classes of materials considered in terms of the criterion called density according to the supplied information. This kind of support is called the semilocal support.

Moreover, if one considers all materials as alternatives, and wants to evaluate them using density as one of the criteria, then an interval [0.016, 15.9], or even a larger one (e.g., [0.01, 20]) becomes the support of *MX* or *MI*. The reason is that the suggested support includes all intervals for all the materials considered in terms of the criterion called density according to the supplied information. This kind of support is called the global support.

## 4. INDUCTION OF A TRIANGULAR FUZZY NUMBER FROM NUMERICAL DATA

In certain cases, the uncertainty associated with a set of numerical data can be represented by a possibility distribution of triangular form, that is, a triangular fuzzy number. To do this, it is important to develop a transformation mechanism based on the probability–possibility consistency principle,



Fig. 6. Representing the uncertainty of numerical data using a triangular fuzzy number.

which states that lessening of the possibility of an event tends to lessen its probability, but not vice versa (Zadeh, 1978). Figure 6 illustrates a triangular fuzzy number induction process using an arbitrary set of numerical data  $X = \{(i, x(i)) \in \Re \mid i = 0, ..., 100\}$ . As we have seen in Figure 6, the variability associated with a variable *X* is first represented by a point-cloud that is the plot in ordered pairs  $\{(x(i), x(i+1)) \mid i = 0, 1, ..., 99\}$ . Using a probability–possibility transformation, the pointcloud can be transformed into a triangular fuzzy number. See Sharif Ullah and Shamsuzzaman (2013) for a detailed procedure that transforms a point-cloud to a triangular fuzzy number. The induced triangular fuzzy number can be used to calculate the degree of compliance of the supplied set of data on *X* with respect to *MX* or *MI*, as described in Section 2.6.

It is worth mentioning that the set of numerical data must lie in the support of MX or MI; that is,  $x(i) \in [a, b]$ , i = 0,  $1, \ldots, n$ . Otherwise, the calculation of the degree of compliance cannot be performed. In addition, if a variable X takes values from a unimodal probability distribution (e.g., from uniform, normal, or triangular distribution), then its equivalent possibility distribution (a triangular fuzzy number) can be used while calculating the degree of compliance in accordance with the procedure described in Section 2.6. Sharif Ullah and Shamsuzzaman (2013) shows the equivalent triangular fuzzy numbers for the uniform and normal distributions.

## 5. PROPOSED DECISION MODEL

This section describes the proposed decision model. The proposed decision model employs the formulations described in Section 2 to Section 4, and helps users to make a decision under epistemic uncertainty, as described in Section 1. Figure 7

schematically illustrates the proposed decision model and its relationship with the decision-relevant (analytic and/or empirical) knowledge. As seen from Figure 7, the decision model consists of four modules, namely, formulation, information gathering, compliance calculation, and aggregation. The formulation and information gathering modules work in coordination with the decision-relevant knowledge. This means that the available knowledge regarding a given decision problem plays a vital role while performing the activities of formulation and information gathering modules. The output of the formulation module serves as an input for the information gathering module. The combined output of the formulation and information gathering modules serves as the input for the compliance calculation module. The output of the compliance calculation module is the degrees of compliances for all alternatives for each criterion. Once the compliance calculation module completes its function, the aggregation module makes a trade-off among the compliances of some of the selected criteria based on the user-defined importance in order to rank the alternatives. The ranks of the alternatives thus help make an informed decision. The decision made can be fed into the existing body of knowledge to enrich it, as schematically illustrated in Figure 7.

However, the above description of the proposed decision model is rather informal. A relatively formal description of the decision model is given, as follows: consider the formulation module. To be more specific, let  $A = \{A_1, \ldots, A_N\}$  be the set of *N* different alternatives,  $C = \{C_1, \ldots, C_M\}$  be the set of *M* different criteria, and  $O = \{O_1, \ldots, O_M\}$  be the set of the states of the members in *C* so that  $\forall O_j \in \{\text{maximization}, \text{mini$  $mization}\}$ ,  $j = 1, \ldots, M$ . The purpose of the formulation module is to define *A*, *C*, and *O*. In doing so, the formulation



Fig. 7. Proposed decision model.

module relies on the analytical and empirical knowledge underlying the decision problem, as schematically illustrated in Figure 7. Finally, the formulation module decides the natures of the objective functions for the criteria in *C* as follows. Let  $OB = \{OB_1, \ldots, OB_M\}$  be the set of the objective functions of the criteria defined in *C*. As such, if  $O_j$  = maximization, then  $OB_j = MX_j$ ; otherwise,  $OB_j = MI_j$ .

Once the formulation module completes its functions, the second module, called information gathering, gathers all sorts of data/information needed for determining the degree of compliances. It gathers the information to define the supports of the objective functions. Needless to say, there are four types of supports, namely, deterministic, local, semiglobal, and *global* supports, as described in Section 3. However, to be more specific, let  $S_i = [a_i, b_j]$  be the support of  $OB_j, \forall j$  $\in \{1, \ldots, M\}$ . Thus,  $S_i = [a_i, b_i], \forall j \in \{1, \ldots, M\}$  can be a deterministic, local, semiglobal, or global support. The other function of the information gathering module is to gather the decision-relevant information on each alternative defined in A for all criteria defined in C. Here, a piece of decision-relevant information denoted as  $DRI_{i,i}$  can be a set of numerical values  $\{d_{i,j} \mid k = 1, 2, ...\}$ , a set of real intervals  $\{P_{i,j}^l | l = 1, 2, ...\}$ , a set of triangular fuzzy numbers  $\{D_{i,j}^r | l = 1, 2, ...\}$  $r = 1, 2, \ldots$ , and any combination of these. This implies that  $DRI_{i,j} \subseteq \{DRI^{k}_{i,j}, DRI^{l}_{i,j}, DRI^{r}_{i,j}\}, \text{ where } DRI^{k}_{i,j} = \{d^{k}_{i,j} \mid k =$ 1,2,...},  $DRI_{ij}^{l} = \{ P_{ij}^{l} | l = 1, 2, ... \}, \text{ and } DRI_{ij}^{r} = \{ D_{ij}^{r} \}$  $| r = 1, 2, \ldots \}.$ 

Using the outcomes of the formulation and information gathering modules, the subsequent module, that is, the compliance calculation module, calculates the degree of compliance for each combination of alternative and criterion. A degree of compliance denoted as  $COM_{i,j} \in [0, 1]$  is calculated by inputting each member of  $DRI_{i,j}$  in to  $CC_{MX}$ ,  $CC_{MI}$ ,  $RC_{MX}$ ,  $RC_{MI}$ ,  $TC_{MX}$ , or  $TC_{MI}$ , as defined in Section 2. If  $DRF_{i,j}$  is a member of  $DRI_{i,j}$ , then the corresponding degree of compliance can be represented as  $COM_{i,j}^2$ .

Finally, the aggregation module aggregates the compliances of an alternative for some selected criteria in order to rank the alternatives so that one can make an informed decision. To be more specific let  $Y_{i,j} = \{COM_{i,j}^z | z = 1, 2, ...\}$  be the set of compliances of the *i*th alternative with respect to *j*th criterion. Using  $Y_{i,j} \in [0, 1]$  a triangular fuzzy number denoted as  $TA_{i,i}$  can be induced. The induction process is described in Section 4. Let the support and core of the induced triangular fuzzy number  $TA_{i,j}$  be  $[t_{1ij}, t_{3ij}]$  and  $t_{2ij}$ , respectively. As the values of the compliance lie in the interval [0, 1] and the compliance must be maximized, a special maximization fuzzy number denoted as  $COM_{MX}$  can be considered where the support and core are [a, b] = [0, 1] and b =1, respectively. As a result, the compliance of  $TA_{i,i}$  with respect to  $COM_{MX}$  is the ranking score of the *i*th alternative with respect to the *j*th criterion denoted as  $RS_{i,j}$ . Recall the procedure of determining the compliance of a triangular fuzzy number with respect to a maximization fuzzy number described in Section 2 [see Fig. 4 and Eqs. (8)-(12)]. This procedure is valid for  $TA_{i,j}$  and  $COM_{MX}$ , too. The interaction between  $TA_{i,j}$  and  $COM_{MX}$  is schematically illustrated in Figure 8, which is a similar case illustrated in Figure 4. In Figure 8, the points of intersections of  $TA_{i,i}$  and  $COM_{MX}$ are  $V_{MXij}(V_{MXxij}, V_{MXyij})$  and  $W_{MXij}(W_{MXxij}, W_{MXyij})$ . This yields the following expression defining  $RS_{i,j}$ :

$$RS_{ij} = \frac{V_{MXyij}(W_{MXxij} - t_{1ij}) + W_{MXyij}(t_{3ij} - V_{MXxij})}{(t_{3ij} - t_{1ij})}.$$
 (17)



Fig. 8. Determining the ranking of an alternative based on a criterion.

We found the following relationships by substituting 0, 1,  $t_{1ij}$ ,  $t_{2ij}$ ,  $t_{3ij}$ ,  $V_{MXxij}$ ,  $V_{MXyij}$ ,  $W_{MXxij}$ , and  $W_{MXyij}$  for a, b,  $t_1$ ,  $t_2$ ,  $t_3$ ,  $V_{MXx}$ ,  $V_{MXy}$ ,  $W_{MXx}$ , and  $W_{MXy}$ , respectively, in Eqs. (9) and (10):

$$V_{MXxij} = V_{MXyij} = \frac{t_{1ij}}{1 - (t_{2ij} - t_{1ij})},$$
(18)

$$W_{MXxij} = W_{MXyij} = \frac{t_{3ij}}{1 + (t_{3ij} - t_{2ij})}.$$
 (19)

Therefore, the ranking score  $RS_{i,j}$  defined in Eq. (17) is calculated after calculating  $V_{MXxij}$ ,  $V_{MXyij}$ ,  $W_{MXxij}$ , and  $W_{MXyij}$  using Eqs. (18) and (19), respectively. The ranking scores of an alternative  $A_i$  for all criteria can be added using the weighted importance. This yields a decision score denoted as  $DC(A_i)$ , as follows:

$$DC(A_j) = \sum_{j=1}^{M} w_j RS_{ij}, \text{ so that}$$
$$w_j = \frac{IMP_j}{\sum_{i=1}^{M} IMP_i}.$$
(20)

In Eq. (20),  $IMP_j$  is the importance of *j*th criterion that is an integer in the scale 0 to 10; that is,  $IMP_j \in \{0, 1, ..., 10\}, \forall j \in \{1, ..., M\}$ . The more the importance of the criterion, the greater the value of  $IMP_j$ . Thus,  $w_j$  represents the normalized weight of the *j*th criterion,  $\forall w_j \in [0, 1]$ . Note that each  $IMP_j$  is assigned subjectively by the decision maker(s).

### 6. RESULTS AND DISCUSSIONS

We will use the same material selection problem illustrated in Figure 1 to show how our proposed model works. Consider the formulation module. Here, three alternatives are considered as listed in Table 1 based on the general knowledge regarding materials used for making vehicle parts (McDowell et al., 2010; Omar, 2011; Mayyas, Mayyas, et al., 2012; Mayyas, Qattawi, et al., 2012; Poulikidou et al., 2015). The first alternative is a set of aluminum alloys (Al) that consists of 197 types of aluminum-based alloys. The second alternative is set of magnesium alloys (Mg) that consists of 30 types of magnesium-based alloys. The last alternative is set of titanium alloys (Ti) that consists of 45 types of titanium-based alloys. The number of alloys 197, 30, and 45 of Al, Mg, and Ti are considered based on the information available in a material database (CES Selector, Granta Design Limited, UK).

**Table 1.** Alternatives (A)

$A_1 = \text{Aluminum} \\ \text{Alloys (Al)}$	$A_2 = Magnesium$ Alloys (Mg)	$A_3 = $ Titanium Alloys (Ti)
197 total types of Al alloys are considered in A <sub>1</sub>	30 total types of Mg alloys are considered in A <sub>2</sub>	45 total types of Ti alloys are considered in A <sub>3</sub>

To select materials for engineering components, there are material indices (Ashby, 2005, pp. 509-512). The indices depend on the nature of a component (e.g., tie, shaft, beam, column, plate, and panel) and the objective (e.g., stiffness-limited design at minimum mass and strength-limited design at minimum mass). In these indices, such material properties as density, tensile strength, and Young's modulus are involved. Therefore, when the nature of the component is unknown or not given, as it is the case here (Fig. 1), at least, three material properties, namely, density, tensile strength, and Young's modulus, must be considered to ensure the structural integrity of the component. In addition, according to the material indices (Ashby, 2005, pp. 509–512), to achieve a given objective (e.g., stiffness-limited design at minimum mass and strength-limited design at minimum mass), the density must be minimized whereas the tensile strength and Young's modulus must be maximized. For example, the environmental impact of a vehicle can be minimized by reducing its weight. Therefore, minimization of density helps reduce the environmental impact, too. Moreover, to reduce the usages of material, that is, to increase the material efficiency (Allwood et al., 2011; Ullah et al., 2013; Sharif Ullah et al., 2014), the recycle fraction of materials must be maximized. At the same time, the primary production of materials must not produce a large quantity of greenhouse gasses (i.e., consume energy) and consume resources (e.g., water and land; Rashid et al., 2011; Ullah et al., 2013; Sharif Ullah et al., 2014). Thus, besides density, water usage, CO<sub>2</sub> footprint of primary production of materials, and the recycle fraction must be considered in order to accommodate the issue of sustainability while selecting material for making the body of a vehicle.

Based on the above contemplation, a set of six criteria, namely, density, tensile strength, Young's modulus, water usage,  $CO_2$  footprint, recycle fraction, are considered to evaluate the alternatives called Al, Mg, and Ti. The decision-relevant information of these six criteria are shown by the minimum–maximum plots in Figure 9. As the material properties of an alloy are given by some numerical ranges or as a crisp granular information (see CES Selector database), the minimum and maximum values of each range can be plotted on the horizontal and vertical axis, respectively. For example, let the density of an alloy be [2.63, 2.78] Mg/m<sup>3</sup> (here "Mg" is mega-gram not magnesium). This piece of decision-relevant information is thus a point (2.63, 2.78) on the minimum–maximum plot.

However, based on the decision-relevant information shown in Figure 9, the supports of the respective criterion are determined, as summarized in Table 2. As such, all supports here are local supports except the support of recycle fraction, which is a global support. The optimization states of the criteria are also listed in Table 2. As we see from Table 2, the tensile strength, Young's modulus, and recycle fraction must be maximized, whereas the density, water usage, and  $CO_2$  footprint must be minimized, as described above.

The compliances of each alloy are determined using the procedure described in the previous section and shown by



Fig. 9. Decision-relevant information for three different categories of metal alloys.

Table 2.	States	of	criteria	and	their	supports
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	Criteria (C)						
Items (↓)	$C_1 = \text{Density}$ (mg/m <sup>3</sup> )	$C_2 = \text{Tensile}$ Strength (MPa)	$C_3 = Young's$ Modulus (GPa)	$C_4 = Water$ Usage (kg/kg)	$C_5 = CO_2$ Footprint (kg/kg-CO <sub>2</sub> )	$C_6 = \text{Recycle}$ Fraction (%)	
States Supports [a, b]	Minimize [1, 15]	Maximize [5, 1800]	Maximize [10, 250]	Minimize [0.1, 10]	Minimize [1, 65]	Maximize [0, 100]	



Fig. 10. Compliances of the alternatives for respective criterion.

the plots in Figure 10. As we see from the plots in Figure 10, the order of preference in terms density is Mg > Al > Ti, tensile strength is Ti > Al > Mg, Young's modulus is Ti > Al > Mg, water usage is Al > Ti > Mg,  $CO_2$  footprint is Al > Mg > Ti, and recycle fraction is Al > Mg > Ti.

The ranking scores of the three alternatives for each criterion are also determined using the procedure described in the previous section and shown in Table 3. This ranking score also preserves the abovementioned order of preferences, as indicated in the last row in Table 3. This means that the ranking score is an effective means to aggregating the uncertainty associated with an alternative for a given criterion.

Once the ranking scores are known, one can determine the decision score as described in the previous section. In doing so, the importance of the criteria must be set. For this particular case, the criteria called density, water usage,  $CO_2$  footprint, and recycle fraction are useful in assessing the sustainability of material and, thereby, the sustainability of vehicles, as described in the above. The other two criteria, namely, Young's modulus and tensile strength, are useful for ensuring

Table 3.	Ranking	scores	of the	alternatives
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	Criteria (C)					
Alternatives (A)	$C_1 = \text{Density}$	$C_2 = $ Tensile Strength	$C_3 =$ Young's Modulus	$C_4 =$ Water Usage	$C_5 = CO_2$ Footprint	$C_6 = \text{Recycle}$ Fraction
$A_1 = Al$	0.982	0.327	0.470	0.992	0.966	0.426
$A_2 = Mg$	0.995	0.243	0.255	0.872	0.871	0.418
$A_3 = Ti$	0.906	0.741	0.666	0.915	0.780	0.399
Preferential order	Mg > Al > Ti	Ti > Al > Mg	Ti > Al > Mg	Al > Ti > Mg	Al > Mg > Ti	Al > Mg > Ti

 Table 4. Decision scores of the alternatives

	Importance				
Criteria (C)	Set 1	Set 2	Set 3		
$C_1 = \text{density}$	10	10	10		
$C_2$ = tensile strength	10	5	1		
$C_3 =$ Young's modulus	10	5	1		
$C_4 =$ water usage	10	10	10		
$C_5 = CO_2$ footprint	10	10	10		
$C_6$ = recycle fraction	10	10	10		
Alternatives (A)		Decision Scores			
$A_1 = Al$	0.694	0.753	0.820		
$A_2 = Mg$	0.609	0.681	0.763		
$A_3 = Ti$	0.735	0.741	0.748		
_	Ti > Al > g	Al > Ti > Mg	Al > M > Ti		

the structural integrity of the body of a vehicle. Therefore, density, water usage, CO<sub>2</sub> footprint, and recycle fraction are called sustainability criteria, and the other two are called integrity criteria. One can determine the decision-scores of the alternatives for different sets of importance as shown in Table 4. In particular, three sets of importances are chosen here for determining the decision scores. In the first set, both sustainability and integrity criteria are considered equally important. This makes Ti's decision score the maximum followed by those of Al and Mg, respectively. Thus, when both sustainability and integrity criteria have the same degree of importance, the list of preferences is Ti >Al > Mg. In the second set, sustainability criteria are considered relatively more important than the integrity criteria. This makes Al's decision score the maximum followed by those of Ti and Mg, respectively. Thus, when the sustainability criteria are more important than the integrity criteria, the list of preferences is Al > Ti > Mg. This means that Ti and Al alternate their positions once the integrity criteria lose their importance compared to those of sustainability. In the last set, the sustainability criteria are considered very important compared to those of integrity. This makes Al's decision score the maximum followed by those of Mg and Ti, respectively. Thus, when the integrity criteria are somewhat insignificant compared to those of sustainability, the list of preferences is Al > Mg > Ti. This means that Al and Mg are the preferred materials when the sustainability is a key concern.

### 7. CONCLUDING REMARKS

Selecting appropriate materials at an early stage of a design process helps manage the complexity in the subsequent steps of product realization (detailed design, manufacturing, assembly, and operations management). Therefore, material selection entails a great deal of significance in engineering design.

The early stage of a design process means that the design specifications and requirements are not known. Therefore, conventional material selection procedures are not applicable for selecting materials at an early stage of a design process. This study sheds some lights on this issue by developing a novel decision model that helps make a decision even though the design specifications and requirements are still evolving.

In the presented decision model, the mathematical entities called triangular fuzzy number, compliance, and decisionscore play a vital role. They are helpful for assessing and managing the heterogeneous decision-relevant information and conflicting objectives. The participation of a decision maker is also assured by introducing the user-defined importance in the calculation process of the decision score.

Although a set of six criteria (density, tensile strength, Young's modulus, water usage,  $CO_2$  footprint, and recycle fraction) is used in selecting materials for the body of a vehicle under epistemic uncertainty, one can add other criteria (e.g., cost, reserve, thermal property) if needed. Adding criteria will enlarge the set of the degrees of compliances without adding any additional information processing steps in the decision-making process. Therefore, the presented decision model possesses a great deal of scalabilities.

The advanced outlook on design process states that a design process is not only a knowledge-using process but also a knowledge-creation process; the creation of knowledge takes place if one can handle the epistemic uncertainty in a systematic manner. As demonstrated in this study, the presented decision model can handle epistemic uncertainty in a systematic manner. It is also shown to be useful in creating new knowledge (e.g., it can create a list of material preferences even though the required design knowledge is not available). Thus, the presented decision model can be integrated with a design process when knowledge creation is preferred over knowledge use. This particularly true when a problem-based design is transformed into a solution-based design. Nonetheless, how to integrate the presented decision model with the multiexpert decision-making scenarios (Noor-E-Alam et al., 2011) is a future direction of research.

#### REFERENCES

- Achiche, S., & Ahmed-Kristensen, S. (2011). Genetic fuzzy modeling of user perception of three-dimensional shapes. Artificial Intelligence for Engineering Design, Analysis and Manufacturing 25(1), 93–107. doi:10. 1017/S0890060410000466
- Allwood, J.M., Ashby, M.F., Gutowski, T.G., & Worrell, E. (2011). Material efficiency: a white paper. *Resources, Conservation and Recycling* 55(3), 362–381. doi:10.1016/j.resconrec.2010.11.002
- Antonsson, E.K., & Otto, K.N. (1995). Imprecision in engineering design. Journal of Mechanical Design 117(B), 25–32. doi:10.1115/1.2836465
- Ashby, M.F. (2005). *Materials Selection in Mechanical Design*, 3rd ed. Oxford: Butterworth-Heinemann.
- Booker, J.M., & Ross, T.J. (2011). An evolution of uncertainty assessment and quantification. *Scientia Iranica* 18(3), 669–676. doi:10.1016/j. scient.2011.04.017
- Dempster, A.P. (1968). A generalization of Bayesian inference. Journal of the Royal Statistical Society. Series B (Methodological) 30(2), 205–247.
- Dempster, A.P. (2008). A generalization of Bayesian inference. In *Classic Works of the Dempster-Shafer Theory of Belief Functions* (Yager, R.R., & Liu, L., Eds.), pp. 73–104. Berlin: Springer.
- Dijkman, J.G., van Haeringen, H., & de Lange, S.J. (1983). Fuzzy numbers. Journal of Mathematical Analysis and Applications 92(2), 301–341. doi:10.1016/0022-247X(83)90253-6

- Dubois, D., Foulloy, L., Mauris, G., & Prade, H. (2004). Probability-possibility transformations, triangular fuzzy sets, and probabilistic inequalities. *Reliable Computing 10(4)*, 273–297. doi:10.1023/B:REOM. 0000032115.22510.b5
- Dubois, D., & Prade, H. (1978). Operations on fuzzy numbers. International Journal of Systems Science 9(6), 613–626. doi:10.1080/0020772780 8941724
- Dubois, D., & Prade, H. (1988). Possibility Theory. New York: Plenum Press.
- Gurnani, A.P., & Lewis, K. (2005). Robust multiattribute decision making under risk and uncertainty in engineering design. *Engineering Optimization* 37(8), 813–830. doi:10.1080/03052150500340520
- Huang, G.Q., & Jiang, Z. (2002). FuzzySTAR: fuzzy set theory of axiomatic design review. Artificial Intelligence for Engineering Design, Analysis and Manufacturing 16(4), 291–302. doi:10.1017/S0890060402164031
- Jiang, Z., Li, W., Apley, D.W., & Chen, W. (2015). A spatial-random-process based multidisciplinary system uncertainty propagation approach with model uncertainty. *Journal of Mechanical Design* 137(10), 101402– 101402. doi:10.1115/1.4031096
- Joslyn, C.A., & Booker, J.M. (2004). Generalized information theory for engineering modeling and simulation. In *Engineering Design Reliability Handbook* (Nikolaidis, E., Ghiocel, D.M., & Singhal, S., Eds.). Boca Raton, FL: CRC Press.
- Khozaimy, O., Al-Dhaheri, A., & Ullah, A.M.M.S. (2011). A decision-making approach using point-cloud-based granular information. *Applied Soft Computing* 11(2), 2576–2586. doi:10.1016/j.asoc.2010.10.007
- Klir, G.J. (1990). A principle of uncertainty and information invariance. International Journal of General Systems 17(2–3), 249–275. doi:10.1080/ 03081079008935110
- Klir, G.J. (1999). On fuzzy-set interpretation of possibility theory. *Fuzzy Sets and Systems 108(3)*, 263–273. doi:10.1016/S0165-0114(97)00371-0
- Matsumura, T., & Haftka, R.T. (2013). Reliability based design optimization modeling future redesign with different epistemic uncertainty treatments. *Journal of Mechanical Design 135(9)*, 091006–091006. doi:10.1115/ 1.4024726
- Mayyas, A.T., Mayyas, A., Qattawi, A., & Omar, M.A. (2012). Sustainable lightweight vehicle design: a case study of eco-material selection for body-in-white. *International Journal of Sustainable Manufacturing* 2(4), 317–337. doi:10.1504/IJSM.2012.048586
- Mayyas, A.T., Qattawi, A., Omar, M., & Shan, D. (2012). Design for sustainability in automotive industry: a comprehensive review. *Renewable and Sustainable Energy Reviews* 16(4), 1845–1862. doi:10.1016/j.rser.2012.01.012
- McDowell, D.L., Panchal, J.H., Choi, H.-J., Seepersad, C.C., Allen, J.K., & Mistree, F. (2010). Managing Design Complexity Integrated Design of Multiscale, Multifunctional Materials and Products. Boston: Butterworth-Heinemann.
- Nikolaidis, E., Chen, S., Cudney, H., Haftka, R.T., & Rosca, R. (2003). Comparison of probability and possibility for design against catastrophic failure under uncertainty. *Journal of Mechanical Design 126(3)*, 386–394. doi:10.1115/1.1701878
- Nikolaidis, E., Ghiocel, D.M., & Singhal, S. (Eds.) (2004). Engineering Design Reliability Handbook. Boca Raton, FL: CRC Press.
- Noor-E-Alam, M., Lipi, T.F., Hasin, M.A.A., & Sharif Ullah, A.M.M. (2011). Algorithms for fuzzy multi expert multi criteria decision making (ME-MCDM). *Knowledge-Based Systems* 24(3), 367–377. doi:10.1016/ j.knosys.2010.10.006
- Omar, M.A. (2011). The Automotive Body Manufacturing Systems and Processes. Hoboken, NJ: Wiley.
- Poulikidou, S., Schneider, C., Björklund, A., Kazemahvazi, S., Wennhage, P., & Zenkert, D. (2015). A material selection approach to evaluate material substitution for minimizing the life cycle environmental impact of vehicles. *Materials & Design*, 83, 704–712. doi:10.1016/j.matdes.2015.06.079
- Rashid, M.M., Sharif Ullah, A.M.M., Tamaki, J., & Kubo, A. (2011). Evaluation of hard materials using eco-attributes. *Advanced Materials Research* 325, 693–698.
- Rezaee, R., Brown, J., Augenbroe, G., & Kim, J. (2015). Assessment of uncertainty and confidence in building design exploration. Artificial Intelligence for Engineering Design, Analysis and Manufacturing 29(4), 429–441. doi:10.1017/S0890060415000426
- Ross, T.J., Booker, J.M., & Montoya, A.C. (2013). New developments in uncertainty assessment and uncertainty management. *Expert Systems With Applications* 40(3), 964–974. doi:10.1016/j.eswa.2012.05.054
- Shafer, G. (1976). A Mathematical Theory of Evidence. Princeton, NJ: Princeton University Press.

- Shamasuzzaman, M., Sharif Ullah, A.M.M., & Dweiri, F.T. (2013). A fuzzy decision model for the selection of coals for industrial use. *International Journal of Industrial and Systems Engineering* 14(2), 230–244.
- Sharif Ullah, A.M.M., Fuji, A., Kubo, A., & Tamaki, J. (2014). Analyzing the sustainability of bimetallic components. *International Journal of Automation Technology* 8(5), 745–753.
- Sharif Ullah, A.M.M., Rashid, M.M., & Tamaki, J. (2012). On some unique features of C-K theory of design. CIRP Journal of Manufacturing Science and Technology 5(1), 55–66. doi:10.1016/j.cirpj.2011.09.001
- Sharif Ullah, A.M.M., Sato, M., Watanabe, M., & Rashid, M.M. (2016). Integrating CAD, TRIZ, and customer needs. *International Journal of Automation Technology* 10(2), 132–143.
- Sharif Ullah, A.M.M., & Shamsuzzaman, M. (2013). Fuzzy Monte Carlo simulation using point-cloud-based probability-possibility transformation. *Simulation* 89(7), 860–875. doi:10.1177/0037549713482174
- Sharif Ullah, A.M.M., & Tamaki, J. (2011). Analysis of Kano-model-based customer needs for product development. *Systems Engineering* 14(2), 154–172. doi:10.1002/sys.20168
- Ullah, A.M.M.S. (2005a). A fuzzy decision model for conceptual design. Systems Engineering 8(4), 296–308. doi:10.1002/sys.20038
- Ullah, A.M.M.S. (2005b). Handling design perceptions: an axiomatic design perspective. *Research in Engineering Design 16(3)*, 109–117. doi:10.1007/ s00163-005-0002-2
- Ullah, A.M.M.S. (2008). Logical interaction between domain knowledge and human cognition in design. *International Journal of Manufacturing Technol*ogy and Management 14(1–2), 215–227. doi:10.1504/IJMTM.2008.017496
- Ullah, A.M.M.S., & Harib, K.H. (2008). An intelligent method for selecting optimal materials and its application. Advanced Engineering Informatics 22(4), 473–483. doi:10.1016/j.aei.2008.05.006
- Ullah, A.M.M.S., Hashimoto, H., Kubo, A., & Tamaki, J. (2013). Sustainability analysis of rapid prototyping: material/resource and process perspectives. *International Journal of Sustainable Manufacturing* 3(1), 20–36. doi:10.1504/IJSM.2013.058640
- Walley, P. (1991). Statistical Reasoning With Imprecise Probabilities. London: Chapman Hall.
- Walley, P. (2000). Towards a unified theory of imprecise probability. *International Journal of Approximate Reasoning* 24(2–3), 125–148. doi:10.1016/S0888-613X(00)00031-1
- Youn, B.D., & Choi, K.K. (2004). Selecting probabilistic approaches for reliability-based design optimization. AIAA Journal 42(1), 124–131. doi:10. 2514/1.9036
- Zadeh, L.A. (1975). The concept of a linguistic variable and its application to approximate reasoning. *Information Sciences Part I* (8), 199–249; *Part II* (8), 301–357; *Part III* (9), 43–80.
- Zadeh, L.A. (1978). Fuzzy sets as a basis for a theory of possibility. *Fuzzy* Sets and Systems 1(1), 3–28. doi:10.1016/0165-0114(78)90029-5
- Zadeh, L.A. (2005). Toward a generalized theory of uncertainty (GTU)—an outline. *Information Sciences* 172(1–2), 1–40. doi:10.1016/j.ins.2005.01.017

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