

Investigation of stearic acid additive effects on the mechanochemical synthesis of silver nanoparticles

Behruz Khakan,^{1,a)} Abbas Shahroozi,¹ Ahmad Afsari,^{2,*} and Seyed Reza Hosseini¹

¹Department of Materials Science and Engineering, School of Engineering, Shiraz University, Shiraz, Iran

²Department of Mechanical Engineering, School of Engineering, Islamic Azad University, Shiraz Branch, Iran

(Received 29 October 2016; accepted 2 February 2017)

The silver (Ag) powder was synthesized in a mechanochemical (MC) process by inducing a solid-state displacement reaction between silver chloride (AgCl) and copper (Cu). This process was carried out in argon atmosphere conditions using a planetary ball mill. The reaction caused the mixture of AgCl and Cu to change the composition of the mixture to Ag and copper chloride (CuCl). CuCl was separated from MC product by leaching with ammonium hydroxide. Thus, Ag powder was obtained as the final product. Stearic acid (C₁₈H₃₆O₂) was used as the additive to improve dispersion of Ag powder during the MC process. The ground powders, formed in the presence and absence of additive, were characterized by X-ray diffraction (XRD) and scanning electron microscope (SEM). The XRD determined that the reaction between AgCl and Cu was completed in 18 h milling. SEM and particle size analysis examinations revealed that the size of the particles in the synthesized metallic Ag powder was in the range of 30–300 nm. © 2017 International Centre for Diffraction Data. [doi:10.1017/S0885715617000203]

Key words: silver powder, mechanochemical processing, solid-state displacement reaction, stearic acid

I. INTRODUCTION

Silver (Ag) powder has been extensively applied in the electronic industry over the last three decades, particularly in the preparation of conducting inks and paste for thin/thick films. Conductive Ag paste forms the basis for electronic components such as hybrid microcircuits and the internal electrodes of multi-layer ceramic capacitors. A specific morphological feature of Ag powder is needed for such applications. The powders should be composed of crystalline non-agglomerated micron/submicron particles with a narrow size distribution (Sinha and Sharma, 2005). To date, the preparation of Ag powder has involved many routes, such as chemical reduction of Ag ions on aqueous solution with or without stabilizing agents (Chou and Ren, 2000; Nersisyan *et al.*, 2003; Sondi *et al.*, 2003), radiation chemical reduction (Wu *et al.*, 1997), polyol method, physical and electrochemical processes, and each of these processes generates Ag powder with unique morphological properties. Among these methods, the mechanochemical (MC) process because of the low cost and simplicity is highly regarded (Keskinen *et al.*, 2001; Lee *et al.*, 2006). The main purpose of this investigation is to make a comparative study of the morphological characteristics of fine Ag powder prepared by MC reactions in the presence and absence of an additive, i.e. stearic acid.

II. EXPERIMENTAL PROCEDURE

All the experiments were carried out by taking analytical grade AgCl (purity, >99%, <100 μm) (Fluka Chemical Co.) and Cu (purity: >99.9%, <100 μm) (Merck Chemical Co.) as starting materials. To prevent agglomeration, 1 wt.% stearic acid was added to the initial powders. The two starting materials were mixed at equivalent molar ratio, and the mixture was kept in a desiccator. A high-energy ball milling Fritsch P-5 planetary mill (Fritsch, IdarOberstein, Germany) using stainless steel containers and balls of different diameters was used for grinding the mixture. The mixture was subjected to grinding in argon atmosphere at rotation speed of 400 rpm and ball-to-powder ratio (BPR) of 20 for different times: 9, 12, 15, and 18 h. Leaching treatment of the ground samples was carried out with NH₃ (aq). One gram of the ground sample was dispersed in 100 ml of 1.0 M NH₃ (aq) and the slurry was stirred by a magnetic bar to extract Ag from CuCl in the ground mixture. After leaching, it was filtered to separate solid phase from slurry by using membrane filter (cellulose acetate, pore size 0.2 μm, Advance MFS Inc., Japan). The solid phase was analyzed by a Philips diffractometer (30 kV and 25 mA) with CuKα₁ radiation (λ = 1.5404 Å). All X-ray diffraction (XRD) experiments were performed with a step size of 0.05° and a time per step of 1 s. The recorded XRD patterns were used for the calculation of crystallite size. Prior to calculations from the XRD peaks, the background was automatically removed and the Kα₂ radiation was stripped from the scans using the computer software Xpert High Score developed by PANalytical B.V. Company. The morphology of Ag powder prepared in this investigation was observed by scanning electron microscopy (SEM).

a)Author to whom correspondence should be addressed. Electronic mail: behruz.khakan@yahoo.com, eng.khakan@gmail.com

*List of authors has been corrected to include Ahmad Afsari since original publication. An erratum notice detailing this change as well as a correction to affiliations was also published and appears in this issue (doi:10.1017/S088571561700063X).

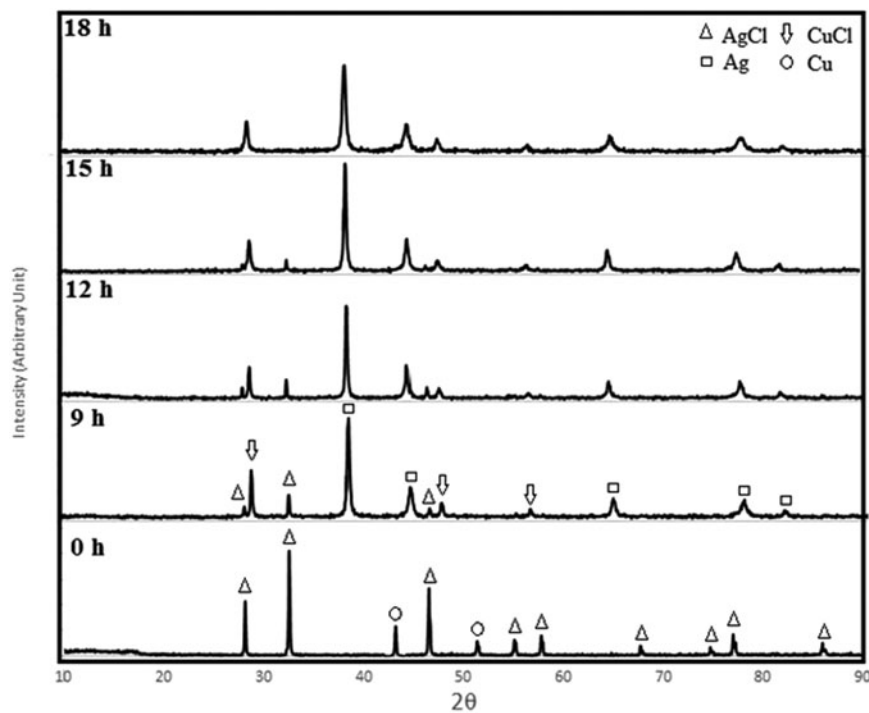


Figure 1. XRD patterns of AgCl + Cu mixture ground for different milling times.

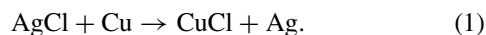
TABLE I. Milling conditions of the samples.

Sample	Milling time (h)	Additive (wt.%)	Atmosphere of milling	BPR	Speed (rpm)
1	18	–	Ar	20:1	400
2	18	1	Ar	20:1	400

III. RESULTS AND DISCUSSION

A. Characterization of time effects on the MC reaction

The XRD patterns of the mixture of AgCl and Cu, for different milling times in the absence of additive (stearic acid) are shown in Figure 1. The displacement reaction during the synthesis can be written as:



According to Figure 1, it is observed that the appearance of Ag and CuCl in the final ground mixture after 9 h of milling reveals that the displacement reaction has partially taken place during the MC process. With the increase of milling time to 18 h, the diffraction peaks of remaining AgCl and Cu are completely disappeared, and only the diffraction peaks of crystalline Ag and CuCl exist in the pattern.

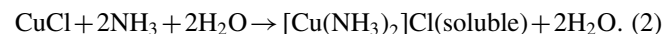
B. Effect of additive on the MC reaction

To determine the effect of additive, two samples were prepared with similar milling conditions. Table I summarizes the milling conditions. As seen in Figure 2, when stearic acid added as an additive in the starting materials, after 18 h of milling, AgCl in the final ground mixture [Figure 2(b)] was observed. This represents the role of stearic acid in controlling MC reaction. The stearic acid that is absorbed on the surface of the particles helps the cold-welding and agglomeration processes. Because the cold-welding process is an essential requirement to the progress of

MC reaction, through decreasing cold welding, the reaction rate is slowed. Accordingly, the reaction in the presence of stearic acid needs more time to be completed (Lü and Lai, 1998).

C. Characterization of powder sample after leaching

Leaching process formed a single phase of Ag in the residue. The process can be explained by the following reaction (Prakash *et al.*, 2000):



In the presence of additive, the small remnant of AgCl presents in the mixture reacted with NH_3 (aq) during the leaching process and formed the following complex (Prakash *et al.*, 2000):

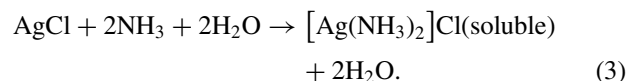


Figure 3 shows the XRD pattern of the separated Ag powder from liquid during the leaching process. The diffraction peaks correspond to the (111), (200), (220), (311), and (222) planes, respectively. All reflections on the XRD pattern can be indexed to a face centered cubic (fcc) structure according to the literature pattern (JCPDS, file no. 04-0783). The peaks in Figure 3 show the existence of Ag only.

Thus, it confirmed that the material synthesized during the leaching process is pure Ag powder. The broadening of the pattern peaks correlates to the fineness of the Ag crystallite. The crystallite size of the powder was calculated by line broadening of (111) peak of the XRD pattern using Scherrer's formula:

$$\text{Crystallite size} = \frac{0.9\lambda}{\beta \cdot \cos \theta}. \quad (4)$$

The width β is usually measured in radians, at intensity equal to half the maximum intensity. The crystallite size of

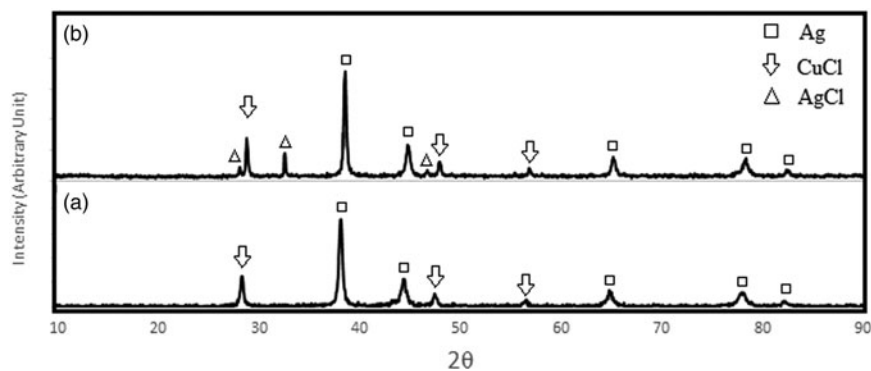


Figure 2. XRD patterns of AgCl+Cu mixture ground for 18 h (a) without additive, (b) stearic acid additive.

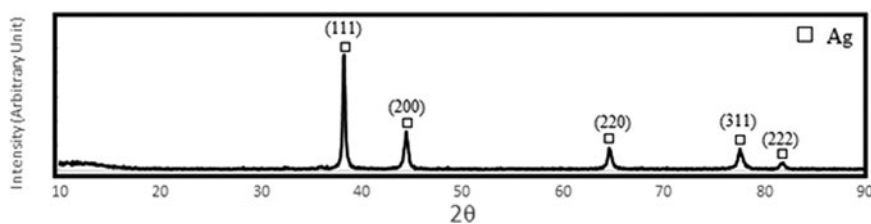


Figure 3. XRD patterns of AgCl+Cu mixture ground for 18 h after leaching by NH_3 (aq) solution.

TABLE II. Crystallite size of Ag particles in samples 1 and 2.

Sample	Crystallite size (nm)
1	46
2	38

Ag particles in samples 1 and 2 are presented in Table II. As seen in the table, the crystallite size is decreased by addition of stearic acid. The larger crystallite size of sample 1 could be because of the relatively higher temperature existed during milling in the absence of stearic acid. Enhanced lubrication is believed to reduce the local temperature during collisions.

The SEM photomicrographs of the Ag powder are shown in Figure 4. It is observed that the morphology of the powder

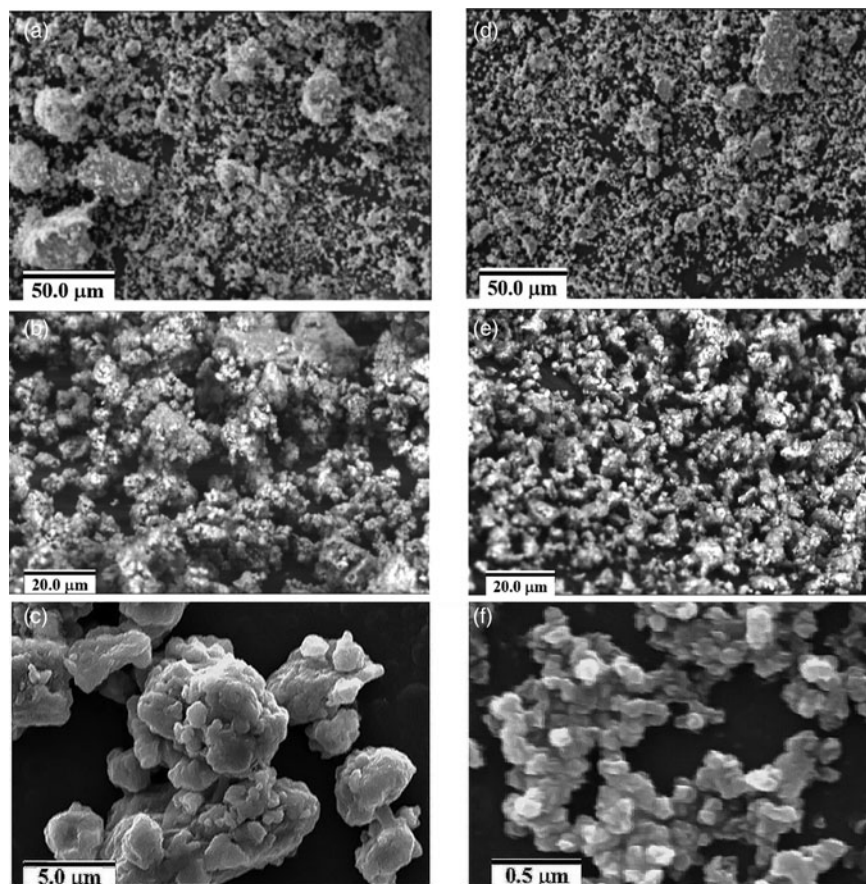


Figure 4. SEM images of Ag powders formed (a)–(c) without additive and (d)–(f) stearic acid additive.

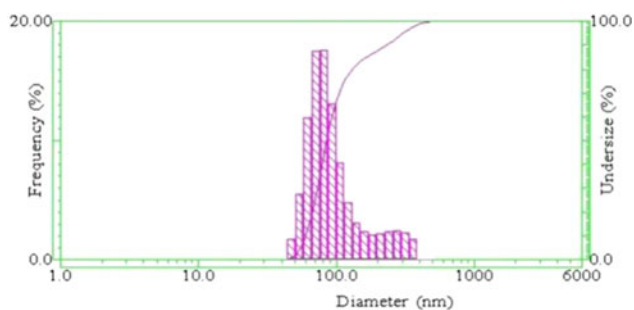


Figure 5. (Color online) PSA diagram for Ag powder in the presence of stearic acid as additive.

processed in the presence of stearic acid differed considerably from that of processed without stearic acid. Figures 4(a)–4(c) show the photomicrographs of the powder prepared without additive in the different magnifications. This reveals that the particles have densely agglomerated and it is difficult to distinguish between them clearly. The formation of large particles may be attributed to Ag and its fcc crystal structure in which particles are easily deformed and cold welded to each other to form large agglomerates (Shaw *et al.*, 2003). Figures 4(d)–4(f) show the photomicrographs of the Ag powder prepared using stearic acid additive in different magnifications. The powder is more dispersive than the sample without additive and the size of particles remain in the range of 30–300 nm. It seems that by addition of stearic acid, the cold-welding process is suppressed.

SEM images in Figure 4 suggest that addition of stearic acid plays an important role during Ag nanoparticle synthesis. This additive behaves as a dispersant in the MC process because of the possibility of the formation of an outer-sphere or a surrounding layer of stearic acid that covers the dispersed Ag particles in the mixture. This helps to prevent the agglomeration of the Ag particles.

Figure 5 shows results of particle size analysis (PSA) for Ag powder in the presence of stearic acid as additive. It can be observed that the size of particles remains in the range of 30–300 nm and verifies the SEM photomicrographs, also according to the diagram the average size of particles is 85.4 nm.

IV. CONCLUSIONS

Silver nanoparticles were synthesized by the MC process with AgCl and Cu as starting materials and the reaction was carried out in the absence and presence of stearic acid as additive. It was found by the XRD analysis that the addition of stearic acid alters the behavior of reactants significantly during the mechanical milling and delays the displacement reaction also. The SEM photomicrographs and PSA data reveal the effective nature of stearic acid in formation of silver nanoparticles during the MC process. Using stearic acid efficiently reduced the particle size of Ag by the suppression of excessive cold welding and led to formation of more dispersed Ag nanoparticles with the range of 30–300 nm. In the absence of stearic acid, the particles densely agglomerated, as the size of particles was roughly more than 1000 nm.

- Chou, K. S. and Ren, C. Y. (2000). "Synthesis of nanosized silver particles by chemical reduction method", *Mater. Chem. Phys.* **64**, 241–246.
- Keskinen, J., Ruuskanen, P., Karttunen, M., and Hannula, S. P. (2001). "Synthesis of silver powder using a mechanochemical process", *Appl. Organometal. Chem.* **15**, 393–395.
- Lee, J., Ahn, J. G., Tung, L. M., Kim, D. J., Kim, C. O., Chung, H. S., and Kim, B. G. (2006). "Preparation of Ag powders by mechanochemical reaction in AgCl–Cu system", *TMS Lett.* **3**, 41–42.
- Lü, L. and Lai, M. O. (1998) *Mechanical Alloying* (Springer Science & Business Media, Springer, New York), pp. 30–40.
- Nersisyan, H. H., Lee, J. H., Son, H. T., Won, C. W., and Meang, D. Y. (2003). "A new and effective chemical reduction method for preparation of nanosized silver powder and colloid dispersion", *Mater. Res. Bull.* **38**, 949–956.
- Prakash, S., Tuli, G. D., Basu, S. K., and Madan, R. D. (2000). *Advanced Inorganic Chemistry* (S. Chand & Co Ltd, India), **Vol. 1**.
- Shaw, L., Zawrah, M., Villegas, J., Luo, H., and Miracle, D. (2003). "Effects of process-control agents on mechanical alloying of nanostructured aluminum alloys", *Metall. Mater. Trans. A* **34**, 159–170.
- Sinha, A. and Sharma, B. P. (2005). "Preparation of silver powder through glycerol process", *Bull. Mater. Sci.* **28**, 213–217.
- Sondi, I., Goia, D. V., and Matijevic, E. (2003). "Preparation of highly concentrated stable dispersions of uniform silver nanoparticles", *J. Colloid Interface Sci.* **260**, 75–81.
- Wu, H., Xu, X., Ge, X., and Zhang, Z. (1997). "Preparation of silver nanocrystals in microemulsion by the γ -radiation method", *Radiat. Phys. Chem.* **50**, 585–588.