

Using Porcelain Replicas for Precision Control in Flintknapping Experiments

Charles A. Speer

Here I present a “how-to” guide to produce accurate copies of lithic artifacts for use in experimental studies that require large numbers of nearly identical copies. This method evolved from research questions about knappers’ failure rates at the fluting stage of Folsom projectile point production. It became apparent that it would be an expensive and long-term process to create hundreds of lithic replicas. The new method presented here is not a replacement for other traditional approaches to answering critical questions in experimental lithic studies such as raw material selection, decision-making, and skill assess-

ment, among others. It is, however, an alternative strategy to assess numerical and mechanical questions about flake morphology and breakage patterns affiliated with successful and unsuccessful strikes and to possibly provide alternative approaches to gauging skill level at particular stages in flintknapping. The subjectivity of the researcher and the knapper is kept to a minimum through enhanced control when certain observable criteria are desired. The method presented here is one approach of many to answer specific questions that concern lithic production experiments (Marsh and Ferguson 2010).

ABSTRACT

The experimental replication of lithic artifacts occasionally encounters issues of standardization and control. Two major issues are how to accurately create a large sample population and how to sample from specific stages over the flaking process. Knappable stone is unpredictable due to inclusions, cracks, and differences in size, texture, and fracture toughness. While this aspect of stone is critical to understanding some aspects of human behavior, decision-making, and skill assessment, in some experimental studies it may hinder other areas. Research for a large study assessing the failure of Folsom preforms during the fluting stage required many knappable facsimiles. The process outlined here uses porcelain as a medium for tackling these requirements. The new method presented here illustrates how a 3-D scanner and printer can be used to record and produce a copy of the artifact form. It then describes how to create a plaster mold of the printed artifact form and, finally, how to cast and fire the artifact replica in porcelain.

La replicación experimental de artefactos líticos ocasionalmente encuentra problemas de estandarización y control. Dos cuestiones importantes son cómo crear con precisión una gran población de muestra y cómo muestrear de etapas específicas sobre el proceso de descamación. Knappable piedra es impredecible debido a inclusiones, grietas y diferencias en tamaño, textura y tenacidad a la fractura. Si bien este aspecto de la piedra es fundamental para comprender algunos aspectos del comportamiento humano, la toma de decisiones y la evaluación de habilidades en algunos estudios experimentales, puede obstaculizar otras áreas. La investigación para un gran estudio que evaluó el fracaso de las preformas de Folsom durante la etapa de estría requirió muchos facsimiles knappable. El proceso descrito aquí utiliza la porcelana como medio para abordar estos requisitos. El nuevo método presentado aquí ilustra cómo se puede utilizar un escáner 3D e impresora para grabar y producir una copia del formulario del artefacto. A continuación, se describe cómo crear un molde de yeso de la forma de artefacto impreso, y luego, por último, cómo arrojar y disparar la réplica de artefacto en porcelana.

Advances in Archaeological Practice 6(1), 2018, pp. 72–81
Copyright 2017 © Society for American Archaeology
DOI:10.1017/aap.2017.30



FIGURE 1. Folsom preform from Big Black site, North Dakota. Photo courtesy of Robert Lassen.

BACKGROUND

Flintknapping is an irrevocable process of reduction. While similarities in form, debitage, and process can be re-created experimentally, the archaeological form in the *chaîne opératoire* is approximated (Andrefsky 2005). By sharing a process for creating nearly identical lithic tool facsimiles, this article provides a new method for engaging experimental studies in lithic production. This method attempts to eliminate some of the inconsistencies in experimental knapping when specific stages need to be recorded or the production of a large sample population is not feasible with traditional approaches. Advantages of this new method over traditional approaches to flintknapping experiments include allowing the flaking of highly precise facsimiles of actual artifacts; the recording and replication of critical stages in the reduction process, such as creating a Folsom preform ready for fluting (see Figure 1); and the production of a large number of these precise replicas at a relatively low cost. The methods described here obtain optimum reproduction of surface details and similarity in size by using a Cone 10 porcelain slip. The use

of porcelain as a proxy substrate for knapping has been presented by previous researchers (Khreisheh, Davies, and Bradley 2013; Tsirk 2014) and will be discussed in terms of its mechanical properties in relation to knappable stone used in prehistory. Porcelain is used for experimental lithic studies because of its fracture toughness values and because it is comparable to some materials used in prehistory, in historical contexts, and in modern flintknapping. The reasons this method can be useful are presented below and will be followed by the “how-to” section describing accurate porcelain replica production.

Control in experimental archaeology can be difficult to maintain in a project due to the nature of the materials used in the experimental process. Some questions about lithic production are challenging to examine because of the heterogeneity of naturally occurring raw materials such as agate, chert/flint, jasper, obsidian, and quartzite. These raw materials typically contain internal structural differences in the form of cracks and inclusions (Luedtke and Meyers 1992). Even raw materials from the same outcrop can have textural, size, and fracture toughness differences. These factors can create different sets of debitage during the reduction process and may require alternative approaches and/or skill levels to reduce to the same final form (see Figure 2; Rezek et al. 2011). There is utility to being able to isolate and control as many variables as possible in an experiment to observe a specific phenomenon (Bernard 2006; Gerber and Green 2012; Klaus and Kempthorne 1993).

For flintknapping experimentation, in particular, the ability to record and reproduce the incident form can potentially answer questions concerning skill level at some stages in the reduction process. There could be many opportunities to explore the stages of reduction found at lithic workshops, such as at the Clovis-period workshop found at the Gault site (Bradley et al. 2010). Additionally, precision control can provide discernment of the subsystems that interact with lithics, namely, antler, bone, and wood (Bello et al. 2013). This precision control may allow us to observe how various subsystems create different flake patterns and debitage at critical stages in terms of those materials that react similarly to porcelain.

The criteria for knapping are met when using porcelain, as it can be flaked conchoidally as well as being isotropic, brittle, and elastic. However, even the use of porcelain must be employed with caution, per the following:

While porcelain may be usefully applied in most experiments, there are some occasions where it cannot be substituted. For example, experiments investigating the properties of specific material types, such as the effects of heat treating upon various flints, can only be conducted using those specific materials. While the fracture properties of porcelain are similar to flint, it is not a perfect replica of any individual material type, which can be highly variable [Khreisheh, Davies, and Bradley 2013:44].

The problem encountered by many researchers exploring other materials is the difficulty in creating a consistent starting point for experiments. In the past, the process has relied on making simple forms and pressing either porcelain clay or slumping glass into a mold (Dibble and Rezek 2009). This produces several problems. While these forms are very useful for creating a supply of raw



FIGURE 2. Set of errors that would be difficult to re-create exactly using traditional experimental knapping techniques.

material, they cannot provide the detailed surface morphology required to create a standard from any stage in the knapping process—that is, other than a simple form. In fact, it has been stated that “because each core surface varies in an infinite number of ways due to its own, unique, reduction history, it is virtually impossible to design experiments with cores having identical surface characteristics” (Rezek et al. 2011:1346). Furthermore, the method described here can anticipate the shrinkage of the ceramic slip material and adjust the model appropriately. Thus, the method presented here with porcelain slip employed as a medium can allow for highly detailed replication of surface characteristics.

MATERIALS

The methods presented here used both a μ -CT scanner and a scanning arm to record the artifact form for comparative purposes; two 3-D printers, also used for comparative purposes; numerous plaster molding techniques; and finally, casting, production, and firing of the artifact form from several porcelain slips of different firing temperatures. The plaster used for the production of the molds was a generic USG No. 1 pottery plaster. The porcelain slip used was a Cone 10 high-fire porcelain that is completely vitrified at 1,340°C (2,444°F). The porcelain used adheres to the industry standard composition of 25% pure kaolin, 25% ball clay, 25% feldspar, and 25% flint. Early experiments used a Cone 5 porcelain slip that was used for the production of doll faces; however, it failed to capture surface details and was prone to a greater incidence of step fractures. All of the porcelain casts produced for this project were fired in a Cone 10 digital electric kiln.

The properties of Cone 10 porcelain are comparable to those of other knappable materials as shown in Table 1. Porcelain-

TABLE 1. Fracture Toughness Values of Quartz-Based Materials.

Material	Fracture Toughness (K_{IC} (MPa $m^{1/2}$))	Grain Morphology
Agate, banded	1.8	0.02 mm by 0.1 mm, acicular
Raw Edwards Plateau chert	1.7	0.01 mm to 0.02 mm, equidimensional
Porcelain	1.5	0.05 mm to 0.01 mm, acicular
Flint	1.4	0.005 mm to 0.01 mm, equidimensional
Heat-treated Edwards Plateau chert (350°C)	1.4	0.01 mm to 0.02 mm, equidimensional
Chalcedony, nonbanded	1.3	0.02 mm by 0.1 mm, acicular
Fused quartz	0.7	Amorphous
Wood opal	0.7	Amorphous
Tigereye	0.7	0.08 mm by 10 mm, acicular
Aventurine	0.6	0.1 mm to 0.5 equidimensional quartz; 0.4 mm by 0.4 mm by 0.4 mm mica

like materials were used in prehistory, such as porcellanite, fine quartzites, novaculite, and others (Bamforth 2006; Etchieson and Trubitt 2013; Fredlund 1976; Morgenstein 2006; Saul 1969). Even today, many modern flintknappers use what is often called



FIGURE 3. Folsom chert preform replicas; the preform on the right is used to describe the method given here. It is made from a black variety of Edwards Plateau chert.

TABLE 2. Fracture Toughness of Porcelain with Same Composition.

Sample #	Fracture Toughness (K_{Ic} (MPa m ^{1/2}))
1	1.51
2	1.57
3	1.71
4	1.62
5	1.51
6	1.33
7	1.49
8	2.09
9	1.50
10	1.56

Source: Adapted from Bragança and Bergmann 2003:804.

“johnstone,” or discarded toilet bowl porcelain, to knap highly complex forms (Whittaker 1994:68). Australian Aborigines were known to climb telegraph lines to retrieve porcelain insulators in the late nineteenth and early twentieth centuries, as well (Harrison 2006).

Values for raw and heated Edwards Plateau chert fracture toughness were experimentally derived using a Vickers microhardness tester and a universal testing machine (Speer 2010:166). The other fracture toughness values and grain morphology were derived from multiple sources, and the values for porcelain in Table 2 are derived from multiple tests of the same porcelain composition as in this experiment, also fired to 1,340°C (2,444°F; Bragança and Bergmann 2003; Carty and Senapati 1998; Wood and Weidlich 1982).

METHODS

The primary objective of this research is to provide a method to re-create exact stages during the reduction process as well as to create unlimited, accurate experimental replicas. Even when a researcher uses a glass or porcelain preform, after the first strike, the experiment deviates due to individual skill and circumstance. The secondary objective of this research is to provide a method to engage the archaeological record directly by exploitation of artifacts themselves without damage. In order to re-create the same morphology of the artifact form at any point in the reduction process, this “how-to” method is presented below in several steps. Ten Folsom chert preforms were created by an expert flintknapper for the major flintknapping experiment that this method was designed to demonstrate. The preform used to document the process is presented in Figure 3.

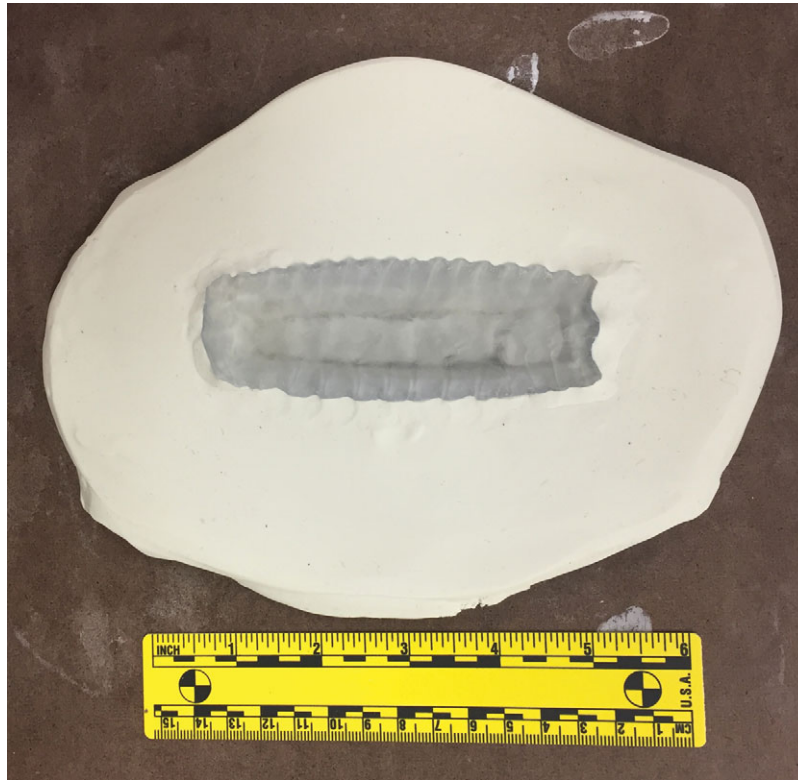


FIGURE 4. 3-D model encased in clay up to the midline. An area was hollowed out to allow ideal fit, and a small bead of clay was laid below the model for support.

Scanning and Printing

In order to begin the process, first a 3-D scan of the lithic artifact was recorded using a μ -CT scanner (also used to scan for internal material flaws). A scan arm or other 3-D scanner may also be used for this 3-D scan process with appropriate resolution for specific research questions. The μ -CT scanner has an accuracy of sub-micron levels, while the scan arm used had an accuracy of $\pm 25 \mu\text{m}$ (0.001 inches). This difference represented a trade-off between speed of scan and accuracy. The μ -CT scanner requires a specialized operator and can take several hours to get high-quality scans. Additionally, the cost of the μ -CT scanner is nearly 10 times the cost of the scan arm. For the μ -CT scanner any format can be exported directly, and there is little to no postprocessing. The detailed models are merged using proprietary software, and export is fairly simple.

The maximum settings of the scan arm allowed for optimal capture of surface features. The scan arm was used for early-stages recording of the artifact shown in Figure 3 before trying other methods. The scan arm used has a rapid scan rate of 280 frames per second at around 2,000 points per line (or 560,000 points per second), with an accuracy of $\pm 25 \mu\text{m}$. The scans were imported into a 3-D metrology software program, and then scans from each pass were grouped. Both sides of the model were pre-aligned and then oriented and meshed. The alignment of the model was optimized using overlapping scans, and a point cloud was produced using proprietary software. A polygonal model was then rendered from the point cloud data. The polygonal model was cleaned; holes were filled as necessary, and/or areas not cap-

tured were rescanned. For the model presented, the scans took approximately 10 minutes, while the postprocessing took around an hour and a half.

The model data from the scans performed by both instruments were transferred to two different 3-D printers. Each model was printed in proprietary materials that come from a family of rigid photopolymers that provide excellent detail visualization, durability, and strength. The technique used to print the models was PolyJet 3-D printing. This is similar to inkjet document printing, but instead of jetting drops of ink onto paper, the 3-D printer jets layers of liquid photopolymer onto a build tray and cures them with ultraviolet light. The layers build up one at a time to create a 3-D model at a maximum resolution of $16 \mu\text{m}$ (0.0006 inches). The models were printed in several varieties of print material at maximum settings to determine which had the appropriate characteristics and resolution for mold-making. It became evident that most of these print mediums could not reach the appropriate level of resolution. It was determined that a clear, even-dispersing photopolymer, which simulates a standard plastic transparent material, was ideal. Fully cured models can be handled and used immediately, without additional postcuring.

The total printing time for the Folsom preform was 6 or 11 hours depending on the model of 3-D printer used. There was no noticeable difference in the print quality between the two printers other than the time it took to build. The time difference is likely due to the size of the build trays. The smaller printer had

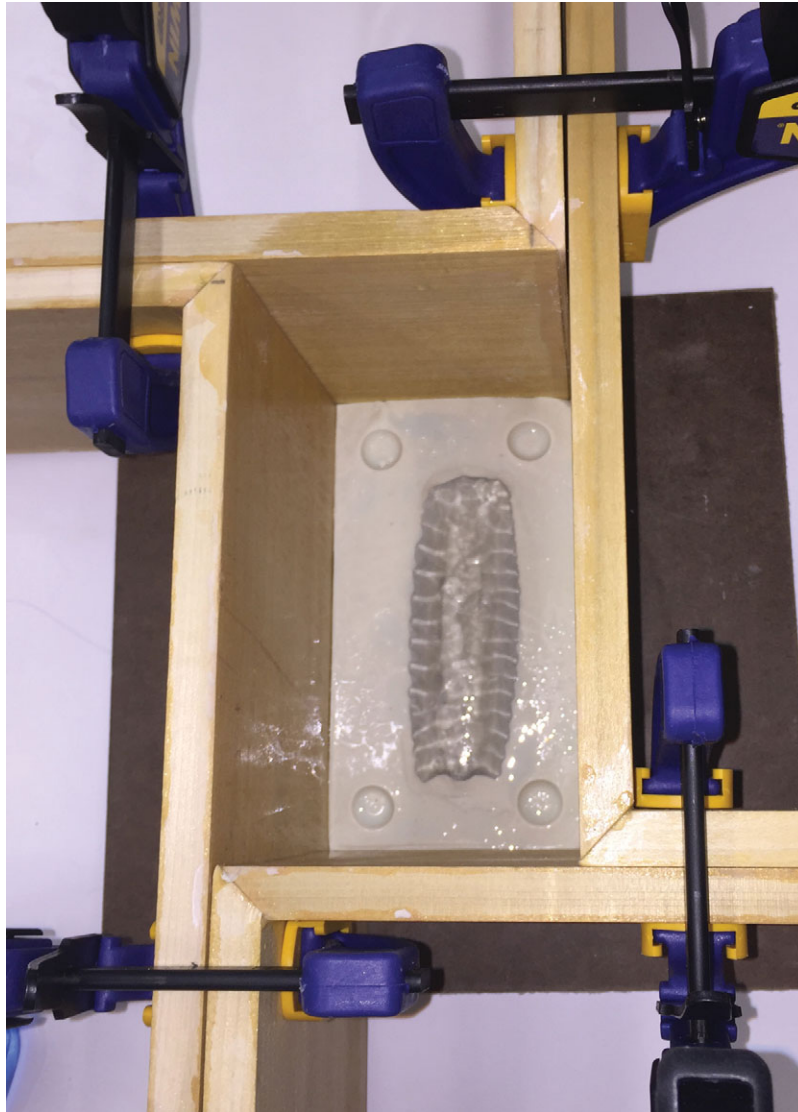


FIGURE 5. 3-D model enclosed in cottle boards with a release agent sprayed on the surface.

a build tray of $294 \times 192 \times 148.6$ mm, and the large printer had a build tray of $490 \times 390 \times 200$ mm. Therefore, the larger of the two printers would take longer to sweep across the build tray each time.

Molding and Casting

An issue that had to be resolved in order to obtain ~100% accuracy of the porcelain casts was that the porcelain used in this method shrank at a rate of ~14.5% when dried and fired. In order to overcome this, it was necessary to print out a 3-D model ~116.96% the size of the original artifact. For the initial mold production, the 3-D model was encased in clay up to the midline of the 3-D biface model (see Figure 4). Key impressions were made to align both sides of the mold. The 3-D model and clay were then coated with a release agent. The clay base was enclosed in cottle boards (see Figure 5). A fine and sifted plaster was mixed with water and poured over the top of the 3-D model. After the

plaster dried, the mold was released from the cottle boards and separated from the model.

For the second stage of mold production, the first half of the mold was flipped over, and the 3-D model was seated in its negative space. The 3-D model was again coated with a release agent as well as the plaster mold. Both were enclosed in cottle boards, and mixed plaster was poured over the surface. After the plaster dried, the second half of the mold was released from the cottle boards and separated from the model. After both sides of the plaster mold were fully dried and cured, casting could begin.

Casting and Firing

Both sides of the plaster casts of the 3-D model were joined together and held tightly with large rubber bands. A fine Ferro-filtered Cone 10 porcelain slip was mixed and poured into the mold fill hole (~6 mm) that was drilled in the opposite side, along



FIGURE 6. Mold being filled with porcelain slip. Note the air hole at the right in between rubber bands.

with a small (~2 mm) air hole (Figure 6). There are several options available for the filling of a mold. A cone-shaped piece of clay can be formed at the beginning of the mold-making process and filled from one end, or a hole can be drilled into the plaster on whichever side that will not be (or will be least) affected by experimentation. For larger objects, the cone fill hole appears to work better. For smaller items, the drill method seems to work better and has fewer issues of cavitation of the slip and air pockets being trapped in the form. These small fill holes can easily be cleaned up and blended in by hand on flat surfaces of the original. This depends on the specific experiment at hand. The fill hole must be topped off, as the moisture is absorbed by the plaster.

After sufficient drying was allowed, the mold was opened carefully, and the porcelain cast was removed and allowed to fully dry. In between castings, the plaster must be allowed to dry before proceeding. After the porcelain casts were bone dry, they were then loaded into an electric kiln and fired to Cone 10 (1,340°C [2,444°F]). After the porcelain casts cooled, they were ready to be knapped for experimentation.

RESULTS

Lithic replication experiments produce tools and debitage that may be the result of individual variation and raw material

inconsistencies. The method presented here can provide new and exciting avenues of research to explore how and to what extent those variations and inconsistencies affect not only experimental results but also the tools and debitage of the archaeological record. The next question that arises is, how accurate is the porcelain replica in comparison with the original artifact? To answer this question, it was necessary to return to using the 3-D scanner. Scans of the artifact and scans of the porcelain replica were both taken and processed. These two scans were then imported into a proprietary 3-D software program that allowed for reverse engineering of parts and comparison of production models. The results are shown in Figure 7.

The postanalysis of the method was extremely useful because it highlights certain processes that were going on inside of the plaster mold. The 3-D deviation in Figure 7 represents high spots shifting toward the red end of the spectrum and low spots shifting toward blue and purple. The maximum deviations for this first model overall were 0.8540 mm and -0.9416 mm. The standard deviation was 0.2192 mm, with average deviations of 0.1065 mm and -0.2806 mm. What this illustrates is that the mold was not dry enough in some areas as opposed to others, which highlights the need for a completely dry plaster mold prior to casting. In addition, it also shows that the fill hole needed to be coated in wax prior to casting, as it was removing too much moisture from

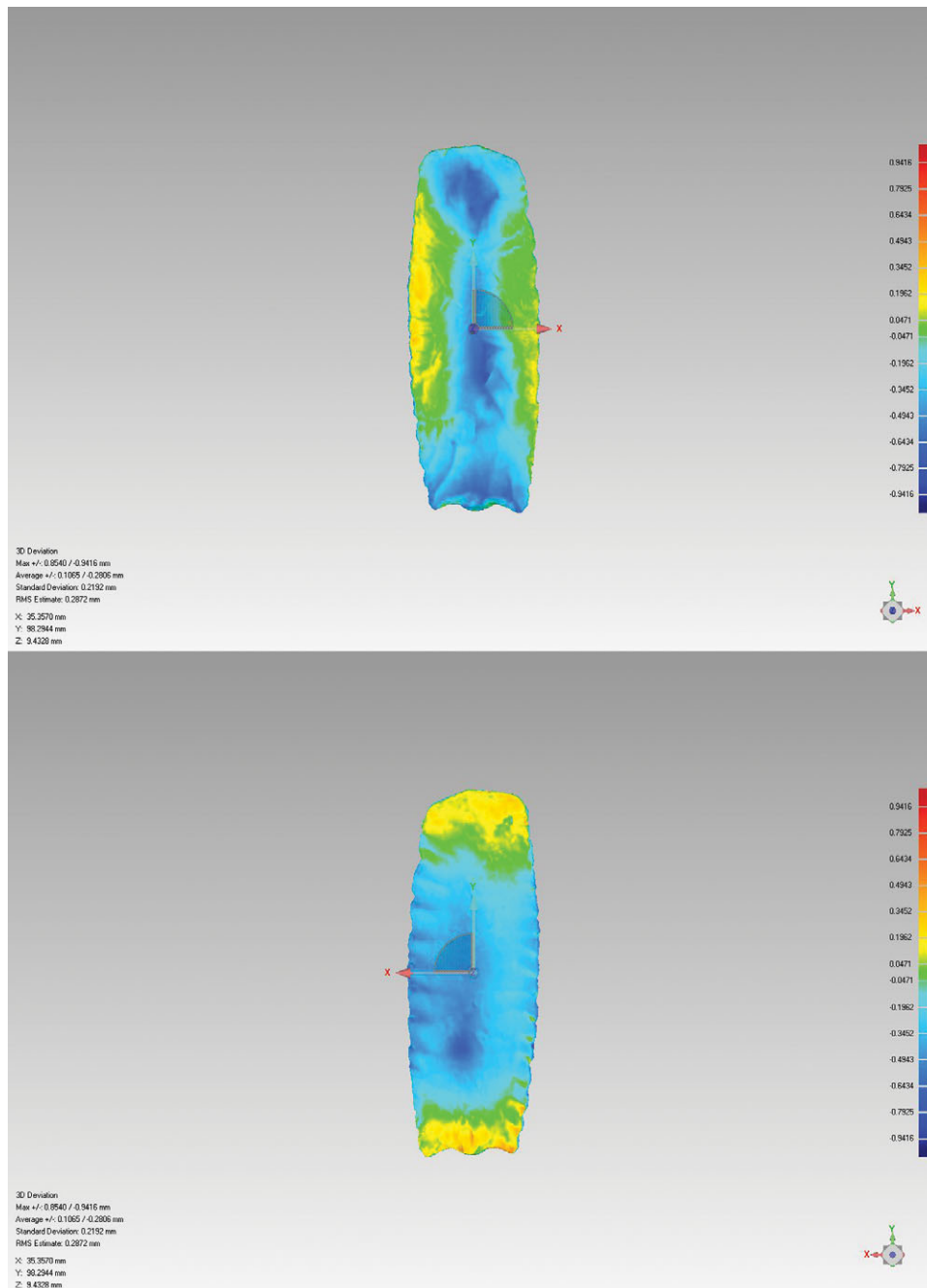


FIGURE 7. Results comparing the original artifact with an early porcelain cast. The base model is the original artifact, and the color variation is the difference of the porcelain replica. The green color is nearly exact to the original.

the porcelain. A postanalysis is highly recommended for improving the accuracy of final casts.

DISCUSSION

The fracture properties of Cone 10 porcelain make it an ideal (and cheap) substitute for other materials (see [Table 1](#)). As mentioned, Cone 10 porcelain is brittle, elastic, homogeneous, and

isotropic and fractures conchoidally (Khreisheh, Davies, and Bradley 2013). Many new research topics can be explored with this method in experimental archaeology. The precision with which every step can be documented, replicated, and tested an unlimited number of times can potentially allow new insights into difficult experimental studies in stone tool production. Skill level can be assessed among knappers more accurately as raw material constraints are removed; various steps or stages can be focused on, and there is no lack of raw material. It is



FIGURE 8. From left to right: original chert Folsom preform; porcelain replica; and 3-D print at 116.96% the size of the original.

possible using this method to essentially “pause” at a step and use multiple approaches to remove a critical flake, such as a fluting or channel flake. At any stage in the process the knapper can stop, scan and print the experimental form, make porcelain casts, and then see how different techniques alter the morphology of the form (see Figure 8). The specific research question can be answered from many different approaches. This method offers another tool for experimental flintknapping researchers to use in conjunction with other techniques.

CONCLUSIONS

There are several drawbacks to achieving the same quality of results for the methods shown. The first is that in order to achieve the optimal level of resolution for each reproduced lithic artifact, there is a high initial investment in equipment. The initial investment in a 3-D scanner may be anywhere from ~\$100,000 to \$1.2 million, and the printer can cost between \$60,000 and \$300,000. Cheaper 3-D scanners can be used, but this depends on the requirements of the experiment. In addition, the learning curve required to produce consistent and accurate molds and casts can be challenging. For some lithic forms there may be a serious issue of air pocket inclusion and cavitation of the porcelain slip in the mold. Further, the drying time for the

porcelain casts is approximately one–two weeks depending on thickness.

There are several solutions to all these drawbacks. A scan and model made of an artifact or experimental piece can be created by sending it to a company that specializes in 3-D scanning and printing. These will need to be carefully scrutinized to make sure that the optimum settings and materials were used for scanning and printing. For example, when the scan and print settings are above 120 μm , the flake arrises on the models become rounded off and not sharp to the touch, as would be felt on a lithic artifact. The methods presented here aim to assist researchers in answering questions requiring large sample populations and accurate, knappable copies of artifacts.

Acknowledgments

I would like to acknowledge and thank the Department of Anthropology, the College of Arts and Letters, and Dean Kandi Turley-Ames at Idaho State University for their purchase of the 3-D printer used in this research and the start-up funds that enabled the purchase of supplies. I would also like to acknowledge and thank all of the staff at the Grady Early Forensic Anthropology Laboratory at Texas State University for their assistance using the μ -CT scanner and other resources. I thank Jesse Pruitt

and Robert Schlader at the Idaho Virtualization Laboratory for assisting me with scanning and processing models and the students who assisted me over the course of this project with mold-making and casting, including Kayla Fuhrman, Daniel Parker, and Shanda Putnam. No permits were required for this work.

Data Availability Statement

All relevant data are contained within this essay.

REFERENCES CITED

- Andrefsky, W., Jr.
2005 *Lithics: Macroscopic Approaches to Analysis*. Cambridge: Manuals in Archaeology. Cambridge University Press, Cambridge.
- Bamforth, D. B.
2006 The Windy Ridge Quartzite Quarry: Hunter-Gatherer Mining and Hunter-Gatherer Land Use on the North American Continental Divide. *World Archaeology* 38(3):511–527.
- Bello, Silvia M., Simon A. Parfitt, Isabelle De Groote, and Gabrielle Kennaway
2013 Investigating Experimental Knapping Damage on an Antler Hammer: A Pilot-Study Using High-Resolution Imaging and Analytical Techniques. *Journal of Archaeological Science* 40:4528–4537.
- Bernard, H. Russell
2006 *Research Methods in Anthropology: Qualitative and Quantitative Approaches*. 4th ed. AltaMira Press, Lanham, Maryland.
- Bradley, Bruce A., Michael B. Collins, Andrew Hemmings, Marilyn Shoberg, and Jon C. Lohse
2010 *Clovis Technology*. Archaeological Series. International Monographs in Prehistory, Ann Arbor, Michigan.
- Bragança, S. R., and C. P. Bergmann
2003 A View of Whitewares Mechanical Strength and Microstructure. *Ceramics International* 29(7):801–806.
- Carty, William M., and Udayan Senapati
1998 Porcelain—Raw Materials, Processing, Phase Evolution, and Mechanical Behavior. *Journal of the American Ceramic Society* 81:3–20.
- Dibble, Harold L., and Zeljko Rezek
2009 Introducing a New Experimental Design for Controlled Studies of Flake Formation: Results for Exterior Platform Angle, Platform Depth, Angle of Blow, Velocity and Force. *Journal of Archaeological Science* 36:1945–1954.
- Etchieson, M., and M. B. Trubitt
2013 Taking It to the River: Arkansas Novaculite Quarrying and Archaic Period Tool Production. *North American Archaeologist* 34(4):387–407.
- Fredlund, Dale E.
1976 Fort Union Porcellanite and Fused Glass: Distinctive Lithic Materials of Coal Burn Origin on the Northern Plains. *Plains Anthropologist* 21(73):207–211.
- Gerber, Alan S., and Donald P. Green
2012 *Field Experiments: Design, Analysis, and Interpretation*. W. W. Norton, New York.
- Harrison, Rodney
2006 An Artefact of Colonial Desire? Kimberley Points and the Technologies of Enchantment. *Current Anthropology* 47(1):63–88.
- Khreisheh, Nada N., Danielle Davies, and Bruce A. Bradley
2013 Extending Experimental Control: The Use of Porcelain in Flaked Stone Experimentation. *Advances in Archaeological Practice* 1(1): 37–46.
- Klaus, Hinkelmann, and Oscar Kempthorne
1993 *Design and Analysis of Experiments, Volume 1: Introduction to Experimental Design*. 2nd ed. Wiley Series in Probability and Statistics 1. 3 vols. John Wiley and Sons, Hoboken, New Jersey.
- Luedtke, Barbara E., and J. T. Meyers
1992 *An Archaeologist's Guide to Chert and Flint*. Archaeological Research Tools 7. Institute of Archaeology, University of California, Los Angeles.
- Marsh, Erik J., and Jeffrey R. Ferguson
2010 Introduction. In *Designing Experimental Research in Archaeology: Examining Technology through Production and Use*, edited by J. R. Ferguson, pp. 1–12. University Press of Colorado, Boulder.
- Morgenstein, Maury
2006 Geochemical and Petrographic Approaches to Chert Tool Provenance Studies; Evidence from Two Western USA Holocene Archaeological Sites. *Geological Society Special Publications* 257:307–321.
- Rezek, Zeljko, Sam C. Lin, Radu Iovita, and Harold L. Dibble
2011 The Relative Effects of Core Surface Morphology on Flake Shape and Other Attributes. *Journal of Archaeological Science* 38(6):1346–1359.
- Saul, John M.
1969 Study of the Spanish Diggings, Aboriginal Flint Quarries of Southeastern Wyoming. *National Geographic Society Research Reports* 1964:183–199.
- Speer, Charles A.
2010 Understanding the Effects of Heat Treatment on Edwards Plateau Chert. *Ethnoarchaeology* 2(2):153–172.
- Tsirk, Are
2014 *Fractures in Knapping*. Archaeopress, Oxford.
- Whittaker, John C.
1994 *Flintknapping: Making and Understanding Stone Tools*. University of Texas Press, Austin.
- Wood, Michael M., and J. E. Weidlich
1982 Empirical Evaluation of Fracture Toughness: The Toughness of Quartz. *American Mineralogist* 67:1065–1068.

AUTHOR INFORMATION

Charles A. Speer ■ Department of Anthropology, Idaho State University, 921 South 8th Avenue, Pocatello, ID 83209–8005, USA (speechar@isu.edu)