Adaptive Measurement Model of Navigation by Stellar Refraction based on Multiple Models Switching

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In recent years, navigation by stellar refraction has received considerable attention, having advantages of high accuracy, simple construction, and low cost. Nevertheless, there are many limitations to the precision and application of this method using a traditional measurement model. This article studies the changing pattern of atmospheric density, the disturbed atmospheric density model and measurement model of stellar refraction ranging from 20 km to 50 km. Furthermore, a control algorithm of multiple mode switching and an adaptive measurement model are proposed. With this method, any refracted starlight from the scope of between 20 km and 50 km can be captured and the measurement model at the appropriate height can be automatically established. Due to this, the reliability and practicality of navigation have been raised considerably. Accuracy of navigation using the adaptive measurement method is observed to improve by about 14%, using computer simulation based on an Unscented Kalman Filter (UKF).

KEY WORDS

 1. Stellar refraction.
 2. Atmospheric density model.
 3. Adaptive measurement model.

 4. Multiple models switching.

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1. INTRODUCTION. In order to realize precise positioning of satellites, navigation by stellar refraction makes use of the relationship between the refraction angle and refraction height in the atmosphere, to sense the horizon indirectly and accurately with a high-precision CCD star sensor (second of arc) (Yang et al., 2010). Traditional navigation by stellar refraction is limited in application and its development is seriously held back due to the difficulty of selection of a refraction navigation star and the fixed height of 25 km in its measurement model (Gounley et al., 1984). This paper responds to these problems and proposes a measurement model that is based on multiple models switching, thus making sure that refracted starlight ranging from 20 km to 50 km can be captured accurately at its corresponding



Figure 1. Geometry of starlight refraction.

height. This is significant for improving the practical accuracy and applicability of navigation by stellar refraction.

2. GENERAL MEASUREMENT MODEL. Owing to the variety of atmospheric density, starlight will be refracted when passing through the spherically layered atmosphere (Lair and Duchon, 1988) as shown in Figure 1. This refraction is more intense if the starlight is closer to the earth's surface.

Supposing ρ_g is the atmospheric density at refraction height h_g , the relationship between refraction angle and refraction height can be given in Equation (1) as follows:

$$R = k(\lambda)\rho_g [2\pi (R_e + h_g)/H_B]^{1/2}$$
(1)

where *R* is refraction angle, H_B is the density scale height, R_e is earth radius and $k(\lambda)$ is the dispersion parameter which is only related to the wavelength λ .

Assuming that atmospheric density changes completely according to the index law, the density at refraction height h_g is given as follows:

$$\rho_g = \rho_0 \exp[-(h_g - h_0)/H_B] \tag{2}$$

where ρ_0 is the atmospheric density at the height h_0 .

Because R_e is much more than h_g , Equation (1) can be simplified as:

$$R \approx k(\lambda)\rho_{\sigma} [2\pi R_e/H_B]^{1/2}$$
(3)

Associating Equation (2) with Equation (3), Equation (4) is thus:

$$h_g = h_0 - H_B \ln(R) + H_B \ln[k(\lambda)\rho_0 (2\pi R_e/H_B)^{1/2}]$$
(4)

The relationship between apparent height h_a and refraction height h_g is as follows:

$$h_a = [1 + k(\lambda)\rho_g]h_g + k(\lambda)\rho_g R_e$$
(5)

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Associating Equation (4) with Equation (5), Equation (6) is thus:

$$h_a = h_0 - H_B \ln(R) + H_B \ln[k(\lambda)\rho_0 (2\pi R_e/H_B)^{1/2}] + R(H_B R_e/2\pi)^{1/2}$$
(6)

where H_B is the density scale height at 25 km. Therefore, Equation (6) is the measurement model of navigation by starlight refraction at 25 km.

3. DISTURBED ATMOSPHERIC DENSITY MODEL. The measurement model of navigation by stellar refraction is based on the atmospheric density model. The precision of the measurement model is closely related to the accuracy of the atmospheric density (Wang and Ma, 2009). Generally, the atmospheric density decreases exponentially with the increase of altitude, and it is influenced by solar activity, time, season, latitude, and geomagnetic activities, especially by season, latitude, and the random changing of atmospheric density. The variety of atmospheric density is defined as the deviation between real density and its standard, expressed as Equation (7):

$$\delta_{\rho} = (\rho - \rho_{CT}) / \rho_{CT} \tag{7}$$

where δ_{ρ} is the variety of atmospheric density; ρ is the real density; ρ_{CT} is the standard value.

3.1. Season and Latitude (Ji, 1995). The complexity of atmospheric density is mainly manifested in that the atmospheric density differs with time and place. The latitude and season are particularly important factors. During a year, the variety of atmospheric density, pressure, wind speed and other factors at the height from 0 km to 150 km is predictable, within certain limits. The mathematical model of variety of atmospheric density affected by season and latitude is as follows:

$$\delta_{\rho cm}(H, L, N) = K_0(H, M) + \sum_{i=1}^{6} K_i(H, M) L^i$$
(8)

where H is height; L is latitude; M is month. Other coefficients can be calculated as follows:

$$K_{0}(H, M) = \delta_{\rho cm1}(H, M)$$

$$K_{1}(H, M) = 0$$

$$K_{2}(H, M) = 0 \cdot 5n_{3}$$

$$K_{3}(H, M) = 0$$

$$K_{4}(H, M) = 8 \cdot 729n_{1} - 1 \cdot 489n_{2} - 1 \cdot 994n_{3}$$

$$K_{5}(H, M) = -11 \cdot 114n_{1} + 2 \cdot 523n_{2} + 2 \cdot 203n_{3}$$

$$K_{6}(H, M) = 3 \cdot 538n_{1} - 0 \cdot 936n_{2} - 0 \cdot 562n_{3}$$
(9)

In Equation (8), other parameters are as below:

$$n_{1} = \delta_{\rho cm2}(H, M) - \delta_{\rho cm1}(H, M)$$

$$n_{2} = \delta_{\rho cm3}(H, M) - \delta_{\rho cm1}(H, M)$$

$$n_{3} = -2u_{cm1}(H, M)[1 + \delta_{\rho cm1}(H, M)\omega_{3}r\rho_{CT}/P_{CT}]$$
(10)

 $\delta_{\rho cmi}(H,M)$, i=1,2,3, are the default variety of density in corresponding height in Equation (10). They are from three different latitudes: $0^{\circ}(i=1)$, $50^{\circ}(i=2)$ and



Figure 2. Variety of density affected by season and latitude.

90°(*i*=3). $U_{cm1}(H,M)$ is the zonal wind on the equator; ω_3 is angular velocity of earth rotation; *r* is the distance between the position of research and geocenter; ρ_{CT} is standard density; P_{CT} is standard pressure.

The season-latitude component of zonal wind is as follows:

$$u_{cm}(H, L, M) = -[1/2(1 + \delta_{\rho cm})\omega_3 r]^* [P_{CT}/(\sin\varphi^*\rho_{CT})]^* (\partial\delta_{\rho cm}/\partial\varphi)$$
(11)

According to Equation (8), the equipotential line of the density variety affected by season and latitude in January and July can be given as shown in Figure 2. In the figure, the axis of abscissa is latitude ($0^{\circ} \sim 90^{\circ}$ N), and the axis of bank is height ($0 \sim 60$ km). It can be seen that the variety of atmospheric density is affected by latitude and height in different seasons. On the specific height, the variety of atmospheric density will increase with the rising of height. However, there are two heights of equal density at 8 km and 25 km, where the variety of atmospheric density is stable, as shown in Figure 2.

3.2. *Random Factors.* The variety of atmospheric density affected by random factors reflects its uncertainty. This uncertainty is mainly caused by the changes of solar activity and geomagnetic processes. At the range of the height $H \le 100$ km, the mathematical model of variety of atmospheric density affected by random factors is as follows:

$$\delta_{\rho c \pi y} = X(H, L, M) f_1(H) f_2(L) + y(H)$$

*(-4.493*10⁻¹ + 1.978*10⁻² $\sqrt{T_{CP} - 483.92}$) (12)

 $f_1(H)$ is the characteristic function of density variety at a particular height, it can be given as:

$$f_1(H) = a_1 + a_2 \sin[\pi(H - 60)/40] \tag{13}$$

 $f_2(L)$ is the characteristic function of density variety on a particular latitude, it can be given as:

$$f_2(L) = 0.92 + 0.08\sin(9L + a_3) \tag{14}$$

y(H) can be ascertained as below:

$$y(H) = \begin{cases} 0 & H < 95 \text{ km} \\ 3.869^{*}10^{-6}(H-95)^{3} + 2.632^{*}10^{-4}(H-95)^{2} & 95 \text{ km} \leqslant H \leqslant 125 \text{ km} \\ 2.632^{*}10^{-2}(H-112) & H > 125 \text{ km} \end{cases}$$
(15)

X(H,L,M) is equal to $\delta_{\rho c \pi}(H,L,M)$, which is the limit of density variety. It, at height from 0 km to 150 km and latitude from 0° to 90°, is shown as follows:

$$\delta_{\rho c \pi}(H, L, M) = [(1 - \sin(H - 115))/2]^* \{-5 \cdot 119^* 10^{-5} H^2 + 6 \cdot 770^* 10^{-2} + [q_1(H, M)(-5 \cdot 160^* 10^{-1} L^3 + 1 \cdot 216 L^2) + q_2(H)] \\ ^* \cos^2[(\pi |H - H_2|)/(H_1 - 2|H - H_2|)] \} \\ ^* \{a_1 + a_2 \sin[\pi(H - 60)/40]\}^* \{1 - 0 \cdot 08[1 - \sin(9L + a_3)]\} \\ + [(1 + \sin(H - 112))/2]^*(H - 112)(-1 \cdot 182^* 10^{-2} + 5 \cdot 205^* 10^{-4} \sqrt{T_{CP} - 483 \cdot 92})$$
(16)

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 $q_1(H), q_2(H), H_1(H), H_2(H)$ can be chosen from Table 1:

H(km)		q_1	(H)				
	January	April	July	October	$q_2(H)$	$H_1(H)$	$H_2(H)$
0<5	0	0	0	0	0	100	0
$5 \leq H \leq 25$	0.050	0.040	0.030	0.040	$-1.155*10^{-2}$	40	15
$25 \leqslant H \leqslant 115$	0.175	0.108	0.040	0.108	$3.238*10^{-2}$	180	70

 a_1 , a_2 , a_3 and T_{CP} can be chosen from Table 2:

Table 2.	Atmospheric	parameter	(2))
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Scheme	a_1	<i>a</i> ₂	<i>a</i> ₃	$T_{CP}(k)$
1	0	0	0	1000
2	1	0	0	700
3	- 1	0	0	2200
4	0	0.33	0	930
5	0	-0.33	0	1280
6	0.33	0.33	0	830
7	0.33	-0.33	0	970
8	-0.33	0.33	0	1120
9	-0.33	-0.33	0	1670
10	1	0	π	700
11	- 1	0	π	2200
12	0	0.33	π	930
13	0	-0.33	π	1280
14	0.33	0.33	π	830
15	0.33	-0.33	π	970
16	-0.33	0.33	π	1120
17	-0.33	-0.33	π	1670

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Figure 3. Variety of density affected by random factors.



Figure 4. Comparison of density.

Figure 4 shows the simulation results calculated by Equation (12), where the axis of abscissa is density variety, and the axis of bank is height ($0 \sim 60$ km). Figure 3 reflects the variety at 30° north latitude and 50° north latitude. It can be seen from the figure that the variety of density affected by random factors can be approximated as a stochastic process that can be simulated by different parameters at different height, latitude, and season. In this random process, there is an obvious interval in which the variety is small. When the height reaches from 20 km to 30 km, the random variety of atmospheric density is slight, and this means that the status is relatively stable in this interval.

3.3. *Establishment and Verification*. Usually, the atmospheric density is approximately described as an exponential function of height: $\rho = Ae^{-Bh}$. The general mathematic model of atmospheric density is as follows:

$$\rho = 1537 \cdot 3e^{-0.1462 * h_g} \tag{17}$$

This needs to be modified according to Sections 3.1 and 3.2; Equation (17) is modified, then a new disturbed model of atmospheric density can be obtained as follows:

$$\rho = 1537 \cdot 3(1 + \delta_{o\Sigma})e^{-0.1462*h_g} \tag{18}$$

$$\delta_{\rho\Sigma} = \delta_{\rho cm} + \delta_{\rho cn} \tag{19}$$

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Height/km	Refraction angle/second of arc	Ideal value/second of arc		
20	318.1 ~ 338.1	334.8		
25	154.6 ~ 165.3	156.7		
30	69.8 ~ 83.6	73.4		
35	$30.6 \sim 42.8$	34.3		
40	$12.5 \sim 21.9$	16.1		
45	$3.4 \sim 12.4$	7.5		
50	$2\cdot 3 \sim 7\cdot 8$	3.5		

Table 3. Refraction angle at different height.

where $\delta_{\rho\Sigma}$ is the variety of atmospheric density, including $\delta_{\rho cm}$ variety affected by season and latitude and $\delta_{\rho cn}$ variety affected by random factors.

Using the temperature, pressure, wind speed, atmospheric composition and other data on different latitude and geopotential height given by cira1986 (international reference atmosphere), the atmospheric density can be calculated as shown in Figure 4. The solid lines in Figure 4 reflect the average status of atmospheric density at a specific interval of atmospheric pressure. The axis of abscissa is height $(20 \sim 50 \text{ km})$, and the axis of bank is atmospheric density (g/m^3) . The dotted lines in the figure reflect atmospheric density calculated by the model in this paper. As the figures show, the two curves are basically consistent with each other, and the average error is less than 10%. Therefore the new disturbed model of atmospheric density can meet the real situation, and it is practicable.

4. ADAPTIVE MEASUREMENT MODEL BASED ON MULTIPLE MODELS SWITCHING. Multiple models adaptive control is used to describe the uncertainty of a system with multiple models, and the corresponding controller is built on each model. The main idea of the multiple models switching approach is that multiple models are built for one system. Furthermore, each model is switched according to the corresponding requirement.

4.1. *Fixed Measurement Model.* According to the atmospheric density model (Equation (18)), the disturbed measurement model can be obtained by associating Equations (1) and (6). When $\lambda = 0.7 \,\mu\text{m}$, $k(\lambda) = 2.25 \times 10^{-7}$. The refraction model can be obtained through mathematical transformation:

$$R = 0.0338(1 + \delta_{o\Sigma})e^{-0.1518026*h_g}$$
(20)

where h_g is the refraction height (unit is km), R is refraction angle (unit is second of arc). The variety of refraction angle based on atmospheric density at different height is shown in Table 3.

The measurement model for corresponding refraction height can be obtained as follows:

$$h_a = h_g - Hg^* \ln(R) + Hg^* \ln[k(\lambda)\rho_o(2\pi R_e/Hg)^{1/2}] + R(HgR_e/2\pi)^{1/2}$$
(21)

where Hg is the density scale height at refraction height h_g ; refraction angle R and atmospheric density ρ_g changes with refraction height.

Refraction angle decreases as height increases. When the refraction height is beyond 50 km, the refraction angle is lower than the measurement accuracy of the star sensor.

Owing to atmospheric brightness, when the refraction height is lower than 20 km, the refraction star is barely captured. Therefore the disturbed measurement models' range is 20 km to 50 km. According to Equations (20) and (21), fixed measurement models are established at $h_g = 20$ km, 25 km, 30 km, 35 km, 40 km, 45 km, and 50 km.

4.2. Multiple Models Switching. According to the seven measurement models established in the range of $20 \text{ km} \sim 50 \text{ km}$ in Section 4.1, the appropriate model is picked up automatically on the basis of a switching performance index. The prediction error of the model is defined as:

$$e_j = h_g - \dot{h}_g \tag{22}$$

 \hat{h}_g is the estimated value of refraction height, which can be calculated by the observed refraction angle. The performance index $J_j(t)$ is formed by each model's prediction error, while each model could be switched according to which model minimises the performance index. The rationality of this approach lies in that a small prediction error will cause a small concomitant error.

The performance index is as follows:

$$J_j(t) = \alpha e_j^2(t) + \beta \int_0^t e^{-\theta(t-\tau)} e_j^2(\tau) d\tau$$
(23)

where $\alpha \ge 0$, $\beta > 0$, $\theta > 0$. Parameters α and β determine the relative importance of transient measurement and long term measurement in the performance index. Parameter θ is a "forgetting" factor, which determines the memory length of the performance index.

4.3. Switching Process. In order to avoid any fast switching, a hysteresis switching algorithm is used. Assuming prediction model I_j is selected at time t and $J_k = \min\{J_i(t)\}$ that $J_j(T)$ is not the minimum, if $J_j(t) \leq J_k(t) + \delta$, model I_j will also be selected. But if $J_j(t) \geq J_k(t) + \Delta$, model I_k will be selected, where Δ is a hysteresis factor (Shi et al., 2004). The switching process is shown in Figure 5.

The above analysis indicates that when the star sensor captures the refracted starlight at a height of 20 km to 50 km, the system could automatically select the corresponding measurement model. Thus the limitation of the traditional model of a fixed height (25 km) is improved, and the scope of application of the measurement model of stellar refraction expands to the range of 20 km to 50 km. The accuracy and application of navigation by stellar refraction is dramatically improved.

5. SIMULATION

5.1. Dynamic Model. A satellite's movement is affected by many perturbations which include non-spherical earth gravity, solar gravity, lunar gravity, sunlight pressure, atmospheric drag, etc. Compared with the earth gravity, these perturbations are very weak. To model the system states equation, the gravitation and the disturbances in two-order gravity field terms are taken into account in this paper. Other disturbances are equal to process noise with a Gaussian distribution. The state of the satellite can be described by $X = [x, y, z, V_x, V_y, V_z]^T$, where x, y, and z are three components of position; V_x , V_y and V_z are three components of velocity in earth-centred inertial coordinates.



Figure 5. Switching process of the adaptive model.

The state equation is described as:

$$f(X(t), 2t) = \begin{cases} V_x & V_y \\ V_z & V_z \\ -\mu^* x/r^3 (1+3J_2/2^*(R_e/r)^2 (1-5(z/r)^2)) + \omega_x \\ -\mu^* y/r^3 (1+3J_2/2^*(R_e/r)^2 (1-5(z/r)^2)) + \omega_y \\ -\mu^* z/r^3 (1+3J_2/2^*(R_e/r)^2 (1-5(z/r)^2)) + \omega_z \end{cases}$$
(25)

where *r* is the size of the satellite position vector; J_2 is the disturbances in a two-order gravity field; $\omega(t) = [0, 0, 0, \omega_x, \omega_y, \omega_z]^T$ is the model noise which can be assumed as a Gaussian white distribution.

5.2. *Measurement Equation*. The number of refracted stars observed by the satellite is assumed to be 40, distributed uniformly. According to the geometrical relationship as shown in Figure 1, the observation equation can be described as:

$$h_a = \sqrt{r_s^2 - u^2 + u^* \tan(R) - R_e - \sigma + v(t)}$$
(26)



Figure 6. Comparison of navigation results.

where $u = |r_s * u_s|$, r_s is the spacecraft position, u_s is the true direction of starlight and σ is very small and can be ignored. v(t) is the measurement noise which also can be assumed as a Gaussian white distribution. v(t) and $\omega(t)$ are independent of each other. Their statistical characteristics are shown as below:

$$E[\omega(k)] = E[\nu(k)] = 0$$

$$E[\omega(k)\omega^{T}(j)] = Q_{k}\delta_{kj}$$

$$E[\nu(k)\nu^{T}(j)] = R_{k}\delta_{kj}$$

$$E[\omega(k)\nu^{T}(j)] = 0$$
(27)

where δ_{ki} is the impulse function.

According to Equation (26), the measurement value of h_a can be calculated. The real value of h_a needs to be calculated according to Equation (21).

5.3. Results and Analysis Based On UKF. The simulation conditions are as follows: semi-major axis a = 7136.635 km; eccentricity $e = 1.809 \times 10^{-3}$; inclination $i = 65^{\circ}$; right ascension of ascending node $\Omega = 30^{\circ}$; argument of perigee $\omega = 30^{\circ}$; the time passing the perigee t = 0. In order to close to a practical application, the filter cycle T is 3 sec. The initial value of the actual state is $X(0) = [4.590 \times 10^{6} \text{ m}, 4.388 \times 10^{6} \text{ m}, 3.228 \times 10^{6} \text{ m}, -4.612 \times 10^{3} \text{ m/s}, 5.014 \times 10^{2} \text{ m/s}, 5.876 \times 10^{3} \text{ m/s}]^{T}$. The initial value of filtering is $X(0|0) = X(0) + [400 \text{ m}, 400 \text{ m}, 0.8 \text{ m/s}, 0.8 \text{ m/s}]^{T}$. The covariance matrix of the initial estimate error covariance matrix is $P(0|0) = \text{diag}((500 \text{ m})^{2}, (500 \text{ m})^{2}, (0.2 \text{ m/s})^{2}, (0.2 \text{ m/s})^{2})$. The noise covariance matrix of discrete system noise is $Q_{k} = E[\omega\omega^{T}] = \text{diag}(q_{1}^{2}, q_{2}^{2}, q_{1}^{2}, q_{2}^{2}, q_{1}^{2})$, where $q_{1} = 1 \times 10^{-3} \text{ m/s}, q_{2} = 2 \times 10^{-3} \text{ m/s}$. The covariance matrix of measurement noise is $R_{k} = E[\omega m^{T}] = (80 \text{ m})^{2}$.

5.3.1. Simulation Results. Refraction angle R is the random value in the range of 1" to 340". This means refraction height h_g is in the range 20 km to 50 km. Based on the multiple models switching algorithm, the adaptive measurement model is automatically selected. Parameter $\alpha = 1$, $\beta = 0.1$.

Figure 6 shows a comparison of navigation results between the adaptive measurement model and the traditional model. The solid lines in Figure 6 reflect the navigation results based on the traditional model, and the dotted lines reflect the navigation results based on the adaptive measurement model. If filter cycle T is 3 sec,

	<i>T</i> =1 s		Т	= 3 s	T=5 s	
β	u/m	<i>v</i> /(m/s)	u/m	<i>v</i> /(m/s)	u/m	<i>v/</i> (m/s)
0.05	200.3	0.1946	215.7	0.2021	244.5	0.2259
0.1	200.5	0.1948	216.6	0.2029	248.9	0.2293
0.5	202.3	0.1960	223.5	0.2083	255.5	0.2347
1	204.2	0.1973	225.3	0.2097	257.1	0.2359
2	206.1	0.1988	227.1	0.2111	259.0	0.2374
5	208.3	0.2004	227.4	0.2114	260.6	0.2387
10	208.7	0.2007	228.9	0.2126	261.3	0.2392

Table 4. Navigation results with different parameters.



Figure 7. Comparison of navigation results with different parameters.

the variance of the system's position vector is 216.6 m, and the variance of the system's velocity vector is 0.2029 m/s. Comparing the results based on the traditional model, position accuracy is improved by 13.6%, and velocity accuracy is improved by 14% after using the adaptive measurement model.

Parameters α and β are two important parameters of the model switching algorithm, which determine the importance of transient measurement and long term measurement in the performance index. The larger β , the more important to long-term measurement is the performance index. If $\alpha = 1$, β could be different values. The navigation results on different filter cycles are shown in Table 4. Character u is the variance of position estimate, and v is the variance of velocity estimate.

Table 4 shows that the accuracy of navigation decreases with β increasing. The importance of long term measurement in the performance index will increase with increasing β , and this will affect the identification error of the adaptive measurement model. Figure 7 reflects the comparison of navigation results with different parameters. As shown in the figure, the filter cycle has a great influence on the accuracy of navigation. If the filter cycle is larger, accuracy of navigation obviously improves, but this improvement is slow when the filter cycle is smaller.

The atmospheric density model has a great influence on the precision of navigation. If the accuracy of the atmospheric density model is 0.5%, 1%, 2%, 3%, 4%, and 5%, the variance of measurement noise can be calculated according to Equation (20) as shown in Table 5.

Table 5. Measurement noise affected by accuracy of atmospheric density model.

accuracy of atmospheric density model (1σ)	0.5%	1%	2%	3%	4%	5%
measurement noise variance (m ²)	$(62)^2$	$(80)^2$	$(144)^2$	$(205)^2$	$(268)^2$	$(330)^2$

Table 6. Navigation results affected by accuracy of atmospheric density model.						
accuracy of atmospheric density model (1σ)	0.5%	1%	2%	3%	4%	5%
variance of position estimate (m) $T=1$ s	191.1	220.2	299.5	367.0	432·1	491.3
variance of velocity estimate (m/s) $T=1$ s	0.1824	0.2082	0.2781	0.3376	0.3953	0.4485
variance of position estimate (m) $T=3$ s	199.9	241.7	366.6	467.1	552.5	620.1
variance of velocity estimate (m/s) $T=3$ s	0.1840	0.2201	0.3306	0.4212	0.5006	0.5656

Using the variance of measurement noise, the accuracy of navigation influenced by atmospheric density can be obtained as shown in Table 6.

As seen from Table 6, the accuracy of the atmospheric density model is an essential factor affecting the accuracy of navigation by stellar refraction. This effect is more obvious when the filter cycle is larger. If the accuracy of the atmospheric density model is 2%, the navigation results meet the accuracy requirements.

5.3.2. *Results Discussion.* As can be seen from the results, navigation by stellar refraction can be affected by many factors. The simulation results show that by using the adaptive measurement model, the accuracy of navigation by stellar refraction could be improved. Comparing navigation based on the tradition model, the accuracy can be improved by 14%. Also, the refraction star range captured by star sensor expands from 20 km to 50 km.

 α and β are two important parameters of the model switching algorithm which determine the importance of transient measurement and long-term measurement. When the importance of long-term measurement in the performance index is heavier, namely if the β is larger, it is more difficult to achieve high accuracy navigation.

The accuracy of the atmospheric density model is an influential factor on the accuracy of navigation. When the accuracy of atmospheric density model decreased to 1%, the accuracy of navigation results will improve by about 80 m.

6. CONCLUSION. For navigation by stellar refraction, the measurement model is the most crucial element which can decide the results and application of navigation. Due to the uncertainty of atmospheric density, the relationship between refraction angle and refraction height is usually hard to describe. After the study of stellar refraction principles and atmospheric density changes with altitude, latitude, season and other factors, the adaptive measurement model based on multi-model switching is established in this paper, which improves on the limitations of the traditional measurement model.

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REFERENCES

- Gounley, R., White, R. L. and Gai, E. (1984). Autonomous Satellite Navigation by Stellar Refraction. *Journal of Guidance, Control, and Dynamics* 7, 129–134.
- Rongfen, Ji. (1995). The disturbed atmospheric model of the earth. Spacecraft Recovery and Remote Sensing, 15, 66-81.
- Lair, J. L. and Duchon, P. (1988). Satellite Navigation by Stellar Refraction. Acta Astronaut ICA 17, 1069– 1079.
- Hongrui, Shi, Zhihong, Ma and Hongtao, Sun (2004). pH Adaptive Control Based on Multiple Model Switching Approach. *Proceedings of the 5th World Congress on Intelligent Control and Automation*, Hangzhou, P.R. China.
- Xinlong, Wang and Shan, Ma (2009). A Celestial Analytic Positioning Method by Stellar Horizon Atmospheric Refraction. *Chinese Journal of Aeronautics*, **3**, 293–300.
- Haiyan, Yang, Xueying, An, Jie, Wu and Guoqiang, Tang. (2010). Autonomous Navigation Based on Stellar Refraction for Elliptic Orbit Spacecraft. 3rd International Symposium on Systems and Control in Aeronautics and Astronautics (ISSCAA), Harbin, P.R. China.