



# Bounds for internally heated convection with fixed boundary heat flux

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We prove a new rigorous bound for the mean convective heat transport  $\langle wT \rangle$ , where  $w$  and  $T$  are the non-dimensional vertical velocity and temperature, in internally heated convection between an insulating lower boundary and an upper boundary with a fixed heat flux. The quantity  $\langle wT \rangle$  is equal to half the ratio of convective to conductive vertical heat transport, and also to  $\frac{1}{2}$  plus the mean temperature difference between the top and bottom boundaries. An analytical application of the background method based on the construction of a quadratic auxiliary function yields  $\langle wT \rangle \leq \frac{1}{2}(\frac{1}{2} + \frac{1}{\sqrt{3}}) - 1.6552 R^{-(1/3)}$  uniformly in the Prandtl number, where  $R$  is the non-dimensional control parameter measuring the strength of the internal heating. Numerical optimisation of the auxiliary function suggests that the asymptotic value of this bound and the  $-1/3$  exponent are optimal within our bounding framework. This new result halves the best existing (uniform in  $R$ ) bound (Goluskin, *Internally Heated Convection and Rayleigh–Bénard Convection*, Springer, 2016, table 1.2), and its dependence on  $R$  is consistent with previous conjectures and heuristic scaling arguments. Contrary to physical intuition, however, it does not rule out a mean heat transport larger than  $\frac{1}{2}$  at high  $R$ , which corresponds to the top boundary being hotter than the bottom one on average.

**Key words:** variational methods

## 1. Introduction

Convection driven by internally generated heat is a common physical phenomenon and underpins several problems in geophysics, such as mantle convection (Schubert, Turcotte & Olson 2001; Mulyukova & Bercovici 2020). One important open problem is to characterise the vertical heat transport as a function of the heating strength, measured by the non-dimensional Rayleigh number  $R$ . Simulations and experiments (Hewitt, McKenzie

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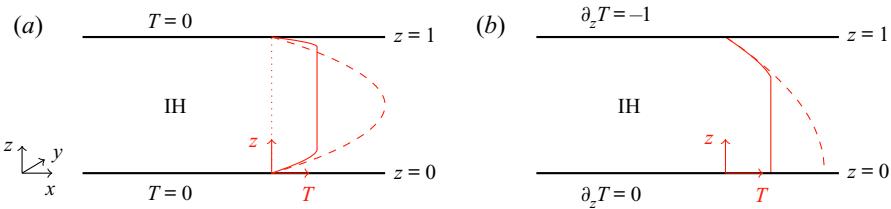


Figure 1. The IH convection (*a*) with isothermal boundaries, studied by Arslan *et al.* (2021), and (*b*) with fixed-flux boundary conditions, studied in this paper. In both panels, IH represents the uniform unit internal heat generation. Red dashed lines denote the conductive temperature profiles, and red solid lines denote indicative mean temperature profiles in the turbulent regime.

& Weiss 1980; Ishiwatari, Takehiro & Hayashi 1994; Lee, Lee & Suh 2007; Goluskin 2015) reveal that the heat transport increases with the heating strength, and heuristic scaling laws based on physically reasonable, but unproven, assumptions have been put forward (Goluskin 2016). However, corroborating or disproving such heuristic arguments through the derivation of rigorous  $R$ -dependent bounds remains a challenge (Arslan *et al.* 2021).

For internally heated (IH) convection between isothermal boundaries, a major difficulty in bounding the heat transport is the subtle interplay between the lower and upper thermal boundary layers (Arslan *et al.* 2021). In contrast to Rayleigh–Bénard convection, for which fixed-temperature or fixed-flux boundary conditions are symmetric and produce unstable thermal boundary layers, internal heating produces positive buoyancy that acts in the positive vertical direction and therefore creates asymmetry in relation to the lower and upper boundaries (see Figure 1*a*). In this regard, the lower thermal boundary layer of IH convection (see, for example, Goluskin & van der Poel 2016) has a different character from those found in Rayleigh–Bénard convection, and is stably stratified.

In this study, we remove the subtleties associated with the lower boundary by specifying a zero-flux condition, as illustrated in figure 1(*b*). The hypothesis behind this choice is that the resulting problem will be driven primarily by the properties of the unstably-stratified thermal boundary layer near the top boundary and, therefore, will bear a closer resemblance to Rayleigh–Bénard convection. To ensure that the energy generated internally leaves the domain and the fluid's temperature does not increase without bound, we also replace the isothermal top boundary with one satisfying a fixed-flux condition. These boundary conditions idealise models of mantle convection, where radioactive decay provides the internal heating, the core–mantle boundary is approximated by a thermal insulator and a warm crust or atmosphere limits the rate of heat loss to space (Kiefer & Li 2009; Trowbridge *et al.* 2016; Mulyukova & Bercovici 2020).

Within this flow configuration, our goal is to bound the dimensionless convective heat flux  $\langle wT \rangle$ , where angled brackets denote an average over volume and infinite time. This quantity is related to the mean temperature difference between the top and bottom boundaries: multiplying the equation governing the evolution of temperature (see § 2) by the vertical coordinate  $z$  and integrating by parts over the volume and infinite time yields

$$\langle wT \rangle + \bar{T}_0 - \bar{T}_1 = \frac{1}{2}, \quad (1.1)$$

with  $\bar{T}_0$  and  $\bar{T}_1$  denoting the average temperatures of the bottom and top boundaries, respectively, where the average is over the horizontal directions and infinite time. The right-hand side of (1.1) represents the input of potential energy (1/2), which balances the reversible work  $\langle wT \rangle$  done by the velocity field (equal to the average viscous dissipation) and the unknown rate  $\bar{T}_0 - \bar{T}_1$  at which the fluid's potential energy decreases due to

conduction. Thus,  $\langle wT \rangle = 0$  corresponds to the static case of upward conductive transport,  $\langle wT \rangle = \frac{1}{2}$  corresponds to purely convective transport between boundaries of equal mean temperature, and  $\langle wT \rangle > \frac{1}{2}$  implies downward conduction on average.

The sign of the conductive term  $\bar{T}_0 - \bar{T}_1$  is *a priori* unknown, but it can be shown that  $|\bar{T}_0 - \bar{T}_1| \leq |\langle T \rangle - \bar{T}_1|^{1/2}$  (Goluskin 2016). For sufficiently large Rayleigh numbers, this estimate can be combined with the lower bound  $cR^{-1/3} < \langle T \rangle - \bar{T}_1$  (Lu, Doering & Busse 2004) and the upper bound  $\langle T \rangle - \bar{T}_1 \leq \frac{1}{3}$  (Goluskin 2015) to yield  $\langle wT \rangle \leq \frac{1}{2} + \frac{1}{\sqrt{3}}$  uniformly in  $R$ . However, assuming that  $\bar{T}_0$  and  $\langle T \rangle$  scale similarly with the Rayleigh number, Goluskin (2016) conjectured that the mean vertical heat flux should satisfy  $\langle wT \rangle \leq \frac{1}{2} - O(R^{-1/3})$ .

The present work proves that

$$\langle wT \rangle \leq \frac{1}{2} \left( \frac{1}{2} + \frac{1}{\sqrt{3}} \right) - cR^{-(1/3)}, \quad (1.2)$$

with  $c \approx 1.6552$ . This bound scales with  $R$  exactly as conjectured and asymptotes to (approximately) 0.5387, which is slightly larger than  $\frac{1}{2}$  but halves the only existing uniform bound. To obtain (1.2), we employ the background method (Doering & Constantin 1994, 1996; Constantin & Doering 1995) interpreted as the search for a quadratic auxiliary function (Chernyshenko *et al.* 2014; Fantuzzi *et al.* 2016; Chernyshenko 2017; Rosa & Temam 2020). This interpretation makes it easier to derive a convex variational problem that yields bounds on  $\langle wT \rangle$  even though, contrary to traditional applications of the background method, the heat flux in IH convection is not directly related to the thermal dissipation.

The work is structured as follows. Section 2 presents the governing equations. In § 3, we derive the variational problem to bound  $\langle wT \rangle$  from above. Analytical and numerical bounds are presented in §§ 4 and 5, respectively. Section 6 offers concluding remarks.

## 2. Model

We consider a uniformly heated layer of fluid bounded between two horizontal plates at a vertical distance  $d$ . The fluid has kinematic viscosity  $\nu$ , thermal diffusivity  $\kappa$ , density  $\rho$ , specific heat capacity  $c_p$ , and thermal expansion coefficient  $\alpha$ . The dimensional heating rate per unit volume  $Q$  is constant in time and space. For simplicity, we assume that the layer is periodic in the horizontal ( $x$  and  $y$ ) directions, with periods  $L_x$  and  $L_y$ . While these values affect the mean vertical heat flux, the analytical bounds derived below do not depend on  $L_x$  or  $L_y$  and therefore apply to domains of all sizes (including the limiting case of a horizontally infinite fluid layer).

To make the problem non-dimensional, we use  $d$  as the characteristic length scale,  $d^2/\kappa$  as the time scale and  $d^2Q/\kappa\rho c_p$  as the temperature scale. The motion of the fluid in the non-dimensional domain  $\Omega = [0, L_x] \times [0, L_y] \times [0, 1]$  is then governed by the Boussinesq equations

$$\nabla \cdot \mathbf{u} = 0, \quad (2.1a)$$

$$\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} + \nabla p = Pr(\nabla^2 \mathbf{u} + RT \hat{\mathbf{z}}), \quad (2.1b)$$

$$\partial_t T + \mathbf{u} \cdot \nabla T = \nabla^2 T + 1, \quad (2.1c)$$

where  $\mathbf{u}$  is the fluid velocity,  $p$  is the pressure, and the unit forcing in (2.1c) represents the non-dimensional internal heating rate. The no-slip, fixed-flux boundary conditions are

expressed by

$$\mathbf{u}|_{z=0} = \mathbf{u}|_{z=1} = 0, \quad (2.2a)$$

$$\partial_z T|_{z=0} = 0, \quad \partial_z T|_{z=1} = -1. \quad (2.2b)$$

The dimensionless quantities

$$Pr = \frac{\nu}{\kappa} \quad \text{and} \quad R = \frac{g\alpha Qd^5}{\rho c_p v \kappa^2}, \quad (2.3a,b)$$

where  $g$  is the acceleration of gravity, are the only two non-dimensional control parameters. The former is the usual Prandtl number, which measures the ratio of momentum and heat diffusivity. The latter, instead, measures the destabilising effect of internal heating compared with the stabilising effects of diffusion, and may therefore be interpreted as a Rayleigh number.

Since the volume-averaged temperature  $\int T(\mathbf{x}, t) d\mathbf{x}$  is conserved in time, we assume it to be zero without loss of generality. With this extra condition, the governing equations admit the solution  $\mathbf{u} = \mathbf{0}$ ,  $p = \text{constant}$  and  $T = -(z^2/2) + \frac{1}{6}$  at all  $R$ , which represents a purely conductive state. This state is globally asymptotically stable irrespective of the horizontal periods  $L_x$  and  $L_y$  if  $R < 1429.86$ , and it is linearly unstable when  $R > 1440$  for sufficiently large horizontal periods (Goluskin 2015). Convection ensues above this Rayleigh number for at least one choice of the horizontal periods, and cannot currently be ruled out above the known global stability threshold. We are therefore interested in bounds on  $\langle wT \rangle$  that hold for arbitrary  $R \geq 1429.86$ .

### 3. Bounding framework

To derive an upper bound on  $\langle wT \rangle$ , it is convenient to lift the inhomogeneous boundary condition on the temperature by introducing the temperature perturbation

$$\theta(\mathbf{x}, t) = T(\mathbf{x}, t) + \frac{z^2}{2} - \frac{1}{6}. \quad (3.1)$$

The heat equation (2.1c) and boundary conditions (2.2b) show that  $\theta$  satisfies

$$\partial_t \theta + \mathbf{u} \cdot \nabla \theta = \nabla^2 \theta + zw, \quad (3.2a)$$

$$\partial_z \theta|_{z=0} = 0, \quad \partial_z \theta|_{z=1} = 0. \quad (3.2b)$$

To rewrite the heat flux in terms of  $\theta$ , observe that, by virtue of incompressibility and of the boundary conditions in (2.2a), the horizontal-and-time average  $\bar{w}(z)$  of the vertical velocity  $w$  vanishes for all  $z$ . Then

$$\langle wf(z) \rangle = \int_0^1 \bar{w}(z)f(z) dz = 0 \quad (3.3)$$

for any  $z$ -dependent function  $f(z)$ , and in particular we conclude that

$$\langle wT \rangle = \langle w\theta \rangle. \quad (3.4)$$

A rigorous upper bound on  $\langle w\theta \rangle$  can be derived using the auxiliary functional method (Chernyshenko *et al.* 2014) with the quadratic auxiliary functional

$$\mathcal{V}\{\mathbf{u}, \theta\} = \oint_{\Omega} \frac{a}{2PrR} |\mathbf{u}|^2 + \frac{b}{2} |\theta|^2 - \phi(\mathbf{x})\theta - \psi(\mathbf{x}) \cdot \mathbf{u} dx, \quad (3.5)$$

where the non-negative scalars  $a$  and  $b$ , the function  $\phi$  and the vector field  $\psi$  are to be optimised in order to obtain the best possible bound. Chernyshenko (2017) showed that

this is equivalent to employing the background method: the profile  $\phi/b$  is the background temperature (defined with respect to  $\theta$ ), the vector field  $(PrR/a)\psi$  is the background velocity, and  $a$  and  $b$  are the so-called balance parameters. Contrary to the classical background method, there is no need to impose boundary or incompressibility conditions on  $\psi$  or  $\phi$  when defining  $\mathcal{V}$ . To simplify the analysis below, however, we take  $\psi$  to be incompressible, horizontally periodic and vanishing at the top and bottom plates. The optimality of these choices can be proved rigorously, but the details are beyond the scope of this work.

Arguments identical to those given by Goluskin & Fantuzzi (2019, appendix A) show that the auxiliary function (3.5) may be taken to be invariant under arbitrary horizontal translations and under the ‘horizontal flow reversal’ variable transformation

$$\begin{pmatrix} \mathbf{u}(x, t) \\ \theta(x, t) \\ p(x, t) \end{pmatrix} \mapsto \begin{pmatrix} \mathbf{G}\mathbf{u}(\mathbf{G}x, t) \\ \theta(\mathbf{G}x, t) \\ p(\mathbf{G}x, t) \end{pmatrix}, \quad \mathbf{G} = \begin{pmatrix} -1 & 0 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 1 \end{pmatrix}. \quad (3.6a,b)$$

This is because the governing equations (2.1a), (2.1b) and (3.2a) are invariant under the same set of transformations. Invariance under horizontal translation requires  $\phi(x) = \phi(z)$  and  $\psi(x) = \psi(z)$ . In particular, the incompressibility and no-slip conditions on  $\psi$  imply that we must have  $\psi(z) = (\psi_1(z), \psi_2(z), 0)$ . Invariance under (3.6a,b) then requires  $\psi_1(z) = \psi_2(z) = 0$ , so  $\psi = \mathbf{0}$ .

Making these restrictions from now on, it can be shown that  $\mathcal{V}\{\mathbf{u}(t), \theta(t)\}$  remains uniformly bounded in time along solutions of (2.1b) and (3.2a) for any given initial velocity and temperature. We can therefore use the fundamental theorem of calculus and the governing equations to write

$$\begin{aligned} \langle w\theta \rangle &= \limsup_{\tau \rightarrow \infty} \frac{1}{\tau} \int_0^\tau \oint_{\Omega} w\theta + \frac{d}{dt} \mathcal{V}\{\mathbf{u}(t), \theta(t)\} dx dt \\ &= \limsup_{\tau \rightarrow \infty} \frac{1}{\tau} \int_0^\tau \oint_{\Omega} w\theta + \frac{a}{PrR} \mathbf{u} \cdot \partial_t \mathbf{u} + b\theta \partial_t \theta - \phi(z) \partial_t \theta dx dt \\ &= U - \liminf_{\tau \rightarrow \infty} \frac{1}{\tau} \int_0^\tau \mathcal{S}\{\mathbf{u}(t), \theta(t)\} dt \end{aligned} \quad (3.7)$$

for any constant  $U$ , where

$$\mathcal{S}\{\mathbf{u}, \theta\} = \oint_{\Omega} \frac{a}{R} |\nabla \mathbf{u}|^2 + b |\nabla \theta|^2 - (a + 1 + bz - \phi') w\theta - \phi' \partial_z \theta + U dx \quad (3.8)$$

and primes denote derivatives with respect to  $z$ . The last equality in (3.7) is obtained after a few integrations by parts that exploit the boundary conditions, incompressibility and the identity (3.3). The bound  $\langle wT \rangle = \langle w\theta \rangle \leq U$  follows from (3.4) and (3.7) if  $\mathcal{S}\{\mathbf{u}, \theta\}$  is non-negative for all time-independent velocities  $\mathbf{u}$  and temperature perturbations  $\theta$  that satisfy incompressibility and the boundary conditions in (2.2a) and (3.2b). Our goal, therefore, is to choose  $a$ ,  $b$  and  $\phi(z)$  such that this condition holds for the smallest possible  $U$ .

To simplify this task, we invoke the horizontal periodicity and expand the velocity and temperature fields using Fourier series:

$$\begin{bmatrix} \theta(x, y, z) \\ \mathbf{u}(x, y, z) \end{bmatrix} = \sum_k \begin{bmatrix} \hat{\theta}_k(z) \\ \hat{\mathbf{u}}_k(z) \end{bmatrix} \exp(i(k_x x + k_y y)). \quad (3.9)$$

The sum is over wavevectors  $\mathbf{k} = (k_x, k_y)$  of magnitude  $k = \sqrt{k_x^2 + k_y^2}$  that are compatible with the horizontal periods  $L_x$  and  $L_y$ . The (complex-valued) Fourier amplitudes  $\hat{\theta}_{\mathbf{k}}$  and  $\hat{u}_{\mathbf{k}} = (\hat{u}_{\mathbf{k}}, \hat{v}_{\mathbf{k}}, \hat{w}_{\mathbf{k}})$  satisfy

$$\hat{u}_{\mathbf{k}}(0) = \hat{u}_{\mathbf{k}}(1) = \hat{v}_{\mathbf{k}}(0) = \hat{v}_{\mathbf{k}}(1) = 0, \quad (3.10a)$$

$$\hat{w}_{\mathbf{k}}(0) = \hat{w}'_{\mathbf{k}}(0) = \hat{w}_{\mathbf{k}}(1) = \hat{w}'_{\mathbf{k}}(1) = 0, \quad (3.10b)$$

$$\hat{\theta}'_{\mathbf{k}}(0) = \hat{\theta}'_{\mathbf{k}}(1) = 0. \quad (3.10c)$$

After substituting (3.9) into (3.8), the Fourier-transformed incompressibility condition  $ik_x \hat{u}_{\mathbf{k}} + ik_y \hat{v}_{\mathbf{k}} + \hat{w}'_{\mathbf{k}} = 0$  can be combined with Young's inequality to estimate

$$\mathcal{S}\{\mathbf{u}, \theta\} \geq \mathcal{S}_0\{\hat{\theta}_0\} + \sum_{\mathbf{k}} \mathcal{S}_{\mathbf{k}}\{\hat{w}_{\mathbf{k}}, \hat{\theta}_{\mathbf{k}}\}, \quad (3.11)$$

where

$$\mathcal{S}_0\{\hat{\theta}_0\} := U + \int_0^1 b|\hat{\theta}'_0(z)|^2 - \phi' \hat{\theta}'_0(z) dz \quad (3.12a)$$

and

$$\begin{aligned} \mathcal{S}_{\mathbf{k}}\{\hat{w}_{\mathbf{k}}, \hat{\theta}_{\mathbf{k}}\} &:= \int_0^1 \frac{a}{R} \left( \frac{|\hat{w}''_{\mathbf{k}}(z)|^2}{k^2} + 2|\hat{w}'_{\mathbf{k}}(z)|^2 + k^2 |\hat{w}_{\mathbf{k}}(z)|^2 \right) + b|\hat{\theta}'_{\mathbf{k}}(z)|^2 \\ &\quad + bk^2 |\hat{\theta}_{\mathbf{k}}(z)|^2 - [a + 1 + bz - \phi'(z)] \hat{w}_{\mathbf{k}}(z)^* \hat{\theta}_{\mathbf{k}}(z) dz. \end{aligned} \quad (3.12b)$$

Standard arguments (see e.g. Arslan *et al.* 2021) show that the right-hand side of (3.11) is non-negative if and only if each summand is non-negative, and that to check these conditions one can assume that  $\hat{w}_{\mathbf{k}}$  and  $\hat{\theta}_{\mathbf{k}}$  are real functions. Thus, the best bound on  $\langle wT \rangle$  is found upon solving the optimisation problem

$$\begin{aligned} \inf_{U, \phi'(z), a, b} \{U : \mathcal{S}_0\{\hat{\theta}_0\} \geq 0 \quad \forall \hat{\theta}_0 \text{ s.t. (3.10c)}, \\ \mathcal{S}_{\mathbf{k}}\{\hat{w}_{\mathbf{k}}, \hat{\theta}_{\mathbf{k}}\} \geq 0 \quad \forall \hat{w}_{\mathbf{k}}, \hat{\theta}_{\mathbf{k}} \text{ s.t. (3.10a), } \forall \mathbf{k} \neq 0\}. \end{aligned} \quad (3.13)$$

We refer to the condition  $\mathcal{S}_{\mathbf{k}}\{\hat{w}_{\mathbf{k}}, \hat{\theta}_{\mathbf{k}}\} \geq 0$  as the spectral constraint and consider  $\phi'$ , rather than  $\phi$ , as the optimisation variable because only the former appears in the problem.

#### 4. Analytical bound

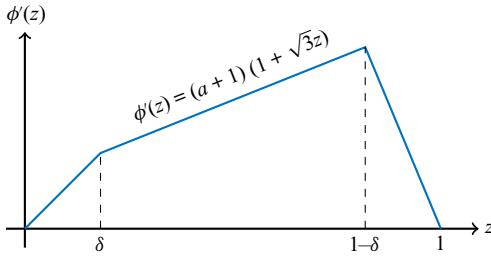
To derive an analytical bound on  $\langle wT \rangle$ , we begin by observing that

$$\mathcal{S}_0\{\hat{\theta}_0\} = \int_0^1 b \left( \hat{\theta}'_0(z) - \frac{\phi'(z)}{2b} \right)^2 - \frac{\phi'(z)^2}{4b} + U dz \geq U - \int_0^1 \frac{\phi'(z)^2}{4b} dz, \quad (4.1)$$

so the constraint on  $\mathcal{S}_0$  in (3.13) is satisfied if we choose

$$U = \int_0^1 \frac{\phi'(z)^2}{4b} dz. \quad (4.2)$$

This choice is also optimal because the lower bound in (4.1) is sharp. To see this, let  $\hat{\theta}_0$  be such that  $\hat{\theta}'_0(z) = (1/2b)\phi'(z)$  except for boundary layers of width  $\epsilon$  near  $z = 0$  and


 Figure 2. Sketch of the piecewise linear  $\phi'(z)$  in (4.5a,b).

$z = 1$ , where  $\hat{\theta}'_0(z) = 0$  to satisfy (3.10c). Then, let  $\epsilon \rightarrow 0$  and apply Lebesgue's dominated convergence theorem to conclude that  $\mathcal{S}\{\hat{\theta}_0\}$  converges to the right-hand side of (4.1).

Next, we seek constants  $a$  and  $b$  and a function  $\phi(z)$  that minimise the right-hand side of (4.2) whilst satisfying the spectral constraint in (3.13). The simplest way to ensure this is to set  $\phi'(z) = a + 1 + bz$ , because then the only sign-indefinite term in  $S_k$  vanishes. This choice yields

$$\langle wT \rangle \leq U = \frac{1}{12} \left[ b + 3(a+1) + \frac{(a+1)^2}{b} \right], \quad (4.3)$$

which attains the minimum value of  $\frac{1}{2}(\frac{1}{2} + \frac{1}{\sqrt{3}})$  when  $b = \sqrt{3}(a+1)$  and  $a = 0$ .

While this simple construction already halves the uniform bound proved by Goluskin (2016), an even better result that depends explicitly on the Rayleigh number can be obtained by letting  $\phi'$  develop boundary layers of width  $\delta$  near  $z = 0$  and  $z = 1$ . Specifically, we still fix

$$b = \sqrt{3}(a+1), \quad (4.4)$$

but this time take

$$\phi'(z) = (a+1)\xi(z), \quad \xi(z) = \begin{cases} \left(\frac{1}{\delta} + \sqrt{3}\right)z, & 0 \leq z \leq \delta, \\ 1 + \sqrt{3}z, & \delta \leq z \leq 1-\delta, \\ \left(\frac{1+\sqrt{3}}{\delta} - \sqrt{3}\right)(1-z), & 1-\delta \leq z \leq 1. \end{cases} \quad (4.5a,b)$$

This profile, illustrated in figure 2, yields the upper bound

$$\langle wT \rangle \leq U = \frac{1}{2} \left( \frac{1}{2} + \frac{1}{\sqrt{3}} - \frac{6+5\sqrt{3}}{9}\delta + \frac{\sqrt{3}}{6}\delta^2 \right) (a+1) \quad (4.6a)$$

$$\leq \frac{1}{2} \left( \frac{1}{2} + \frac{1}{\sqrt{3}} - A\delta \right) (a+1), \quad (4.6b)$$

where the last inequality holds for any constant  $A$  satisfying  $A \leq \frac{1}{9}(6+5\sqrt{3}) - \frac{\sqrt{3}}{6}\delta$ . Anticipating that the height of the boundary layers in  $\phi'$  will have to be small, we arbitrarily assume that  $\delta \leq \frac{1}{3}$  (this will be checked *a posteriori*) and therefore set  $A = (4+3\sqrt{3})/6$  irrespective of  $\delta$ . These conservative choices considerably simplify the algebra in what follows.

Note that although (4.2) suggests setting  $\xi(z) = 0$  throughout the boundary layers, a linear variation makes the spectral constraint easier to satisfy and results in a smaller bound on  $\langle wT \rangle$ . The values of  $a$  and  $\delta$  must be chosen as functions of  $R$  to minimise (4.6b) whilst ensuring that the indefinite term in  $\mathcal{S}_k$ ,

$$\mathcal{I} := (a+1) \int_{[0,\delta] \cup [1-\delta,1]} [1 + \sqrt{3}z - \xi(z)] \hat{w}_k(z) \hat{\theta}_k(z) dz, \quad (4.7)$$

can be controlled. For the boundary layer at  $z = 0$ , we can use the boundary conditions on  $\hat{w}_k$  and  $\hat{w}'_k$  in (3.10b) and the Cauchy–Schwarz inequality to estimate

$$\begin{aligned} |\hat{w}_k(z)| &= \left| \int_0^z \int_0^\zeta \hat{w}''_k(\eta) d\eta d\zeta \right| \leq \int_0^z \int_0^\zeta |\hat{w}''_k(\eta)| d\eta d\zeta \\ &\leq \int_0^z \sqrt{\zeta} d\zeta \|\hat{w}''_k\|_2 = \frac{2}{3} z^{3/2} \|\hat{w}''_k\|_2. \end{aligned} \quad (4.8)$$

Using this estimate, the definition of  $\xi$  from (4.5a,b), and the Cauchy–Schwarz inequality once again, we obtain

$$\left| \int_0^\delta [1 + \sqrt{3}z - \xi(z)] \hat{w}_k(z) \hat{\theta}_k(z) dz \right| \leq \frac{\delta^2}{3\sqrt{15}} \|\hat{w}''_k\|_2 \|\hat{\theta}_k\|_2. \quad (4.9)$$

Similar arguments near  $z = 1$  yield

$$\left| \int_{1-\delta}^1 [1 + \sqrt{3}z - \xi(z)] \hat{w}_k(z) \hat{\theta}_k(z) dz \right| \leq \frac{1 + \sqrt{3}}{3\sqrt{15}} \delta^2 \|\hat{w}''_k\|_2 \|\hat{\theta}_k\|_2. \quad (4.10)$$

Using these inequalities we can now estimate

$$\begin{aligned} \mathcal{S}_k\{\hat{w}_k, \hat{\theta}_k\} &\geq \frac{a}{Rk^2} \|\hat{w}'_k\|_2^2 + \sqrt{3}(a+1)k^2 \|\hat{\theta}_k\|_2^2 - |\mathcal{I}| \\ &\geq \frac{a}{Rk^2} \|\hat{w}'_k\|_2^2 + \sqrt{3}(a+1)k^2 \|\hat{\theta}_k\|_2^2 - \frac{2 + \sqrt{3}}{3\sqrt{15}} (a+1)\delta^2 \|\hat{w}''_k\|_2 \|\hat{\theta}_k\|_2. \end{aligned} \quad (4.11)$$

The last expression is a homogeneous quadratic form in  $\|\hat{w}''_k\|_2$  and  $\|\hat{\theta}_k\|_2$ , and is non-negative if its discriminant is non-positive. To ensure that the spectral constraints hold with the largest possible  $\delta$ , so the bound (4.6b) is minimised, we therefore set

$$\delta = \alpha \left( \frac{a}{(a+1)R} \right)^{1/4}, \quad (4.12)$$

with  $\alpha = [540(7\sqrt{3} - 12)]^{1/4}$ . Substituting this into (4.6a) yields an upper bound on  $\langle wT \rangle$  that depends only on  $a$ , and in principle this parameter can be optimised numerically for each value of  $R$ . To obtain a fully analytical bound, however, we substitute (4.12) into the

weaker bound (4.6b) and use the fact that  $a > 0$  to arrive at

$$\begin{aligned}\langle wT \rangle &\leq \frac{1}{2} \left( \frac{1}{2} + \frac{1}{\sqrt{3}} \right) (a+1) - \frac{1}{2} A \alpha a^{1/4} (a+1)^{3/4} R^{-(1/4)} \\ &\leq \frac{1}{2} \left( \frac{1}{2} + \frac{1}{\sqrt{3}} \right) (a+1) - \frac{1}{2} A \alpha a^{1/4} R^{-(1/4)}.\end{aligned}\quad (4.13)$$

This bound can be optimised analytically over  $a$  by solving the equation  $\partial U / \partial a = 0$ , which gives

$$a = a_0 R^{-(1/3)} \quad (4.14)$$

with  $a_0 = [\frac{1}{2} A \alpha (2\sqrt{3} - 3)]^{4/3}$ . This translates into the upper bound

$$\langle wT \rangle \leq \frac{1}{2} \left( \frac{1}{2} + \frac{1}{\sqrt{3}} \right) \left( 1 - 3a_0 R^{-(1/3)} \right). \quad (4.15)$$

Substituting (4.14) into (4.12) shows that  $\delta = O(R^{-(1/3)})$ , which agrees with scaling arguments proposed for Rayleigh–Bénard convection (Spiegel 1963). Moreover, the constraint  $\delta \leq \frac{1}{3}$  imposed at the beginning is satisfied for all  $R \geq 591.51$ , which is below the energy stability limit (cf. § 2). As required, therefore, the upper bound (4.15) applies to all values of  $R$  for which convection cannot be ruled out.

## 5. Numerically optimised bounds

To assess how far the analytical bound (4.15) is from being optimal, we numerically approximated the best upper bounds on  $\langle wT \rangle$  implied by problem (3.13) using the MATLAB toolbox QUINOPT (Fantuzzi *et al.* 2017). This toolbox employs truncated Legendre series expansions for the tunable function  $\phi$  and for the unknown fields  $\hat{\theta}_0, \hat{\theta}_k$  and  $\hat{w}_k$  in order to discretise the convex variational problem (3.13) into a numerically tractable semidefinite program (SDP) (for more details on this approach, see Fantuzzi & Wynn 2015, 2016; Fantuzzi, Pershin & Wynn 2018). Numerically optimal solutions to (3.13) were obtained for  $10^3 \leq R \leq 10^9$  in a two-dimensional domain with horizontal period  $L_x = 2$ . The number of terms in the Legendre series expansion used by QUINOPT was increased until the optimal upper bound changed by less than 1 %, and an iterative procedure (see e.g. Fantuzzi & Wynn 2016) was employed to check the spectral constraints  $S_k \geq 0$  up to the cutoff wavenumber

$$k_c := \left( \frac{R}{4ab} \right)^{1/4} \|a + 1 + bz - \phi'\|_\infty^{1/2}, \quad (5.1)$$

where  $\|\cdot\|_\infty$  is the  $L^\infty$  norm. This value was derived using the method described in Arslan *et al.* (2021, appendix B), which ensures that  $S_k \geq 0$  is non-negative for all  $k > k_c$  given any fixed choices of  $R, a, b$  and  $\phi'$ .

The numerically optimal bounds on  $\langle wT \rangle$  are compared to the analytical bound (4.15) in figure 3(a). The former are zero until  $R_E = 2147$ , which differs from the energy stability limit reported by Goluskin (2015) due to the choice of horizontal period made in our numerical implementation. The inset (b) reveals that the optimal and analytical bounds appear to tend to the same asymptotic value as  $R \rightarrow \infty$ . Moreover, as evidenced by panel (c), they seem to do so at the same rate. This suggests that the only possible improvement to our analytical bound is in the coefficient of the  $O(R^{-(1/3)})$  correction, which for our numerically optimal bound is estimated to be  $5.184 \pm 0.062$ .

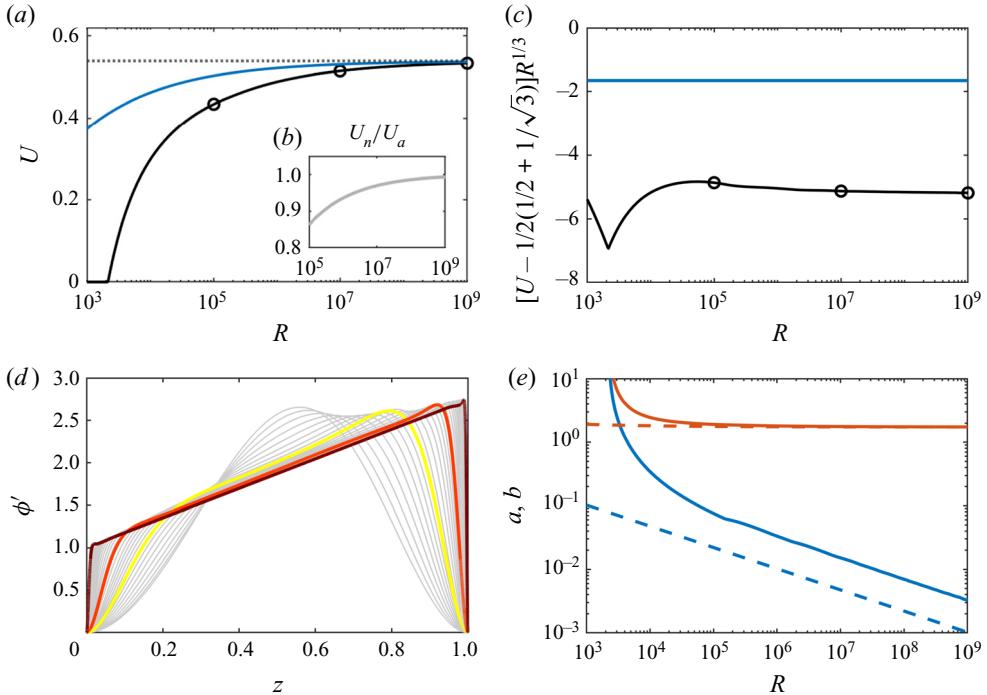


Figure 3. (a) Numerically optimal bounds  $U_n$  computed with QUINOPT (black solid line), compared to the analytical bound  $U_a$  (blue solid line) and the improved uniform upper bound  $\frac{1}{2}(\frac{1}{2} + \frac{1}{\sqrt{3}})$  (dotted line). The inset (b) shows the ratio of the two  $R$ -dependent bounds. (c) Analytical (blue) and numerical (black) corrections to the uniform bound  $\frac{1}{2}(\frac{1}{2} + \frac{1}{\sqrt{3}})$ , compensated by  $R^{1/3}$ . (d) Numerically optimal profiles  $\phi'$  for  $10^3 \leq R \leq 10^9$  (grey). Highlighted profiles for  $R = 10^5$  (yellow),  $R = 10^7$  (red) and  $R = 10^9$  (brown) correspond to the circles in panels (a) and (c). (e) Balance parameters  $a$  (blue solid line, optimal; blue dashed line, analytical) and  $b$  (orange solid line, optimal; orange dashed line, analytical).

Figures 3(d) and 3(e) show the optimal profiles of  $\phi'$  and the optimal balance parameters  $a, b$  in the range of  $R$  spanned by our computations. For large  $R$ , the optimal  $\phi'$  are approximately piecewise linear, corroborating our analytical choice in (4.5a,b), and the optimal balance parameters behave like the analytical ones from § 4 (plotted with dashed lines). The main differences between the optimal and analytical  $\phi'$  profiles are oscillations near the edge of the boundary layers and the fact that the two boundary layers of the optimal  $\phi'$  have different widths. This suggests that a better prefactor for the  $O(R^{-(1/3)})$  term in our analytical bound could be obtained, at the expense of more complicated algebra, by considering boundary layers of different sizes.

## 6. Conclusions

We have proved that the mean convective heat transport  $\langle wT \rangle$  in IH convection with fixed boundary flux is rigorously bounded above by  $\frac{1}{2}(\frac{1}{2} + \frac{1}{\sqrt{3}}) - cR^{-(1/3)}$  uniformly in  $Pr$ , where  $c \approx 1.6552$ . This result is the first to depend explicitly on the Rayleigh number and halves the previous uniform bound  $\langle wT \rangle \leq \frac{1}{2} + \frac{1}{\sqrt{3}}$  (Goluskin 2016) in the infinite- $R$  limit. Our proof relies on the construction of a feasible solution to a convex variational problem, derived by formulating the classical background method as the search for a quadratic

auxiliary function in the form (3.5). Numerical solution of this variational problem yields bounds that approach the same asymptotic value as  $R$  increases and, crucially, appear to do so at the same  $O(R^{-1/3})$  rate. This suggests that our analytical bound is qualitatively optimal within our bounding approach, the only possible improvement being a relatively uninteresting increase in the magnitude of the  $O(R^{-1/3})$  correction to the asymptotic value. In particular, we conclude that the background method (at least as formulated here) cannot prove that  $\langle wT \rangle \leq \frac{1}{2} - O(R^{-1/3})$  as conjectured by Goluskin (2016, § 1.6.3.4).

With the identity (1.1), our upper bound on  $\langle wT \rangle$  can be translated into the lower bound  $\bar{T}_0 - \bar{T}_1 \geq \frac{1}{2}(\frac{1}{2} - \frac{1}{\sqrt{3}}) + 1.6552 R^{-(1/3)}$ . This bound is negative when  $R \geq 78\,390$ , so conduction downwards from the top to the bottom cannot be ruled out in this regime. Determining whether  $\bar{T}_0 - \bar{T}_1$  can indeed be negative or is positive at all Rayleigh numbers, as physical intuition suggests, remains an open question for future work. Possible approaches to answer this question include direct numerical simulations at high  $R$ , the construction of incompressible flows with optimal wall-to-wall transport (Hassanzadeh, Chini & Doering 2014; Tobasco & Doering 2017; Doering & Tobasco 2019), and the computation of certain steady solutions to the Boussinesq equations (2.1a–c), which in Rayleigh–Bénard convection have been shown to transport heat more efficiently than turbulence over a wide range of  $R$  (Wen, Goluskin & Doering 2020). These and other alternatives could provide a crucial understanding of the difference between the conjectured asymptotic value of  $\frac{1}{2}$  for  $\langle wT \rangle$  and the larger asymptotic value,  $\frac{1}{2}(\frac{1}{2} + \frac{1}{\sqrt{3}})$ , of the upper bound proved in this paper.

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