## Structure and X-ray reference diffraction patterns of $(Ba_{6-x}Sr_x)R_2Co_4O_{15}$ (x = 1, 2) (R = lanthanides)

W. Wong-Ng,<sup>1,a)</sup> G. Liu,<sup>2</sup> Y.G. Yan,<sup>3</sup> and J.A. Kaduk<sup>4</sup> <sup>1</sup>Materials Measurement Science Division, NIST, Gaithersburg, Maryland 20899 <sup>2</sup>Beijing National Laboratory for Condensed Matter Physics, Institute of Physics, Chinese Academy of Sciences, Beijing 100190, People's Republic of China <sup>3</sup>State Key Laboratory of Advanced Technology for Materials Synthesis and Processing, Wuhan University of Technology, Wuhan, Hubei 430070, People's Republic of China <sup>4</sup>BCPS, Illinois Institute of Technology, Chicago, Illinois 60616

(Received 16 October 2012; accepted 4 February 2013)

The structure and X-ray patterns of two series of barium lanthanide cobaltates, namely,  $Ba_4Sr_2R_2Co_4O_{15}$  (R = La, Nd, Sm, Eu, Gd, and Dy), and  $Ba_5Sr_2Co_4O_{15}$  (R = La, Nd, Sm, Eu, and Gd) have been determined. These compounds crystallize in the space group  $P6_{3mc}$ ; the unit-cell parameters of Ba<sub>4</sub>Sr<sub>2</sub> $R_2$ Co<sub>4</sub>O<sub>15</sub> (*R* from La to Dy) decrease from a = 11.6128(2) Å to 11. 5266(9) Å, c = 6.86903(11) to 6. 7630(5) Å, and V = 802.23(3) Å<sup>3</sup> to 778.17(15) Å<sup>3</sup>, respectively. In the Ba<sub>5</sub>SrR<sub>2</sub>Co<sub>4</sub>O<sub>15</sub> series (R = La to Gd), the unit-cell parameters decrease from a = 11.735 44(14) Å to 11.619 79(12) Å, c = 6.942 89 (14) Å to 6.836 52(8) Å, and V = 828.08(3) Å<sup>3</sup> to 799.40(2) Å<sup>3</sup>. In the general structure of  $(Ba_{6-x}Sr_x)R_2Co_4O_{15}$ , there are four Co ions per formula unit occupying one  $CoO_6$  octahedral and three  $CoO_4$  tetrahedral units. Through corner-sharing of these polyhedra, a larger  $Co_4O_{15}$  unit is formed.  $Sr^{2+}$  ions adopt both octahedral and 8-fold coordination environment.  $R^{3+}$  ions adopt 8-fold coordination (mixed site with Sr), while the larger Ba<sup>2+</sup> ions assume both 10and 11-fold coordination environments. The samples were found to be insulators. X-ray diffraction patterns of these samples have been determined and submitted to the Powder Diffraction File (PDF). © 2013 International Centre for Diffraction Data. [doi:10.1017/S0885715613000171]

Key words: X-ray reference diffraction patterns,  $(Ba_{6-x}Sr_x)R_2Co_4O_{15}$  (x = 1, 2) (R = La, Nd, Sm, Eu, and Gd), crystal structure

### **I. INTRODUCTION**

Continuing demands for environmentally friendly alternative-energy technologies have led to increased activities in the area of thermoelectric (TE) research. For high-temperature waste-heat conversion applications, low-dimensional layered oxides have been found to have relatively high efficiency. The efficiency and performance of TE energy conversion or cooling is related to the dimensionless figure of merit (ZT) of the TE materials, given by  $ZT = S^2 \sigma T / \kappa$ , where T is the absolute temperature, S is the Seebeck coefficient or TE power,  $\sigma$  is the electrical conductivity, and k is the thermal conductivity (Nolas et al., 2001). Examples of these oxides include  $NaCoO_x$  (Terasaki et al., 1997), Ca<sub>2</sub>Co<sub>3</sub>O<sub>6</sub> (Mikami et al., 2003; Mikami and Funahashi, 2005), and Ca<sub>3</sub>Co<sub>4</sub>O<sub>9</sub> (Masset et al., 2000; Minami et al., 2002; Grebille et al., 2004; Hu et al., 2005). Among these materials, the most efficient material,  $Ca_3Co_4O_9$ , is a misfit layered oxide that has two monoclinical subsystems with identical a, c,  $\beta$ , but different b (Masset et al., 2000). However, to have materials with high enough efficiency for large-scale industrial applications, ZT of two or higher is a requirement.

The search for cobaltate compounds with improved TE properties continues worldwide. The goal of this paper is two-fold. Firstly,  $(Ba_{6-x}Sr_x)R_2Co_4O_{15}$  (x = 1, 2) compounds are investigated for their structures. The structures of Ba<sub>6</sub>La<sub>2</sub>Co<sub>4</sub>O<sub>15</sub> and Ba<sub>5</sub>CaNd<sub>2</sub>Co<sub>4</sub>O<sub>15</sub> have been reported by Mevs and Müller-Buschbaum (1990a), and Müller-Buschbaum and Martin (1992). Since X-ray diffraction is a non-destructive technique for phase identification, X-ray diffraction patterns are especially important for phase characterization, therefore another goal of this investigation was to determine the experimental patterns for  $Ba_4Sr_2R_2Co_4O_{15}$  (R = La, Nd, Sm, Gd, and Dy), and  $Ba_5SrR_2Co_4O_{15}$  (R = La, Nd, Sm, Eu, and Gd), and to make them widely available through submission to the Powder Diffraction File (PDF) (ICDD).

#### **II. EXPERIMENTAL**

#### A. Sample preparation

All samples were prepared by heating a stoichiometric mixture of BaCO<sub>3</sub>  $R_2O_3$  (R = La, Nd, Sm, Eu, Gd, Dy, Ho, Y, Er, Tm, Yb, and Lu), and  $Co_3O_4$  in air.  $La_2O_3$  and  $Nd_2O_3$  were first heat treated at 550 °C overnight prior to use to ensure the absence of carbonates and hydroxides. Samples were weighed, well-mixed, and calcined at 800 °C for one day, 950 °C for one day, and subsequently at 980 °C, with intermediate grindings and pelletizations, for another 6 days. During each heat treatment, all samples were furnace cooled. The phase purity of the samples was established by powder X-ray diffraction.

<sup>&</sup>lt;sup>a)</sup>Author to whom correspondence should be addressed. Electronic mail: winnie.wong-ng@nist.gov

# B. X-ray Rietveld refinements and powder reference patterns

The Ba<sub>4</sub>Sr<sub>2</sub> $R_2$ Co<sub>4</sub>O<sub>15</sub> (R = La, Nd, Sm, Eu, and Gd) and Ba<sub>5</sub>Sr $R_2$ Co<sub>4</sub>O<sub>15</sub> (R = La, Nd, Sm, Eu, Gd, and Dy) powders were mounted as ethanol slurries on zero-background cells. The X-ray powder patterns of the former samples were measured on a Bruker D2 Phaser diffractometer. The X-ray powder patterns of the latter group of samples were measured at ambient conditions on a Panalytical X'Pert Pro MPD diffractometer equipped with a PIXcel positionsensitive detector and an Anton Paar HTK1200N furnace. Patterns were measured (Cu $K\alpha$  radiation, 45 kV, 40 mA, 0.5° divergence slit, and 0.02 rad Soller slits) from 5 to 130°2 $\theta$  in 0.02° steps.

The Rietveld refinement technique (Rietveld, 1969) with the software suite GSAS (Larson and von Dreele, 2004) was used to determine the structure of  $(Ba_{6-x}Sr_x)R_2Co_4O_{15}$ . A structural model of  $Ba_5SrPr_2Co_4O_{15}$  reported previously (Müller-Buschbaum and Uensal, 1996) was used for structural refinements. Reference patterns were obtained with a Rietveld pattern decomposition technique. Using this technique, the reported peak positions were derived from the extracted integrated intensities, and positions calculated from the unit-cell parameters. When peaks are not resolved at the resolution function, the intensities are summed, and an intensityweighted *d*-spacing is reported. They are also corrected for systematic errors both in *d*-spacing and intensity. In summary, these patterns represent ideal specimen patterns.

#### C. Bond valence sum (V<sub>b</sub>) calculation

The bond valence sum values,  $V_b$ , for the Ba, R, and Co sites were calculated using the Brown–Altermatt empirical expression (Brown and Altermatt, 1985; Brese and O'Keeffe, 1991). The  $V_b$  of an atom i is defined as the sum of the bond valences  $v_{ij}$  of all the bonds from atoms i to atoms j. The most commonly adopted empirical expression for bond valence  $v_{ij}$ as a function of the interatomic distance  $d_{ij}$  is  $v_{ij} = \exp [(R_0 - d_{ij})/B]$ . The parameter, B, is commonly taken to be a "universal" constant equal to 0.37 Å. The values for the reference distance  $R_0$  (Å) for Ba–O, Sr–O, Co<sup>2+</sup>–O, Co<sup>3+</sup>–O, La–O, Nd–O, Sm–O, Eu–O, Gd–O, and Dy–O are 2.29, 2.118, 1.692, 1.70, 2.172, 2.117, 2.088, 2.076, 2.065, and 2.036, respectively (Brown and Altermatt, 1985; Brese and O'Keeffe, 1991).

#### **III. RESULTS AND DISCUSSION**

Phases for Ba<sub>4</sub>Sr<sub>2</sub> $R_2$ Co<sub>4</sub>O<sub>15</sub>, and Ba<sub>5</sub>Sr $R_2$ Co<sub>4</sub>O<sub>15</sub> were successfully prepared only for compounds with relatively larger size of *R*. Based on X-ray diffraction results, in Ba<sub>4</sub>Sr<sub>2</sub> $R_2$ Co<sub>4</sub>O<sub>15</sub>, compounds with R = Dy, Ho, Er, Yb, Tm, and Lu, and in Ba<sub>5</sub>Sr $R_2$ Co<sub>4</sub>O<sub>15</sub>, compounds with R = Ho,

TABLE I. Refinement residuals and phases present for (a)  $Ba_4Sr_2R_2Co_4O_{15}$  and (b)  $Ba_5SrR_2Co_4O_{15}$ . Values inside brackets are standard deviations.

(a) $Ba_4Sr_2R_2Co_4O_{15}$						
R	La	Nd	Sm	Eu	Gd	Dy
R <sub>wp</sub>	0.0688	0.0116	0.0293	0.0258	0.0257	0.0226
Rp	0.0458	0.0088	0.0220	0.0195	0.0194	0.0177
$\chi^2$	2.354	2.990	2.056	2.238	2.231	2.497
R(F)	0.0401	0.0300	0.1159	0.0782	0.0708	0.1059
$R(F^2)$	0.0705	0.0745	0.1728	0.1291	0.1176	0.1575
$\Delta F(+), e Å^{-3}$	4.0	1.52	6.36	3.79	3.35	4.06
$\Delta F(-), e Å^{-3}$	-6.6	-1.43	-6.15	-2.87	-2.60	-7.10
Impurities (% mass fraction)						
(Ba,Sr)CoO <sub>4</sub>	-	4.1(1)	-	-	-	15.9(4)
$R_2O_3$	-	0.7(1)	-	-	-	-
BaSrCo <sub>2</sub> O <sub>6</sub>	-	0.7(1)	-	-	-	-
CoO	-	1.2(1)	-	-	-	_
BaCoO <sub>x</sub>	0.1(1)	-	-	-	-	-
$BaR_2O_4$	1.2(1)	-	-	-	-	-
Ba <sub>2</sub> CoO <sub>4</sub>	6.9(1)	-	-	-	-	_
(b) $Ba_5SrR_2Co_4O_{15}$						
Rwp	0.1249	0.0654	0.0582	0.0767	0.0498	
Rp	0.0972	0.0496	0.0451	0.0598	0.0386	
χ2	1.492	2.429	2.265	1.527	1.712	
R(F)	0.0585	0.0268	0.0240	0.0299	0.0251	
$R(F^2)$	0.0985	0.0492	0.0451	0.0538	0.0440	
$DF(+), eÅ^{-3}$	4.2	1.9	1.9	2.2	2.2	
$DF(-), eÅ^{-3}$	-2.6	-1.9	-2.2	-3.1	-2.3	
Impurities (% mass fraction)						
(Ba, Sr)CoO <sub>3</sub>	0.6(1)	0.2(1)	2.9(1)	4.9(1)	3.5(1)	
BaCO <sub>3</sub>	0.5(1)	2.1(1)	1.6(1)	1.6(1)	1.9(1)	
BaR2CoO <sub>5</sub>	0.3(1)	1.6(1)	-	-	-	
BaCoOx	0.3(1)	2.1(1)	0.6(1)	1.1(1)	0.5(1)	
$BaR_2O_4$	-	2.1(1)	-	-	-	
$R_2O_3$	_	-	0.6(1)	0.5(1)	0.7(1)	



Figure 1. Observed (crosses), calculated (solid line), and difference XRD pattern (bottom) for  $Ba_5SrSm_2Co_4O_{15}$  by Rietveld analysis technique. The difference pattern is plotted at the same scale as the other patterns up to  $70^{\circ}$  2 $\theta$ . At higher  $2\theta$  angles, the scale has been magnified five times. Phases present are indicated next to the rows of tick marks (from bottom to top:  $Ba_5SrSm_2Co_4O_{15}$ , (Ba, Sr)CoO<sub>3</sub>, BaCO<sub>3</sub>, BaSm\_2CoO<sub>5</sub>, BaCoO<sub>x</sub>, and Sm<sub>2</sub>O<sub>3</sub>).

Er, Yb, Tm, and Lu cannot be made at all under the current synthesis conditions. X-ray diffraction data of each Ba<sub>4</sub>Sr<sub>2</sub> $R_2$ Co<sub>4</sub>O<sub>15</sub> and Ba<sub>5</sub>Sr $R_2$ Co<sub>4</sub>O<sub>15</sub> were indexable with a hexagonal unit cell and with a space group of  $P6_3mc$  (No. 186). X-ray patterns of the composition of the Ho-analog, Ba<sub>4</sub>Sr<sub>2</sub>Ho<sub>2</sub>Co<sub>4</sub>O<sub>15</sub>, indicate a different structure. The major product of this preparation has the *P*4mm SrHoO3 type structure, with a = 4.1301(1), c = 4.1430(2) Å, and V = 70.670(5) Å<sup>3</sup>. Refinement of this structure indicated that the A site was occupied by Sr, and that the oxygen sites were fully occupied. This sample contains 5.9(1)% mass fraction of BaSrHo<sub>4</sub>O<sub>8</sub>, 3.4(1)% mass fraction of CaCoO<sub>2+x</sub>, and 0.8(1)% mass fraction of a spinel, and traces of additional phases.

The samples are essentially isolators as they are very resistive and no reasonable Seebeck coefficient signal could be obtained.

### A. Structure of Ba<sub>6-x</sub>(Sr,Ca)<sub>x</sub>R<sub>2</sub>Co<sub>4</sub>O<sub>15</sub>

Table I gives the refinement residuals for  $Ba_4Sr_2R_2Co_4O_{15}$  and  $Ba_5SrR_2Co_4O_{15}$ . Figure 1 provides the

TABLE II. Unit cell parameters of  $Ba_4Sr_2R_2Co_4O_{15}$  and  $Ba_5SrR_2Co_4O_{15}$  (P6<sub>3</sub>mc (No. 186), Z=2),  $D_x$  refers to calculated density. Values inside brackets are standard deviations.

Compounds	<i>a</i> (Å)	<i>c</i> (Å)	$V(\text{\AA}^3)$	$D_x$ (g cm <sup>-3</sup> )	r(R <sup>3+</sup> ) (VIII-coord)
Ba <sub>4</sub> Sr <sub>2</sub> La <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.7022(1)	6.908 36(8)	819.30(2)	5.991	1.160
Ba <sub>4</sub> Sr <sub>2</sub> Nd <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.6457(2)	6.861 45(11)	805.90(3)	6.135	1.109
Ba <sub>4</sub> Sr <sub>2</sub> Sm <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.6121(8)	6.8392(5)	798.66(14)	6.242	1.079
Ba <sub>4</sub> Sr <sub>2</sub> Eu <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.5940(4)	6.8210(2)	794.05(6)	6.291	1.066
Ba <sub>4</sub> Sr <sub>2</sub> Gd <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.5872(4)	6.8169(2)	792.63(6)	6.342	1.053
Ba <sub>4</sub> Sr <sub>2</sub> Dy <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.5266(9)	6.7630(5)	778.2(2)	6.508	1.027
Ba <sub>5</sub> SrLa <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.7354(2)	6.942 89(14)	828.08(3)	6.127	1.160
Ba <sub>5</sub> SrNd <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.672 18(12)	6.886 89(8)	812.56(2)	6.288	1.109
Ba <sub>5</sub> SrSm <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.640 12(12)	6.860 26(8)	804.98(2)	6.398	1.079
Ba <sub>5</sub> SrEu <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.6250(2)	6.841 91(12)	800.75(3)	6.445	1.066
Ba <sub>5</sub> SrGd <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	11.619 79(12)	6.836 52(8)	799.40(2)	6.500	1.053



Figure 2. Plot of unit-cell volume of (a)  $Ba_4Sr_2R_2Co_4O_{15}$  and (b)  $Ba_5SrR_2Co_4O_{15}$  vs.  $r(R^{3+})$  [where "r" is the Shannon Ionic Radii (1976)].

TABLE III(a).	Atomic coordinates	and isotropic	displacement	factors for	$Ba_4Sr_2R_2$	C04O15; va	alues inside	brackets are	standard deviations.
---------------	--------------------	---------------	--------------	-------------	---------------	------------	--------------	--------------	----------------------

Atom	x	у	Z	Occupied	$U_{ m iso}$	Site
(i) $R = La$						
Sr1	0.0	0.0	-0.0048	1.0	0.0055(2)	2a
Ba2	0.174 78(6)	0.825 22(6)	0.1700(5)	1.0	0.0055(2)	6c
Ba3	0.333 33	0.666 67	0.4801(5)	1.0	0.0055(2)	2b
Sr4	0.475 99(6)	0.524 01(6)	0.8255(4)	0.333 33	0.0055(2)	6c
La5	0.475 99(6)	0.524 01(6)	0.8255(4)	0.666 67	0.0055(2)	6c
C06	0.333 33	0.666 67	-0.0079(9)	1.0	0.0035(2)	2b
Co7	0.175 15(14)	0.824 85(14)	0.6544(7)	1.0	0.0035(2)	6c
08	0.6684(6)	0.0733(6)	0.0280(9)	1.0	0.01	12d
O9	0.2465(3)	0.7535(3)	0.8397(11)	1.0	0.01	6c
O10	0.4130(3)	0.5870(3)	0.1502(11)	1.0	0.01	6c
011	0.9053(4)	0.0947(4)	0.2491(12)	1.0	0.01	6c
(ii) $R = Nd$						
Sr1	0.0	0.0	0.0	1.0	0.0157(4)	2a
Ba2	0.174 53(8)	0.825 47(8)	0.1757(6)	1.0	0.0157(4)	6c
Ba3	0.333 33	0.666 67	0.4875(6)	1.0	0.0157(4)	2b
Sr4	0.476 17(7)	0.523 83(7)	0.8320(6)	0.333 33	0.0103(5)	6c
Nd5	0.476 17(7)	0.523 83(7)	0.8320(6)	0.666 67	0.0103(5)	6c
Co6	0.333 33	0.666 67	-0.0101(10)	1.0	0.0090(8)	2b
Co7	0.1759(2)	0.8241(2)	0.6563(10)	1.0	0.0090(8)	6c
08	0.6658(6)	0.0673(6)	0.0306(10)	1.0	0.01	12d
09	0.2469(3)	0.7531(3)	0.8387(13)	1.0	0.01	6c
O10	0.4105(4)	0.5895(4)	0.1618(14)	1.0	0.01	6c
011	0.9040(4)	0.0960(4)	0.2571(14)	1.0	0.01	6c
(iii) $R = Sm$						
Sr1	0.0	0.0	0.0	1.0	0.01	2a
Ba2	0.1742(2)	0.8259(2)	0.179(2)	1.0	0.01	6c
Ba3	0.333 33	0.666 67	0.498(2)	1.0	0.01	2b
Sr4	0.4763(2)	0.5237(2)	0.833(2)	0.333 33	0.01	6c
Sm5	0.4763(2)	0.5237(2)	0.833(2)	0.666 67	0.01	6c
C06	0.333 33	0.666 67	-0.032(2)	1.0	0.01	2b
Co7	0.1763(4)	0.8237(4)	0.651(2)	1.0	0.01	6c
08	0.6553(7)	0.0789(8)	0.039(2)	1.0	0.01	12d
09	0.2424(3)	0.7576(3)	0.842(2)	1.0	0.01	6c
O10	0.4107(4)	0.5893(4)	0.148(2)	1.0	0.01	6c
011	0.9067(5)	0.0933(5)	0.256(2)	1.0	0.01	6c
(iv) $R = Eu$	. ,					
Sr1	0.0	0.0	0.0	1.0	0.018 16	2a
Ba2	0.1744(2)	0.8256(2)	0.1788(13)	1.0	0.018 16	6c
Ba3	0.333 33	0.666 67	0.4936(11)	1.0	0.018 16	2b
Sr4	0.475 78(14)	0.524 22(14)	0.8338(12)	0.333 33	0.005 05	6c
Eu5	0.475 78(14)	0.524 22(14)	0.8338(12)	0.666 67	0.005 05	6c
Co6	0.333 33	0.666 67	-0.0226(14)	1.0	0.005	2b
Co7	0.1759(3)	0.8241(3)	0.654(2)	1.0	0.005	6c
08	0.6569(6)	0.0766(8)	0.0406(15)	1.0	0.01	12d
09	0.2459(3)	0.7541(3)	0.837(2)	1.0	0.01	6c
O10	0.4111(4)	0.5889(4)	0.153(2)	1.0	0.01	6c
011	0.9061(5)	0.0939(5)	0.258(2)	1.0	0.01	6c
(v) $\mathbf{R} = \mathbf{G}\mathbf{d}$						
Sr1	0.0	0.0	0.0	1.0	0.0131(8)	2a
Ba2	0.1744(2)	0.8256(2)	0.1785(13)	1.0	0.0131(8)	6c
Ba3	0.333 33	0.666 67	0.4937(12)	1.0	0.0131(8)	2b
Sr4	0.475 82(15)	0.524 17(15)	0.8337(12)	0.333 33	0.0064(10)	6c
Gd5	0.475 82(15)	0.524 17(15)	0.8337(12)	0.666 67	0.0064(10)	6c
Co6	0.333 33	0.666 67	-0.0219(15)	1.0	0.005	2b
Co7	0.1761(3)	0.8239(3)	0.654(2)	1.0	0.005	6c
O8	0.6568(7)	0.0768(8)	0.040(2)	1.0	0.019(4)	12d
O9	0.2463(3)	0.7537(3)	0.836(2)	1.0	0.019(4)	6c
O10	0.4110(4)	0.5890(4)	0.154(2)	1.0	0.019(4)	6c
O11	0.9060(5)	0.0940(5)	0.257(2)	1.0	0.019(4)	6c
(vi) $R = Dy$						
Sr1	0.0	0.0	0.0	1.0	0.013 14	2a
Ba2	0.1734(4)	0.8266(4)	0.178(3)	1.0	0.013 14	6c
Ba3	0.333 33	0.666 67	0.486(2)	1.0	0.013 14	2b
Sr4	0.4742(3)	0.5258(3)	0.839(2)	0.333 33	0.006 43	6c
Dy5	0.4742(3)	0.5258(3)	0.839(2)	0.666 67	0.006 43	6c

TABLE III(a). Continued

Atom	x	у	Z	Occupied	$U_{ m iso}$	Site
Co6	0.333 33	0.666 67	0.018(2)	1.0	0.005	2b
Co7	0.1837(5)	0.8163(5)	0.668(3)	1.0	0.005	6c
08	0.6516(8)	0.0802(9)	0.042(3)	1.0	0.019 25	12d
09	0.2636(4)	0.7364(4)	0.820(3)	1.0	0.019 25	6c
O10	0.4125(4)	0.5875(4)	0.177(3)	1.0	0.019 25	6c
O11	0.9031(6)	0.0969(6)	0.251(2)	1.0	0.019 25	6c

Rietveld refinement results for  $Ba_5SrSm_2Co_4O_{15}$  as an example. The observed (crosses), calculated (solid line), and difference XRD patterns (bottom) for  $Ba_5SrSm_2Co_4O_{15}$ , as determined by the Rietveld analysis technique, are shown. The difference pattern is plotted at the same scale as the other patterns up to  $70^{\circ}2\theta$ . At higher  $2\theta$  angles, the scale has been magnified five times. The rows of tick marks refer to the calculated peak positions. The refinement residuals

mainly reflect variations in the counting times, and the presence of traces of additional impurities as indicated.

Table II lists the unit-cell parameters for  $Ba_4Sr_2R_2Co_4O_{15}$ and  $Ba_5SrR_2Co_4O_{15}$ . The calculated density values,  $D_{\infty}$  in both series increase as the size of *R* decreases. Figure 2 gives the plot of the unit-cell volumes, *V*, of  $Ba_4Sr_2R_2Co_4O_{15}$  and  $Ba_5SrR_2Co_4O_{15}$  vs. Shannon ionic radius,  $r(R^{3+})$ . The unit-cell volume decreases across the lanthanide series from La to Dy,

TABLE III(b). Atomic coordinates and isotropic displacement factors for  $Ba_5SrR_2Co_4O_{15}$ . Values inside brackets are standard deviations.

Atom	x	у	Z	Occupied	$U_{ m iso}$	Site
(i) $R = La$						
Ba1/Sr2	0.0	0.0	-0.0048	0.5/0.5	0.0067(4)	2a
Ba3	0.174 56(11)	0.825 44(11)	0.1617(8)	1.0	0.0067(4)	6c
Ba5	0.333 33	0.666 67	0.4745(8)	1.0	0.0067(4)	2b
Ba7	0.475 84(11)	0.524 16(11)	0.8164(7)	0.166 67	0.0067(4)	6c
Sr8	0.475 84(11)	0.524 16(11)	0.8164(7)	0.166 67	0.0067(4)	6c
La9	0.475 84(11)	0.524 16(11)	0.8164(7)	0.666 67	0.0067(4)	6c
Co10	0.333 33	0.666 67	-0.0431(10)	1.0	0.0046(4)	2b
Co11	0.177 35(25)	0.822 65(25)	0.6374(11)	1.0	0.0046(4)	6c
O12	0.6609(5)	0.0800(6)	0.0241(11)	1.0	0.01	12d
O13	0.242 42(25)	0.757 58(25)	0.8301(12)	1.0	0.01	6c
O14	0.412 54(28)	0.587 45(28)	0.1238(11)	1.0	0.01	6c
015	0.9005(4)	0.0995(4)	0.2504(14)	1.0	0.01	6c
(ii) $R = Nd$						
Ba1/Sr2	0.0	0.0	-0.0048	0.5/0.5	0.004 13(17)	2a
Ba3	0.174 70(6)	0.825 30(6)	0.1558(5)	1.0	0.004 13(17)	6c
Ba5	0.333 33	0.666 67	0.4669(5)	1.0	0.004 13(17)	2b
Ba7	0.475 66(6)	0.524 34(6)	0.8150(4)	0.166 67	0.004 13(17)	6c
Sr8	0.475 66(6)	0.524 34(6)	0.8150(4)	0.166 67	0.004 13(17)	6c
Nd9	0.475 66(6)	0.524 34(6)	0.8150(4)	0.666 67	0.004 13(17)	6c
Co10	0.333 33	0.666 67	-0.0126(9)	1.0	0.002 11(17)	2b
Co11	0.176 95(15)	0.823 05(15)	0.6457(8)	1.0	0.002 11(17)	6c
012	0.6663(6)	0.0705(6)	0.0195(9)	1.0	0.01	12d
013	0.250 53(29)	0.749 47(29)	0.8248(11)	1.0	0.01	6c
014	0.413 57(32)	0.586 42(32)	0.1403(12)	1.0	0.01	6c
015	0.9030(4)	0.0970(4)	0.2462(13)	1.0	0.01	6c
(iii) $R = Sm$						
Ba1/Sr2	0.0	0.0	-0.0048	0.5/0.5	0.00673(16)	2a
Ba3	0.174 92(6)	0.825 08(6)	0.1533(4)	1.0	0.00673(16)	6c
Ba5	0.333 33	0.666 67	0.4660(4)	1.0	0.006 73(16)	2b
Ba7	0.47573(5)	0.524 27(5)	0.8167(4)	0.166 67	0.00673(16)	6c
Sr8	0.47573(5)	0.524 27(5)	0.8167(4)	0.166 67	0.00673(16)	6c
Sm9	0.475 73(5)	0.524 27(5)	0.8167(4)	0.666 67	0.006 73(16)	6c
Co10	0.333 33	0.666 67	-0.0071(8)	1.0	0.004 72(16)	2b
Co11	0.176 54(14)	0.823 46(14)	0.6490(8)	1.0	0.004 72(16)	6c
012	0.6672(5)	0.0708(6)	0.0193(8)	1.0	0.0032(13)	12d
013	0.25174(27)	0.748 26(27)	0.8267(11)	1.0	0.0032(13)	6c
O14	0.413 78(30)	0.586 22(30)	0.1418(11)	1.0	0.0032(13)	6c
015	0.902 40(34)	0.097 60(34)	0.2519(12)	1.0	0.0032(13)	6c
(iv) $R = Eu$						
Ba1/Sr2	0.0	0.0	-0.0048	0.5/0.5	0.0065(2)	2a
Ba3	0.174 41(8)	0.825 59(8)	0.1560(6)	1.0	0.0065(2)	 6c
Ba5	0.333 33	0.666 67	0.4711(5)	1.0	0.0065(2)	2h

TABLE III(b). Continued

Atom	X	у	z	Occupied	$U_{ m iso}$	Site
Ba7	0.475 59(8)	0.52441(8)	0.8168(5)	0.166 67	0.0065(2)	6c
Sr8	0.475 59(8)	0.52441(8)	0.8168(5)	0.166 67	0.0065(2)	6c
Eu9	0.475 59(8)	0.52441(8)	0.8168(5)	0.666 67	0.0065(2)	6c
Co10	0.333 33	0.666 67	-0.0264(9)	1.0	0.0045(2)	2b
Co11	0.176 93(18)	0.823 07(18)	0.6401(9)	1.0	0.0045(2)	6c
012	0.6625(5)	0.0753(6)	0.0212(9)	1.0	0.01	12d
013	0.250 57(24)	0.749 43(24)	0.8176(10)	1.0	0.01	6c
O14	0.410 90(28)	0.589 10(28)	0.1380(10)	1.0	0.01	6c
015	0.901 80(34)	0.098 20(34)	0.2509(13)	1.0	0.01	6c
(v) $R = Gd$						
Ba1/Sr2	0.0	0.0	-0.0048	0.5/0.5	0.008 39(18)	2a
Ba3	0.174 81(6)	0.825 19(6)	0.1552(4)	1.0	0.008 39(18)	6c
Ba5	0.333 33	0.666 67	0.4687(4)	1.0	0.008 39(18)	2b
Ba7	0.475 55(6)	0.524 45(6)	0.8185(4)	0.166 67	0.008 39(18)	6c
Sr8	0.475 55(6)	0.524 45(6)	0.8185(4)	0.166 67	0.008 39(18)	6c
Gd9	0.475 55(6)	0.524 45(6)	0.8185(4)	0.666 67	0.008 39(18)	6c
Co10	0.333 33	0.666 67	-0.0136(8)	1.0	0.006 37(18)	2b
Co11	0.176 87(14)	0.823 13(14)	0.6455(8)	1.0	0.006 37(18)	6c
012	0.6648(5)	0.0698(5)	0.0214(8)	1.0	0.01	12d
013	0.252 48(24)	0.747 52(24)	0.8213(10)	1.0	0.01	6c
O14	0.412 47(28)	0.587 53(28)	0.1416(10)	1.0	0.01	6c
015	0.902 24(32)	0.097 76(32)	0.2513(11)	1.0	0.01	6c

or with the decreasing size of the ionic radius (Shannon, 1976) (lanthanide contraction) of the metal ion at the octahedral site. This decreasing volume is a result of the decrease in both the a-and the c-parameters.

The atomic coordinates, displacement parameters for the structures of Ba<sub>4</sub>Sr<sub>2</sub>R<sub>2</sub>Co<sub>4</sub>O<sub>15</sub> and Ba<sub>5</sub>SrR<sub>2</sub>Co<sub>4</sub>O<sub>15</sub> are given in Tables III(a) and 3(b).  $Ba_4Sr_2R_2Co_4O_{15}$  and  $Ba_5SrR_2Co_4O_{15}$  are isostructural with Ba<sub>6</sub>R<sub>2</sub>Fe<sub>4</sub>O<sub>15</sub> (Rüter and Müller-Buschbaum, 1990; Mevs and Müller-Buschbaum, 1990b, 1990c, 1992; Abe *et al.*, 2006). The structure of  $Ba_{6-x}Sr_xR_2Co_4O_{15}$  in general consists of two crystallographically independent Co sites, one is 6-fold, while the other is 4-fold coordinated. The CoO<sub>6</sub> octahedra and  $CoO_4$  tetrahedra are linked by corner-shared oxygen ions. Specifically, a CoO<sub>6</sub> octahedron in the center can be viewed as sharing three corners of its triangular face with three tetrahedral  $CoO_4$  units, leading to a  $Co_4O_{15}$  cluster (Figure 3). In Ba<sub>4</sub>Sr<sub>2</sub>R<sub>2</sub>Co<sub>4</sub>O<sub>15</sub>, all R sites are mixed with Sr (randomly occupied by 2/3R and 1/3Sr), while in Ba<sub>5</sub>SrR<sub>2</sub>Co<sub>4</sub>O<sub>15</sub>, all R sites are mixed with Ba and Sr (randomly occupied by 2/3R, 1/6Ba, and 1/6Sr). Figure 4 gives the structure of  $(Ba_{6-x}Sr_x)R_2Co_4O_{15}$ as viewed along the *c*-axis. It features six units of  $Co_4O_{15}$  and seven SrO<sub>6</sub> octahedral units viewed along the *b*-axis. For clarity,



Figure 3. The structure motif of  $Co_4O_{15}$  which consists of three corner-shared  $[CoO_4]$  tetrahedral units with one  $CoO_6$  octahedral unit at the center.



Figure 4. Crystal structure of  $Ba_4Sr_2R_2Co_4O_{15}$  at room temperature showing the unit cell outline, and different coordination environment of tetrahedral [CoO<sub>4</sub>] and octahedral [CoO<sub>6</sub>] units. The 8-fold coordinated (*R*, Sr)O<sub>8</sub> bisdisphenoids and BaO<sub>10</sub> and BaO<sub>12</sub> polyhedra were not shown for clarity.



Figure 5. Crystal structure of  $Ba_4Sr_2Gd_2Co_4O_{15}$  at room temperature showing the capped trigonal prism  $BaO_{10}$  and cubic close packed  $BaO_{12}$  coordination environment.

TABLE IV(a).	Bond distances and bond valence sum values $(V_b)$ for
Ba <sub>4</sub> Sr <sub>2</sub> R <sub>2</sub> Co <sub>4</sub> O <sub>15</sub>	. Values inside brackets are standard deviations.

TABLE IV(a). Continued

Atom	Atom	Distances	Vh	Atom	Atom	Distances	$V_{\mathrm{b}}$
$\overline{(i)} P - I c$			. 0		O11	1.818(8)	
(1) $K = La$ Sr1	011	$2.601(8) \times 3$	1 710	(iv) $R = Eu$	011	0.555(10) 0	1.010
511	011	$2.565(7) \times 3$	1.,10	Srl	011	$2.5/7(12) \times 3$ $2.508(0) \times 3$	1.913
Ba2	08	2.970(6) × 2	1.772	Ba2	08	$2.508(9) \times 3$ 3.028(8) $\times 2$	1 711
		$2.952(6) \times 2$		542	00	$2.998(8) \times 2$	1.711
	09	2.706(8)			O9	2.739(10)	
	O10	$2.7866(10) \times 2$			O10	$2.770(3) \times 2$	
	011	$3.120(2) \times 2$ 3.220(0)			011	$3.083(3) \times 2$	
Ba3	08	3.072(6) × 6	1 886	5.4	0.0	3.296(15)	
Das	08	$3.044(7) \times 3$	1.000	Ba3	08	$2.939(8) \times 6$	2.332
	010	$2.793(7) \times 3$			09	$2.926(9) \times 3$ 2.800(0) × 3	
La5/Sr4	08	$2.582(6) \times 2$	3.002	Fu5/Sr/	010	$2.800(9) \times 3$ $2.444(7) \times 2$	3 027
		2.418(5) × 2		Eu5/514	08	$2.336(7) \times 2$	5.027
	O9	$2.5256(12) \times 2$			09	$2.499(3) \times 2$	
	O10	2.581(7)			O10	2.535(10)	
<b>a</b> (	0.0	2.555(7)				2.584(8)	
C06	09	$2.051(6) \times 3$	2.692	Co6	O9	$2.001(7) \times 3$	2.780
Co7	010	$1.949(7) \times 3$ 1.821(5) × 2	2 700		O104	$1.969(8) \times 3$	
01	09	1.031(3) × 2	2.199	Co7	08	$1.858(6) \times 2$	2.709
	011	1.756(7)			09	1.877(7)	
(iii) $R - Nd$	011	1.150(1)		$(\mathbf{v}) \mathbf{P} - \mathbf{C} \mathbf{d}$	011	1.790(8)	
Sr1	011	2.619(9) × 3	1.695	(V) K = Gu	011	$2573(12) \times 3$	1 91/
511	011	$2.555(8) \times 3$	11070	511	011	$2.575(12) \times 3$	1.914
Ba2	08	$2.910(7) \times 2$	1.851	Ba2	08	$3.029(8) \times 2$	1.713
		2.937(7) × 2				$2.996(8) \times 2$	
	O9	2.735(9)			O9	2.744(10)	
	O10	$2.7761(14) \times 2$			O10	$2.768(3) \times 2$	
	011	$3.104(2) \times 2$			011	$3.080(3) \times 2$	
	0.0	3.280(10)	1 0 5 2			3.296(15)	
Ba3	08	$3.10/(6) \times 6$ $2.074(0) \times 2$	1.953	Ba3	08	$2.934(8) \times 6$	2.378
	09	$2.974(9) \times 3$ $2.723(0) \times 3$			09	$2.916(9) \times 3$ $2.702(0) \times 2$	
Nd5/Sr4	010	$2.725(9) \times 3$ 2.586(6) × 2	2 842	Gd5/Sr4	010	$2.792(9) \times 3$ $2.442(7) \times 2$	2 083
1100/011	00	$2.359(6) \times 2$	2.012	005/514	00	$2.442(7) \times 2$ 2 333(7) × 2	2.905
	09	$2.5140(14) \times 2$			09	$2.393(7) \times 2$ $2.497(3) \times 2$	
	O10	2.622(9)			010	2.541(10)	
		2.567(8)				2.581(8)	
C06	O9	$2.029(7) \times 3$	2.747	Co6	O9	$1.997(7) \times 3$	2.806
	O10	$1.953(8) \times 3$			O10	$1.966(8) \times 3$	
Co7	08	$1.847(6) \times 2$	2.788	Co7	08	$1.857(6) \times 2$	2.714
	09	1.902(7)			09	1.876(7)	
	011	1./54(/)			011	1.790(8)	
(iii) $R = Sm$	0.14	0.5(1/10) 0	1 0 0 0	(V1) K = Dy	011	$2576(14) \times 2$	1 760
Srl	011	$2.564(13) \times 3$	1.930	511	011	$2.570(14) \times 3$ 2 564(12) × 3	1.709
Ba2	08	$2.313(10) \times 3$ $3.071(8) \times 2$	1 706	Ba2	08	$3.074(9) \times 2$	1.545
Daz	00	$3.071(0) \times 2$ $3.004(9) \times 2$	1.700			3.019(10)	
	09	2.684(11)			O9	3.018(13) × 2	
	010	$2.781(4) \times 2$			O10	$2.765(6) \times 2$	
	O11	$3.081(2) \times 2$			O11	$3.046(6) \times 2$	
		3.32(2)				3.26(2)	
Ba3	08	$2.904(8) \times 6$	2.263	Ba3	08	$2.859(9) \times 6$	3.642
	09	$2.980(9) \times 3$			09	$2.650(11) \times 3$	
0.500.4	O10	$2.852(10) \times 3$	2 000	G45/S+4	010	$2.023(11) \times 3$ $2.401(0) \times 2$	2 144
5m5/Sr4	08	$2.439(7) \times 2$	3.088	005/314	08	$2.401(9) \times 2$ 2 296(0) $\times$ 2	3.144
	00	$2.325(7) \times 2$			09	$2.230(5) \times 2$ 2.439(5) × 2	
	09	2.322(4) × 2 2.528(10)			010	2.598(12)	
	010	2.599(9)			- *	2.513(10)	
Co6	09	$2.021(7) \times 3$	2.641	Co6	O9	1.929(8) × 3	3.307
	010	$1.987(7) \times 3$			O10	1.912(8) × 3	
Co7	08	1.864(6) × 2	2.651	Co7	08	$1.867(6) \times 2$	2.577
	O9	1.865(8)			09	1.899(9)	
					011	1.822(9)	

TABLE IV(b).	Bond distances and bond valence sum values $(V_b)$ for
$Ba_5SrR_2Co_4O_{15}$ .	Values inside brackets are standard deviations.

TABLE IV(b). Continued

Atom	Atom	Distances	$V_{\rm b}$	Atom	Atom	Distances	$V_{\rm b}$
(i) D L -					O15	1.741(6)	
(1) $K = La$ $R_{0.1}/S_{r/2}$	015	$2680(10) \times 2$	1 777	(iv) $R = Eu$			
Da1/312	015	$2.069(10) \times 3$ 2.641(7) × 3	1.///	Ba1/Sr2	015	$2.640(9) \times 3$	2.037
Ba3	012	$2.041(7) \times 3$ 3.083(7) $\times 2$	1 624	5.4		$2.589(7) \times 3$	
Dus	012	$3.025(7) \times 2$	1.024	Ba3	012	$2.986(6) \times 2$	1.716
	013	2.684(8)			012	$2.997(6) \times 2$	
	014	$2.807(2) \times 2$			013	2.777(7)	
	015	$3.144(3) \times 2$			014	$2.7742(14) \times 2$ $3.118(2) \times 2$	
		3.238(12)			015	$3.118(2) \times 2$ 3.168(10)	
Ba5	O12	$2.959(7) \times 6$	1.883	Ba5	012	$2.905(6) \times 6$	2 308
	O13	$3.084(7) \times 3$		DaJ	012	$2.995(0) \times 0$ 2.898(7) $\times 3$	2.508
	O14	$2.919(7) \times 3$			014	$2.000(7) \times 3$	
La9/Ba7/Sr8	O12	$2.497(6) \times 2$	3.468	Ba7/Sr8/I a9	012	$2.703(7) \times 3$ 2.504(6) × 2	3 107
		$2.407(5) \times 2$		Da//010/Ea/	012	$2.304(0) \times 2$ 2.372(5) × 2	5.107
	O13	$2.542(2) \times 2$			013	$2.4916(14) \times 2$	
	O14	2.492(7)			014	2.555(7)	
		2.634(6)				2.592(6)	
Co10	O13	$2.047(5) \times 3$	2.567	Co10	013	$1.979(5) \times 3$	3.044
	O14	$1.984(6) \times 3$			O14	1.925(6) × 3	
Col1	012	$1.833(5) \times 2$	2.844	Co11	012	$1.826(4) \times 2$	2.836
	O13	1.881(6)			013	1.917(5)	
	015	1.767(6)			015	1.757(6)	
(ii) $R = Nd$				(iv) $R = Gd$			
Ba1/Sr2	015	$2.615(9) \times 3$	2.053	Ba1/Sr2	015	$2.634(8) \times 3$	2.082
_		$2.606(7) \times 3$				$2.579(6) \times 3$	
Ba3	012	$2.929(7) \times 2$	1.768	Ba3	O12	$2.910(6) \times 2$	1.807
		$2.989(6) \times 2$				$2.993(6) \times 2$	
	013	2.747(8)			O13	2.767(7)	
	014	$2.7795(11) \times 2$			O14	$2.7646(10) \times 2$	
	015	$3.128(2) \times 2$			015	$3.124(2) \times 2$	
D. (	012	3.228(10)	1.074			3.167(8)	
Bas	012	$3.08/(6) \times 6$	1.974	Ba5	O12	$3.072(6) \times 6$	2.164
	013	$2.980(8) \times 3$			O13	$2.908(7) \times 3$	
Do7/S#9/NI40	014	$2.773(8) \times 3$ $2.556(6) \times 2$	2 1 2 4		O14	$2.746(7) \times 3$	
Da//516/INU9	012	$2.330(0) \times 2$	5.154	Ba7/Sr8/La9	012	$2.539(5) \times 2$	3.031
	012	$2.405(0) \times 2$				$2.373(5) \times 2$	
	013	$2.5039(12) \times 2$			013	$2.4866(10) \times 2$	
	014	2.508(8)			O14	2.547(6)	
Co10	013	2.342(7) 2.014(6) × 3	2 878	~		2.558(6)	
010	014	$1.934(7) \times 3$	2.070	Co10	013	$1.980(5) \times 3$	3.090
Coll	012	$1.936(5) \times 2$	2 772	0.11	014	$1.914(6) \times 3$	2 702
com	013	1.030(5) × 2	2.772	Coll	012	$1.834(4) \times 2$	2.792
	015	1.758(7)			013	1.939(5)	
(iii) $R = Sm$					015	1.749(0)	
Ba1/Sr2	015	$2.641(8) \times 3$	2.061				
		$2.580(7) \times 3$					
Ba3	O12	2.915(6) × 2	1.832	the 11- and 12-	fold coordinated	l Ba–O polyhedra and	l the 8-fold
		2.987(6) × 2		coordinated R/S	r_O or R/Ba/Sr-	-O polyhedra are not (	drawn The
	O13	2.724(7)		unit_cell outline	is also illustrate	d There are two Co.(	D clusters
	O14	$2.7671(10) \times 2$		non unit coll the	is also intustiate	ained by verieus lent	bonido and
	O15	$3.135(2) \times 2$				Sined by various failu	
		3.164(9)		alkaline-earth ca	ations that are in	1 6-fold (octahedral Sr	$O_6$ ), 8-fold
Ba5	O12	3.081(6) × 6	2.043	(bisdisphenoid	$(R/Sr)O_8), 10$	-fold (capped trigor	nal prism,
	O13	$2.972(7) \times 3$		$BaO_{10}$ ), and 12	-fold (cubic clo	ose packed, $BaO_{12}$ ) co	oordination
	O14	$2.752(7) \times 3$		to various oxyge	en ions. In Ba <sub>5</sub> Sr	$Gd_2Co_4O_{15}$ , the octahe	edral cation
Ba7/Sr8/Sm9	O12	$2.563(6) \times 2$	3.037	positions are ran	domly occupied	by an equal amount of	f Sr and Ba,
		$2.395(5) \times 2$		and the bisdisph	enoid cation po	sitions are randomly o	ccupied by
	013	$2.4960(10) \times 2$		2/3R = 1/6Ra and	d 1/6Sr In Ra	$Sr_2R_2C_0O_{12}$ the bis	disphenoid
	O14	2.556(7)		cotion positions	a = 1/0.51. III $Da$	$\frac{101}{102}$	and 1/2°
G 10	~	2.530(6)		Element 5	the example of the	n anning mark of D	anu 1/331.
Co10	013	$2.001(6) \times 3$	2.999	Figure 5 gives	une coordinatio	n environment of Ba	exhibiting
G 11	014	$1.917(6) \times 3$		both 10-fold and	a 12-told coordi	nation.	
Coll	012	$1.837(5) \times 2$	2.792	Tables IV(	a) and IV(b) g	give the bond distand	ces of Ba/
	013	1.945(6)		Sr–O, <i>R</i> –O, an	nd Co-O, and	bond valence sum v	values $(V_b)$
			Continued	for $Ba_4Sr_2R_2C_4$	0 <sub>4</sub> O <sub>15</sub> and Ba <sub>5</sub>	$SrR_2Co_4O_{15}$ , respect	ively. The

TABLE V. X-ray powder pattern for  $Ba_4Sr_2Gd_2Co_4O_{15}$  ( $P6_{3}mc$  (No. 186), a = 11.5872(4) Å, c = 6.8169(2) Å, V = 792.63(6) Å<sup>3</sup>, Z = 2, and  $D_x = 6.35$  g cm<sup>-3</sup>). The symbols "M" and "+" refer to peaks containing contributions from two and more than two reflections, respectively. The symbol \* indicates that the particular peak has the strongest intensity of the entire pattern and is designated a value of "999."

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	L
3.7928       6       2       1       0       3.4084       3.8       0       0       2       3.3143       149       2       1       1       3.2274       75       1       0       2       3.0029       106       3       0         2.5767       35       3       1       1       2.5352       144       2       1       2       2.3874       348       3       0         2.2073       55       2       2       2       2.1811       46       3       2       1       2.1558       26       3       1         2.2073       55       2       1       3       1.9312       18       3       3       0       1.9252       95       5       0         1.9078       17       3       2       2       1.8796       14       3       0       3       1.8423       214       4       1         1.4270       40       4       2       1       1.8023       26       5       0       2       1.7042       6       0       0       1.6572       91       4       2       2       1.6137       125       2       0       1       1.5645	1
3.314.3       1.49       2       1       1       3.2274       75       1       0       2       3.0029       106       3       0         2.9378       3.29       1       1       2.5866       999*       2       2       0       2.8194       461       2       0         2.3543       1.34       4       0       1       2.3021       20       3       2       0       2.2162       89       1       0         2.073       55       2       2       2.181       46       3       2       1       2.1658       2.6       3       1       1.52084       4       0       1       2.0204       1.83       4       0         1.9492       5       2       1       3       1.9312       18       3       0       1.9252       95       5       0       0         1.9078       17       3       2       2       1.8796       14       3       0       3       1.8423       2.14       4       1       1.14       1.17294       811       5       0       2       1.7642       64       1       1       1.41.5437       101       3       2	0
2.9378       3.29       1       1       2       2.8068       999*       2       2       0       2.8194       4.61       2       0         2.5767       35       3       1       1       2.5321       1.44       2       1       2       2.814       3.84       0         2.2073       55       2       2       2       2.1811       4.6       3       2       1       2.1558       2.6       3       1         2.2073       55       2       2       2       2.1811       4.6       3       2       1.21558       2.6       3       1         1.9402       5       2       1       3       1.9312       1.8       3       3       0       1.9252       95       5       0         1.9078       17       3       2       2       1.8706       14       3       0       3       1.8423       2.14       4       1         1.8073       9       5       1       0       1.7622       30       3       1       1.5636       7       4       1         1.6641       1       4       1.6172       101       3       2	1
25767       35       3       1       1       2.5352       144       2       1       2       2.8874       348       3       0         2.3543       134       4       0       1       2.3021       20       3       2       0       2.1558       26       3       1         2.0848       71       4       1       1       2.0699       21       2       0       3       2.0204       183       4       0         1.9492       5       2       1       3       1.9178       17       3       2       2       1.8796       14       3       0       3       1.8423       214       4       1         1.8270       40       4       2       1       1.8024       64       3       0       1.8423       21.042       6       0       0         1.6325       161       6       0       3       1.6602       64       3       3       2.0.16497       8       4       3       1         1.6344       5       2       1       1.5545       2.8       2       1       4       1.153       67       3       0       1.5443       3 <td>2</td>	2
2.3543       134       4       0       1       2.3021       20       3       2       0       2.2162       89       1       0         2.2073       55       2       2       2       2.1814       46       3       2       0       3       2.1258       26       3       1         1.9492       5       2       1       3       1.9312       18       3       3       0       1.9252       95       5       0         1.9078       17       3       2       2       1.8796       14       3       0       3       1.4823       214       4       1         1.8270       40       4       2       1       1.8023       26       5       1       0       1.7602       30       3       1         1.8270       40       4       2       1       1.6802       64       3       3       2       1.6497       8       4       3       3       1       1.6304       3       2       1.6497       8       4       3       3       1       1.5643       3       2       1.6497       8       4       3       3       1       1.5543<	2
2.2073       55       2       2       2.1811       46       3       2       1       2.1588       26       3       1         2.0488       71       4       1       1       2.0699       21       2       0       3       2.0204       183       4       0         1.4922       5       2       1       3       1.9312       18       3       0       1.9252       2.95       5       0         1.9078       17       3       2       2       1.8706       14       3       0       3       1.8423       2.14       4       1         1.7424       14       5       1       1       1.7294       81       5       0       2       1.6497       8       4       3         1.6530       64       1       1       4       1.6172       101       3       2       1.6497       7       4       1         1.6034       68       5       2       1       1.5545       28       2       1       4       1.5168       67       3       0         1.5042       14       5       0       3       1.5014       30       6	3
2.0848       71       4       1       1       2.0699       21       2       0       3       2.024       183       4       0         1.9492       5       2       1       3       1.9312       18       3       3       0       1.9252       95       5       0         1.0708       17       3       2       2       1.8766       14       3       0       3       1.8423       214       4       1         1.8727       40       4       2       1       1.8726       64       3       3       2.01       1.7042       6       0       0         1.6481       8       4       0       3       1.6802       64       3       3       2.01       1.6802       64       1       0         1.6350       66       1       1       4       1.572       10       3       2       1.6137       7       4       1         1.6540       68       5       2       1       1.5545       2.8       2       1       4.836       7       0       1.4335       21       7       1         1.4543       85       3       2	2
19492       5       2       1       3       19312       18       3       3       0       19252       95       5       0         19078       17       3       2       2       18706       14       3       0       3       18423       214       4       1         1.8270       40       4       2       1       18023       26       5       1       0       1.7602       30       3       1         1.641       8       4       0       3       1.6802       64       3       2       1.6497       8       4       3         1.6341       6       0       0       1.6572       91       4       2       2       1.6497       8       4       1         1.634       56       4       3       1       1.5933       9       5       1       2       1.5768       7       4       1         1.540       68       5       2       1       1.5545       28       2       1       4.450       9       4       2         1.4849       55       4       3       2       1.4684       122       4       4	2
$            1.9078  17  3  2  2  1.8796  14  3  0  3  1.8423  214  4  1 \\ 1.8270  40  4  2  1  1.8023  26  5  1  0  1.7602  30  3  1 \\ 1.7424  14  5  1  1  1.7294  81  5  0  2  1.7042  6  0  0 \\ 1.6841  8  4  0  3  1.6802  64  3  3  2  M  1.6802  64  1  0 \\ 1.6751  84  1  1  4  1.6172  101  3  2  3  1.6137  125  2  0 \\ 1.6034  56  4  3  1  1.5933  9  5  1  2  1.5768  7  4  1 \\ 1.5640  68  5  2  1  1.5545  28  2  1  4  4  1.5185  67  3  0 \\ 1.5042  14  5  0  3  1.5014  30  6  0  2  2  1.4931  5  6  1 \\ 1.4849  55  4  3  2  1.4689  33  2  2  4  4  0  1.4355  21  7  0 \\ 1.4334  88  5  2  2  1.4484  122  4  4  0  1.4356  9  4  2 \\ 1.4334  88  5  2  2  1.4484  122  4  4  0  1.4356  9  4  2 \\ 1.4334  88  5  3  2  1.3157  17  2  0  5  1.3120  12  5  2 \\ 1.2990  28  5  0  4  1.2883  19  6  2  2  1.2848  12  5  4 \\ 1.2778  17  3  3  4  1.2033  25  6  1  3  1.2283  41  7  1 \\ 1.2336  20  8  0  1  1  1.2124  46  7  0  3  1  1.2383  41  7  1 \\ 1.2336  20  8  0  1  1  1.2124  46  7  0  3  1  1.2383  41  7  1 \\ 1.2336  20  8  0  1  1  1.2124  46  7  0  3  1  1.2383  41  7  1 \\ 1.2336  20  8  0  1  1  1.2124  46  7  0  3  1  1.2383  41  7  1 \\ 1.2336  20  8  0  1  1  1.2124  46  7  0  3  1  1.2383  41  7  1 \\ 1.236  20  8  0  1  1  1.2124  46  7  0  3  1  1.2383  41  7  1 \\ 1.236  20  7  5  4  4  1  1.2431  11  6  3  1  1  1.2383  41  7  1 \\ 1.236  20  8  0  1  1  1.1979  18  4  0  5  1  1.1977  23  6  0  0 \\ 1.1677  11  8  7  2  1  1.1977  23  0  1  1.1774  18  8  1  1  1.1004  20  9  0 \\ 1.1774  18  4  1  5  5  1  1.1853  61  6  3  2  1  1.1974  18  8  1  1 \\ 1.1774  18  4  1  5  5  1  1.1853  61  6  5  4  1  1  1.1004  20  9  9 \\ 1  1.1774  18  8  1  1  1.1004 $	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	2
1,7424 14 5 1 1 1,7294 81 5 0 2 1,7042 6 0 0              1,6841 8 4 0 3 1,6802 64 3 0 2 1,7042 6 0 0              1,6802 64 1 0              1,6725 161 6 0 0 1,6572 91 4 2 2 1,6497 8 4 3              1,6350 64 1 1 4 4 1,6172 101 3 2 3 1,6137 125 2 0              1,6034 56 4 3 1 1,5933 9 5 1 2 1,5768 7 4 1              1,540 68 5 2 1 1,5545 28 2 1 4 1,5185 67 3 0 0              1,5042 14 5 0 3 1,5014 30 6 0 0 2 1,4931 5 6 1 1              1,4849 55 4 3 2 1,4689 33 2 2 4 4 1,4560 9 4 2 1              1,4334 88 5 2 2 2 1,4484 122 4 4 0 1,4335 21 7 0 0              1,4335 21 5 3 0 M 1,4097 59 4 0 4 1,3634 11 6 2 2 1              1,3214 8 5 3 2 1,3157 17 2 0 5 1,3120 12 5 2 1              1,324 8 5 3 2 1,3157 17 2 0 5 1,3120 12 5 2 1              1,2990 28 5 0 4 1,2883 19 6 2 2 1,2848 12 5 4 1              1,2778 17 3 3 4 1,2693 25 6 1 3 1,22783 41 7 1 1              1,2326 7 5 4 1 1,22431 11 6 3 3 1,22676 49 4 2 2 1              1,290 28 5 0 4 1,2843 19 6 2 2 1,2848 12 5 4 1              1,2778 17 3 3 4 1,2693 25 6 1 3 1,22783 41 7 1 1              1,2326 20 8 0 1 1,2124 46 7 0 3 M 1,2124 46 5 3 1              1,2066 29 7 2 1 1,1979 18 4 0 5 1,1937 23 6 0              1,2066 29 7 2 1 1,1979 18 4 0 5 1,1937 23 6 0              1,1873 61 6 3 2 M 1,1853 61 4 3 3 1              1,278 41 7 1 1              1,236 20 8 0 1 1,12124 46 7 0 3 M 1,1853 61 4 3 3 1              1,1772 11 8 0 2 1,1745 10 8 1 0 1,1731 21 3 2 1              1,091 44 5 2 4 1,1587 14 5 5 0 0 1,1574 18 8 1 1              1,1774 11 8 0 2 1,1745 10 8 1 0 1,1731 21 3 2 1              1,070 12 7 3 3 1              1,174 18 4 1 5 M 1,1587 14 5 5 0 0 1,1574 18 8 1 1              1,1374 12 5 0 5 1,1184 46 5 4 4 3 1,1104 13 8 1 1              1,1070 12 7 3 2 1              1,090 12 7 3 9 0 0              1,077 14 5 1 0 8 1 0 0,1731 21 3 2 1 3 2 1              1,0789 10 7 2 2 1              1,0789 10 7 2 1              1,0789 10 7 2 1              1,0789 10 7 2 1              1,0789 10 7 2 1              1,	3
1.6841 8 4 0 3 1.6802 64 3 3 2 M 1.6802 64 1 0              1.6725 161 6 0 0 1.6572 91 4 2 2 1.6497 8 4 3              1.6137 125 2 0 1              1.6034 56 4 3 1 1.5913 9 5 1 2 1.5768 7 4 1              1.5404 55 2 1 1.5545 28 2 1 4 1.5185 67 3 0 0              1.5042 14 5 0 3 1.5014 30 6 0 2 1.4931 5 6 1 1              1.4849 55 4 3 2 1.4689 33 2 2 4 4 0 1.4355 21 7 0 0              1.4334 88 5 2 2 1 4.4848 122 4 4 0 1.4355 21 7 0 0              1.4335 21 5 3 0 M 1.4097 59 4 0 4 1.3634 11 6 2 1              1.3214 88 5 3 2 2 1.41844 122 4 4 0 1.4335 21 7 0 0              1.3314 7 1 1 6 2 2 1.2848 12 5 4 1 .225 2 1              1.3494 58 4 1 4 1.3330 23 4 4 2 1.3291 13 7 1 1 6 2 2 1              1.3214 8 5 3 3 2 1.3157 17 2 0 5 1.3120 12 5 2 1              1.2990 28 5 0 4 1.2883 19 6 2 2 1.2848 12 5 4 1 .2778 17 3 3 4 1.2693 25 6 1 3 1.2676 49 4 2 2 1 .2848 12 5 4 1 .2778 17 3 3 4 1.2693 25 6 1 3 1.2676 49 4 2 2 1 .2848 12 5 4 1 .2778 17 3 3 4 1.2693 25 6 1 3 1.2676 49 4 2 2 1 .2848 12 5 4 1 .2778 17 3 3 4 1.2693 25 6 1 3 1.2676 49 4 2 2 1 .2848 12 5 4 1 .2778 17 3 3 4 1.2693 25 6 1 3 1.2676 49 4 2 2 1 .2848 12 5 4 1 .12736 20 8 0 1 1 .12124 46 7 0 3 3 M 1.2124 46 5 3 1 .2666 29 7 2 2 1 .11853 61 6 3 2 M 1.1853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 3 .1.853 61 4 3 .3 .1.853 61 4 3 .3 .1.857 14 5 5 0 0 .1.1574 18 8 1 1 .1.104 13 8 1 1 .1.1070 12 7 3 .3 .1.857 14 5 5 0 0 .1.1574 18 8 1 .4 .1.858 61 4 3 .2 .1.1853 61 6 .3 .2 M 1.1853 61 4 3 .3 .1.1074 13 8 .1 .1.1070 12 7 .3 .3 .1.1077 14 8 5 5 .2 M 1.0970 18 5 .3 .4 M 1.0999 10 7 .2 .1.1367 14 .2 .2 .1.1587 14 4 .3 .2 .1.1587 14 .5 .5 .0 .1.1574 18 8 1 .1 .1.109 0 12 .7 .3 .3 .1.1077 14 .2 .2 .5 .1.1037 15 4 4 4 .1 .1.1090 12 .7 .3 .3 .1.1077 14 .2 .2 .6 .1.1350 15 6 .4 .1 .1.104 13 8 .1 .2 .1.1079 10 .7 .2 .1.1079 10 .2 .4 .1.0717 8 7 .3 .2 .1.0597 2.3 .9 .0 .1.0577 14 .2 .4	4
$            1.6725  161 \qquad 6 \qquad 0 \qquad 0 \qquad 1.6572 \qquad 91 \qquad 4 \qquad 2 \qquad 2 \qquad 1.6497 \qquad 8 \qquad 4 \qquad 3 \\            1.6330 \qquad 64 \qquad 1 \qquad 1 \qquad 4 \qquad 1.6172 \qquad 101 \qquad 3 \qquad 2 \qquad 3 \qquad 1.6137 \qquad 125 \qquad 2 \qquad 0 \\            1.6034 \qquad 56 \qquad 4 \qquad 3 \qquad 1 \qquad 1.5933 \qquad 9 \qquad 5 \qquad 1 \qquad 2 \qquad 1.5768 \qquad 7 \qquad 4 \qquad 1 \\            1.5640 \qquad 68 \qquad 5 \qquad 2 \qquad 1 \qquad 1 \qquad 1.5545 \qquad 28 \qquad 2 \qquad 1 \qquad 4 \qquad 1.5185 \qquad 67 \qquad 3 \qquad 0 \\            1.5042 \qquad 14 \qquad 5 \qquad 0 \qquad 3 \qquad 1.5014 \qquad 30 \qquad 6 \qquad 0 \qquad 2 \qquad 1.4931 \qquad 5 \qquad 6 \qquad 1 \\            1.4849 \qquad 55 \qquad 4 \qquad 3 \qquad 2 \qquad 1.4689 \qquad 33 \qquad 2 \qquad 2 \qquad 4 \qquad 1.4560 \qquad 9 \qquad 4 \qquad 2 \\            1.4354 \qquad 88 \qquad 5 \qquad 2 \qquad 2 \qquad 1.4484 \qquad 122 \qquad 4 \qquad 4 \qquad 0 \qquad 1.4355 \qquad 21 \qquad 7 \qquad 0 \\            1.4335 \qquad 21 \qquad 5 \qquad 3 \qquad 0 \qquad M \qquad 1.4097 \qquad 59 \qquad 4 \qquad 0 \qquad 4 \qquad 1.3634 \qquad 11 \qquad 6 \qquad 2 \\            1.3349 \qquad 58 \qquad 4 \qquad 1 \qquad 4 \qquad 1.330 \qquad 23 \qquad 4 \qquad 4 \qquad 2 \qquad 1.3291 \qquad 13 \qquad 7 \qquad 1 \\            1.3214 \qquad 8 \qquad 5 \qquad 3 \qquad 2 \qquad 1.3157 \qquad 17 \qquad 2 \qquad 0 \qquad 5 \qquad 1.3120 \qquad 12 \qquad 5 \qquad 2 \\            1.2990 \qquad 28 \qquad 5 \qquad 0 \qquad 4 \qquad 1.2883 \qquad 19 \qquad 6 \qquad 2 \qquad 2 \qquad 1.2848 \qquad 12 \qquad 5 \qquad 4 \\            1.2778 \qquad 17 \qquad 3 \qquad 3 \qquad 4 \qquad 1.2693 \qquad 25 \qquad 6 \qquad 1 \qquad 3 \qquad 1.2676 \qquad 49 \qquad 4 \qquad 2 \\            1.2626 \qquad 7 \qquad 5 \qquad 4 \qquad 1 \qquad 1.2431 \qquad 11 \qquad 6 \qquad 3 \qquad 1 \qquad 1.2383 \qquad 41 \qquad 7 \qquad 1 \\            1.2336 \qquad 20 \qquad 8 \qquad 0 \qquad 1 \qquad 1.2124 \qquad 46 \qquad 7 \qquad 0 \qquad 3 \qquad M \qquad 1.1853 \qquad 61 \qquad 4 \qquad 3 \\            1.1772 \qquad 11 \qquad 8 \qquad 0 \qquad 2 \qquad 1.11873 \qquad 61 \qquad 6 \qquad 3 \qquad 2 \qquad 1.11873 \qquad 61 \qquad 4 \qquad 3 \\ 1.1772 \qquad 11 \qquad 8 \qquad 0 \qquad 2 \qquad 1.11853 \qquad 61 \qquad 6 \qquad 3 \qquad 2 \qquad 1.11833 \qquad 61 \qquad 4 \qquad 3 \\ 1.1771 \qquad 11 \qquad 8 \qquad 0 \qquad 2 \qquad 1.11853 \qquad 61 \qquad 6 \qquad 3 \qquad 2 \qquad 1.11833 \qquad 61 \qquad 4 \qquad 3 \\ 1.1771 \qquad 11 \qquad 8 \qquad 0 \qquad 2 \qquad 1.11853 \qquad 61 \qquad 6 \qquad 3 \qquad 2 \qquad 1.11833 \qquad 61 \qquad 4 \qquad 3 \\ 1.1774 \qquad 18 \qquad 4 \qquad 1 \qquad 5 \qquad M \qquad 1.1536 \qquad 51 \qquad 7 \qquad 2 \qquad 2 \qquad 1.1511 \qquad 9 \qquad 6 \qquad 4 \\ 1.1362 \qquad 42 \qquad 0 \qquad 0 \qquad 6 \qquad 6 \qquad 1.11857 \qquad 14 \qquad 5 \qquad 5 \qquad 0 \qquad 1.1574 \qquad 18 \qquad 8 \qquad 1 \\ 1.1574 \qquad 18 \qquad 4 \qquad 1 \qquad 1 \qquad 5 \qquad M \qquad 1.0850 \qquad 1 \qquad 1.114 \qquad 4 \qquad 4 \qquad 1.1004 \qquad 20 \qquad 9 \qquad 0 \\ 1.0970 \qquad 18 \qquad 5 \qquad 5 \qquad 1.1087 \qquad 1.0906 \qquad 5 \qquad 1 \qquad 1.0979 \qquad 9 \qquad 7 \qquad 3 \qquad 4 \qquad 1.0906 \qquad 2 \qquad 2 \qquad 1.0178 \qquad 10 \qquad 7 \qquad 3 \qquad 3 \qquad 4 \qquad 1.0850 \qquad 2 \qquad 2 \\ 1.0779 \qquad 14 \qquad 6 \qquad 2 \qquad 2 \qquad 0 \qquad 0 \qquad 6 \qquad 1.1184 \qquad 4 \qquad 4 \qquad 1.1004 \qquad 20 \qquad 9 \qquad 0 \\ 0 \\ 1.0970 \qquad 18 \qquad 5 \qquad 5 \qquad 1.0080 \qquad 1 \qquad 4 \qquad 1.09952 \qquad 78 \qquad 7 \qquad 2 \\ 2 \qquad 1.098$	4 M
$            1.6350  64  1  1  4  1.6172  101  3  2  3  1.6137  125  2  0 \\             1.6034  56  4  3  1  1.5933  9  5  1  2  1.5768  7  4  1 \\             1.5640  68  5  2  1  1.5545  28  2  1  4  1.5185  67  3  0 \\             1.5042  14  5  0  3  1.5014  30  6  0  2  1.4931  5  6  1 \\             1.4849  55  4  3  2  1.4689  33  2  2  4  1.4560  9  4  2 \\             1.4334  88  5  2  2  2  1.4484  122  4  4  0  1.4335  211  7  0 \\             1.4335  211  5  3  0  M  1.4097  59  4  0  4  1.3634  111  6  2 \\             1.3214  8  5  3  2  1.3157  17  2  0  5  1.3120  12  5  2 \\             1.2990  28  5  0  4  1.2883  19  6  2  2  1.2848  12  5  4 \\             1.2778  17  3  3  4  1.2693  25  6  1  3  1.2766  49  4  2 \\             1.2366  20  8  0  1  1.2124  46  7  0  3  M  1.2483  411  7  1 \\             1.2366  20  8  0  1  1.2124  46  7  0  3  M  1.2124  46  5  3 \\             1.2066  29  7  2  1  1.1979  18  4  0  5  1.1937  2.3  6  0 \\             1.1853  61  6  3  2  M  1.1853  61  4  3  2 \\             1.1651  6  4  1  1.1243  11  6  5  4  1  1.1243  46  5  3 \\             1.1667  12  6  2  3  1.1853  61  6  3  2  M  1.1853  61  4  3 \\             1.1671  18  8  1  1.174  18  8  1 \\ 1.1772  11  8  0  2  1.1745  10  8  1  0  1.1574  18  8  1 \\ 1.1691  44  5  2  4  1.1587  14  5  5  0  1.1574  18  8  1 \\ 1.1691  44  5  2  4  1.1587  14  5  5  0  1.1574  18  8  1 \\ 1.1691  44  5  2  0  5  1.1184  46  5  4  3  1.1104  13  8  1 \\ 1.1671  18  8  1  1.0079  18  5  3  4  M  1.0049  37  8  2 \\ 1.0076  9  6  4  2  1.0037  15  4  4  4  4  1.0049  20  9  0 \\ 1.0779  14  6  2  4  1.0717  8  7  3  2  1.0079  23  9  0 \\ 1.0577  14  4  2  2  6  1.0509  11  4  3  5  1  M  1.0396  25  5  2 \\$	0
$            1.6034  56  4  3  1  1.5933  9  5  1  2  1.5768  7  4  1 \\ 1.5640  68  5  2  1  1.5545  28  2  1  4  1.5185  67  3  0 \\ 1.694  14  5  0  3  1.5014  30  6  0  2  1.4931  5  67  3  0 \\ 1.4849  55  4  3  2  1.4689  33  2  2  4  1.4560  9  4  2 \\ 1.4534  88  5  2  2  1.4484  122  4  4  0  1.4335  21  7  0 \\ 1.4335  21  5  3  0  M  1.4097  59  4  0  4  1.3634  11  6  2 \\ 1.3449  58  4  1  4  1.3330  23  4  4  2  1.3291  13  7  1 \\ 1.3214  8  5  3  2  1.3157  17  2  0  5  1.3120  12  5  2 \\ 1.2900  28  5  0  4  1.2883  19  6  2  2  2  1.2848  12  5  4 \\ 1.2778  17  3  3  4  1.2693  25  6  1  3  1.2676  49  4  2 \\ 1.2626  7  5  4  1  1.2431  11  6  3  1  1.2383  41  7  1 \\ 1.2366  20  8  0  1  1.2124  46  7  0  3  M  1.2124  46  5  3 \\ 1.2066  29  7  2  1  1.1979  18  4  0  5  1.1937  23  6  0 \\ 1.1867  12  6  2  3  1.1853  61  6  3  2  M  1.1853  61  4  3 \\ 1.0771  11  8  0  2  1.1745  10  8  1  0  1.1731  21  3  2 \\ 1.1772  11  8  0  2  1.1745  10  8  1  0  1.1731  21  3  2 \\ 1.1772  11  8  0  2  1.1745  10  8  1  0  1.1731  21  3  2 \\ 1.1771  11  8  0  2  1.1745  10  8  1  0  1.1731  21  3  2 \\ 1.1771  11  8  0  2  1.1745  10  8  1  0  1.1741  18  8  1 \\ 1.1691  44  5  2  4  1.1587  14  5  5  0  1.1574  18  8  1 \\ 1.1671  12  0  6  1.1350  15  6  4  1  1.1290  12  7  3 \\ 1.1278  12  5  0  5  1.1184  46  5  4  3  1.1104  20  9  0 \\ 0  0  0  0  0  0  0  0  0$	4
$            1.5640  68  5  2  1  1  1.5545  28  2  1  4  1.5185  67  3  0  1 \\ 1.5042  14  5  0  3  1.5014  30  6  0  2  1.4931  5  6  1 \\ 1.4849  55  4  3  2  1.4484  122  4  4  0  1.4335  21  7  0 \\ 1.4335  21  5  3  0  M  1.4097  59  4  0  4  1.3634  11  6  2 \\ 1.3449  58  4  1  4  1.3330  23  4  4  2  1.3291  13  7  1 \\ 1.3214  8  5  3  2  1.3157  17  2  0  5  1.3120  12  5  2 \\ 1.2990  28  5  0  4  1.2883  19  6  2  2  2  1.2848  12  5  4 \\ 1.2778  17  3  3  4  1.2693  25  6  1  3  1.2676  49  4  2 \\ 1.2626  7  5  4  1  1.2431  11  6  3  1  1.2383  41  7  1 \\ 1.2336  20  8  0  1  1  1.2124  46  7  0  3  M  1.2124  46  5  3 \\ 1.2066  29  7  2  1  1  1.1979  18  4  0  5  1  1.937  23  6  0 \\ 1.1867  12  6  2  2  4  1  1.1853  61  4  3 \\ 1.1772  11  8  0  2  1  1.1745  10  8  1  0  1  1.1731  21  3  2 \\ 1.1691  44  5  2  4  1  1.587  14  5  5  0  1  1.574  18  8  1 \\ 1.1362  42  0  0  6  1  1.350  15  6  4  1  1  1.1290  12  7  3 \\ 1.1278  12  5  0  5  1  1.184  46  5  4  3  1  1.1004  13  8  1 \\ 1.1772  11  8  4  1  5  M  1.1536  51  7  2  2  1  1.574  18  8  1 \\ 1.1774  18  4  1  5  M  1.1536  51  7  2  2  1  1.574  18  8  1 \\ 1.1774  18  4  1  5  M  1.1536  51  7  2  2  1  1.574  18  8  1 \\ 1.1774  18  4  1  5  5  1  1.184  46  5  4  3  1  1.1004  13  8  1 \\ 1.1770  20  4  2  5  1  1.037  15  4  4  4  4  1  1.004  20  9  0 \\ 1.0577  114  2  2  6  1  0.509  11  4  3  5  1  1.0048  15  7  1 \\ 1.0424  34  8  2  2  1  0.059  11  4  3  5  1  0.0597  23  9  0 \\ 1.0577  114  2  2  6  1  0.0599  11  4  3  5  1  0.0597  23  9  0 \\ 0.0577  114  2  2  4  1  0.0599  2  78  7  4  2  1  0.0595  5  5  2  2 \\ 1.0286  15  7  4  1  1  0.059  2  5  5  5  1 $	3
1.5042 14 5 0 3 1.5014 30 6 0 2 1.4931 5 6 1              1.4849 55 4 3 2 1.4689 33 2 2 4 1.4560 9 4 2              1.4534 88 5 2 2 2 1.4484 122 4 4 0 1.43560 9 4 2              1.4335 21 5 3 0 M 1.4097 59 4 0 4 1.3634 11 6 2              1.3435 21 5 3 0 M 1.4097 59 4 0 4 1.3634 11 6 2              1.349 58 4 1 4 1.3330 23 4 4 2 2 1.3291 13 7 1              1.3214 8 5 3 2 1.3157 17 2 0 5 1.3120 12 5 2              1.2990 28 5 0 4 1.2883 19 6 2 2 1.2848 12 5 4              1.2978 17 3 3 4 1.2693 25 6 1 3 1.2676 49 4 2              1.2266 7 5 4 1 1.2431 11 6 3 1 1.2383 41 7 1              1.2336 20 8 0 1 1.2124 46 7 0 3 M 1.2124 46 5 3              1.2066 29 7 2 1 1.11979 18 4 0 5 1.1937 23 6 0              1.2066 29 7 2 1 1.11979 18 4 0 5 1.1937 23 6 0              1.2066 29 7 2 1 1.11979 18 4 0 5 1.1937 23 6 0              1.1867 12 6 2 3 1.1853 61 6 3 2 M 1.1853 61 4 3              1.1731 21 3 2              1.691 44 5 2 4 1.1587 14 5 5 0 1.11517 48 8 1              1.1574 18 4 1 5 M 1.1536 51 7 2 2 2 1.1511 9 6 4              1.1574 18 4 1 5 M 1.1536 51 7 2 2 2 1.1511 9 6 4              1.1574 18 4 1 5 M 1.1536 51 7 2 2 2 1.1511 9 6 4              1.1574 18 4 1 5 M 1.1536 51 7 2 2 2 1.1511 9 6 4              1.1574 18 4 1 5 M 1.1536 51 7 2 2 1.1511 9 6 4              1.1574 18 4 1 5 M 1.1536 51 7 2 2 2 1.1511 9 6 4              1.1574 18 4 1 5 M 1.1536 51 7 2 2 1.1511 9 6 4              1.1574 18 4 1 5 M 1.1536 51 7 2 2 2 1.1511 9 6 4              1.1574 18 4 1 5 M 1.1536 51 7 2 2 2 1.1511 9 6 4              1.0970 18 5 5 2 M 1.0970 18 5 3 4 4 1 1.00789 10 7 2              1.0970 18 5 5 2 M 1.0970 18 5 3 4 4 M 1.0949 37 8 2              1.0970 18 5 5 2 M 0.9950 11 4 3 3 5 1.04481 15 7 1 1              1.0789 10 7 2 2              1.0779 14 6 2 4 1.0717 8 7 3 2 1.05577 23 9 0              1.0779 14 6 2 4 1.0717 8 7 3 2 1.05577 23 9 0              1.0779 14 6 2 4 0.09650 16 5 5 1 M 1.0052 33 6 5              1.0052 33 9 1 2 M 0.9952 78 7 7 4 2 M 0.9952 78 7 2	4
	1
1.4534885221.44841224401.433521701.433521530M1.4097594041.363411621.3449584141.3330234421.329113711.321485321.3157172051.312012521.2990285041.2883196221.284812541.2778173341.2693256131.238341711.2336208011.212446703M1.212446531.2066297211.1979184051.193723601.167112621.1745108101.173121321.1691445241.1587145501.157418811.1671145501.1574185111.29012731.1691444151.1037154441.100420901.16741	3
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0 M
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2 2 N
1.20001.237211.1979184031.19572.3001.1867126231.185361632M1.185361431.1772118021.1745108101.173121321.1691445241.1587145501.157418811.157418415517221.15119641.1362420061.1350156411.129012731.1278125051.1184465431.110413811.070204251.1037154441.100420901.097018552M1.097018534M1.094937821.090696421.081068211.078910721.0779146241.071787321.059723901.05771142261.0509114351.048115711.	5 IV
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 N
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0
1.0779       14       6       2       4       1.0717       8       7       3       2       1.0597       23       9       0         1.0577       114       2       2       6       1.0509       11       4       3       5       1.0481       15       7       1         1.0424       34       8       2       2       1.0396       25       6       5       1       M       1.0396       25       5       2         1.0286       15       7       4       1       1.0154       19       6       3       4       1.0052       33       6       5         1.0052       33       9       1       2       M       0.9952       78       7       4       2       M       0.9952       78       7       2       0.9884       6       8       2       0       0.9879       9       7       0       5       0.9864       6       8       2       0.9739       18       6       2       5       0.9671       8       8       1       4       0.9656       16       6       6       6       6       6       6       6       6 <t< td=""><td>3</td></t<>	3
1.0577       114       2       2       6       1.0509       11       4       3       5       1.0481       15       7       1         1.0424       34       8       2       2       1.0396       25       6       5       1       M       1.0396       25       5       2         1.0286       15       7       4       1       1.0154       19       6       3       4       1.0052       33       6       5         1.0052       33       9       1       2       M       0.9952       78       7       4       2       M       0.9952       78       7       2       0.9888       8       9       2       0       0.9879       9       7       0       5       0.9864       6       8       2         0.9739       18       6       2       5       0.9671       8       8       1       4       0.9656       16       6       6	2
1.0424       34       8       2       2       1.0396       25       6       5       1 M       1.0396       25       5       2         1.0286       15       7       4       1       1.0154       19       6       3       4       1.0052       33       6       5         1.0052       33       9       1       2 M       0.9952       78       7       4       2 M       0.9952       78       7       2         0.9888       8       9       2       0       0.9879       9       7       0       5       0.9864       6       8       2         0.9739       18       6       2       5       0.9671       8       8       1       4       0.9656       16       6       6	4
1.0286       15       7       4       1       1.0154       19       6       3       4       1.0052       33       6       5         1.0052       33       9       1       2 M       0.9952       78       7       4       2 M       0.9952       78       7       2         0.9888       8       9       2       0       0.9879       9       7       0       5       0.9864       6       8       2         0.9739       18       6       2       5       0.9671       8       8       1       4       0.9656       16       6       6	5 M
1.0052       33       9       1       2 M       0.9952       78       7       4       2 M       0.9952       78       7       2         0.9888       8       9       2       0       0.9879       9       7       0       5       0.9864       6       8       2         0.9739       18       6       2       5       0.9671       8       8       1       4       0.9656       16       6       6	2 M
0.9888         8         9         2         0         0.9879         9         7         0         5         0.9864         6         8         2           0.9739         18         6         2         5         0.9671         8         8         1         4         0.9656         16         6         6         6	4 M
0.9739 18 6 2 5 0.9671 8 8 1 4 0.9656 16 6 6	3
	0
0.9611 21 7 5 0 M 0.9611 21 5 1 6 M 0.9582 7 5 5	4
0.9560 6 2 0 7 0.9539 9 6 4 4 0.9525 6 10 1	0
0.9482 9 8 4 0 0.9432 16 2 1 7 0.9412 11 7 3	4
0.9398 61 6 0 6 0.9392 12 8 4 1 0.9350 15 5 4	5 M
0.9350 15 3 0 7 M 0.9330 16 9 0 4 0.9297 8 8 3	3
0.9290 14 6 6 2 0.9277 23 9 3 0 0.9270 6 6 3	5
0.9251         20         7         5         2         0.9231         6         8         0         5         0.9212         45         8         2	4
0.9176 27 10 0 3 M 0.9176 27 10 1 2 M 0.9116 21 7 2	5
0.9066 33 9 2 3 0.9012 16 10 2 0 0.8951 61 6 5	4 +
0.8938 77 4 4 6 M 0.8938 77 10 2 1 M 0.8904 17 7 0	6 +
0.8898 12 4 1 7 0.8881 34 7 4 4 0.8812 26 11 0	2
0.8795 16 6 4 5 0.8761 18 5 0 7 0.8751 13 8 4	3
0.8701 19 11 1 0 M 0.8701 19 9 4 0 M 0.8663 11 4 2	7
0.8636 12 7 1 6 0.8631 13 9 4 1 M 0.8631 13 9 0	5 M
0.8568 7 5 1 7 0.8552 29 8 5 2	

results of bond valence calculations show that Co atoms in both octahedral and tetrahedral sites are all of a 3+ valence instead of a 2+ valence. From R = La to R = Gd, all Co<sup>3+</sup> sites experience tensile stress, or underbonding (in an over-

sized cage environment) as  $V_{\rm b}$  values are all smaller than the ideal valence of 3+. However, the  $V_{\rm b}$  values for the octahedral Co site in the Dy-analog are substantially greater than 3.0 (compressive strain). The  $V_{\rm b}$  values for Ba<sub>4</sub>Sr<sub>2</sub> $R_2$ Co<sub>4</sub>O<sub>15</sub>

and  $Ba_5SrR_2Co_4O_{15}$  suggest that all  $Ba^{2+}$  and  $Sr^{2+}$  sites (except for Ba3) are under tensile stress. The  $V_{\rm b}$  of Ba3 changes from 1.886 to 3.642 in  $Ba_4Sr_2R_2Co_4O_{15}$  and from 1.883 to 3.031 in  $Ba_5SrR_2Co_4O_{15}$  as the ionic radius decreases from La<sup>3+</sup> to Dy<sup>3+</sup> and from La<sup>3+</sup> to Gd<sup>3+</sup>, respectively, the Ba3 cage changes from under tensile stress to compressive stress. In the R = Dy analog, the large compressive stress at Ba3 ( $V_{\rm b}$  = 3.6) and at Co6 ( $V_{\rm b}$  = 3.3) imply maximum strain or the last member (with the smallest lanthanide ion) that  $Ba_4Sr_2R_2Co_4O_{15}$  can form. Note that most of the  $V_{\rm b}$  values for R–O in Ba<sub>4</sub>Sr<sub>2</sub>R<sub>2</sub>Co<sub>4</sub>O<sub>15</sub> and  $Ba_5SrR_2Co_4O_{15}$  are significantly greater than the ideal value for that site. Since all R sites are mixed with Sr or with Sr and Ba, the ideal  $V_{\rm b}$  value is 2.666 (2/3 × 3 + 1/  $3 \times 2 = 2.666$ ), the values here, ranging from 2.842 to 3.144 are all greater than 2.666, representing a large compressive stress or overbonding for the R sites except for the phase with R = Dy. All  $V_b$  values for the cobalt sites are mostly less than 3.0, suggesting compressive stress.

#### B. Reference X-ray diffraction patterns

An example of the reference patterns of  $Ba_4Sr_2Gd_2Co_4O_{15}$ is given in Table V. In this pattern, the symbols "M" and "+" refer to peaks containing contributions from two and more than two reflections, respectively. The symbol \* indicates that the particular peak has the strongest intensity of the entire pattern and has been designated a value of "999." The intensity values reported are integrated intensities rather than peak heights. All patterns have been submitted for inclusion in the Powder Diffraction File (PDF) (ICDD).

#### **IV. SUMMARY**

Crystal structure, reference patterns, and TE properties of  $Ba_4Sr_2R_2Co_4O_{15}$  (R = La, Nd, Sm, Eu, Gd, and Dy), and  $Ba_4Sr_2R_2Co_4O_{15}$  (R = La, Nd, Sm, Eu, and Gd) series of compounds have been determined. The small size of Sr (as compared to Ba) apparently gives rise to the stability of  $Ba_4Sr_2Dy_2Co_4O_{15}$ , whereas the corresponding  $Ba_5SrDy_2Co_4O_{15}$  phase is not stable. Bond valence sum calculations indicated that all Co's adopt 3+ valence states in these compounds. In the  $Ba_4Sr_2Dy_2Co_4O_{15}$  analog the large compressive stress at Ba3 ( $V_b = 3.6$ ) and at Co6 ( $V_b = 3.3$ ) imply maximum strain or the last member (with the smallest lanthanide ion) that  $Ba_4Sr_2R_2Co_4O_{15}$  can form.

- Abe, K., Doi, Y., Hinatsu, Y., and Ohoyama, K. (2006). "Magnetic properties of the spin tetramer compound Ba<sub>6</sub>Nd<sub>2</sub>Fe<sub>4</sub>O<sub>15</sub>," Chem. Mater. 18, 785– 789.
- Brese, N. E. and O'Keeffe, M. (1991). "Bond-valence parameters for solids," Acta Crystallogr. B 47, 192–197.
- Brown, I. D., and Altermatt, D. (1985). "Bond-valence parameters obtained from a systematic analysis of the inorganic crystal structure database," Acta Crystallogr. B 41, 244–247.
- Grebille, D., Lambert, S., Bouree, F., and Petricek, V. (2004). "Contribution of powder diffraction for structure refinements of aperiodic misfit cobalt oxides," J. Appl. Crystallogr. 37, 823–831.
- Hu, Y. F., Si, W. D., Sutter, E., and Li, Q. (2005). "In situ growth of c-axis-oriented Ca<sub>3</sub>Co<sub>4</sub>O<sub>9</sub> thin films on Si(100)," Appl. Phys. Lett. 86, 082103.
- Larson, A. C. and von Dreele, R. B. (2004). General Structure Analysis System (GSAS), Los Alamos National Laboratory Report LAUR 86– 748, Los Alamos, USA.
- Masset, A. C., Michel, C., Maignan, A., Hervieu, M., Toulemonde, O., Studer, F., and Raveau, B. (2000). "Misfit-layered cobaltite with an anisotropic giant magnetoresistance: Ca<sub>3</sub>Co<sub>4</sub>O<sub>9</sub>," Phys. Rev. B 62, 166–175.
- Mevs, H. and Müller-Buschbaum, H. (1990a). "Zur Kenntnis von Ba<sub>6</sub>La<sub>2</sub>Co<sub>4</sub>O<sub>15</sub>", Z. Anorg. Allg. Chem. 584, 114–118; ICSD collection code 69635.
- Mevs, H. and Müller-Buschbaum, H. (**1990b**). "Neue Verbindungen mit  $Ba_6Ln_2M_4^{3+}O_{15}$ -Typ:  $Ba_6Nd_2Fe_4O_{15}$ ,  $Ba_5SrLa_2Fe_4O_{15}$  und  $Ba_5SrNd_2Fe_4O_{15}$ ," J. Less-Common Metals **158**, 147–152.
- Mevs, H. and Müller-Buschbaum, H. (**1990c**). "Ba<sub>6</sub>Nd<sub>2</sub>Fe<sub>4</sub>O<sub>15</sub>: Ein oxometallat mit neuem strukturtyp," J. Less-Common Metals **157**, 173–178.
- Mikami, M. and Funahashi, R. (2005). "The effect of element substitution on high-temperature thermoelectric properties of Ca<sub>3</sub>Co<sub>2</sub>O<sub>6</sub> compounds", J. Solid State Chem. 178, 1670–1674.
- Mikami, M., Funashashi, R., Yoshimura, M., Mori, Y., and Sasaki, T. (2003). "High-temperature thermoelectric properties of single-crystal Ca<sub>3</sub>Co<sub>2</sub>O<sub>6</sub>," J. Appl. Phys. 94, 6579–6582.
- Minami, H., Itaka, K., Kawaji, H., Wang, Q. J., Koinuma, H., and Lippmaa, M. (2002). "Rapid synthesis and characterization of (Ca<sub>1-x</sub>Ba<sub>x</sub>)<sub>3</sub>Co<sub>4</sub>O<sub>9</sub> thin films using combinatorial methods," Appl. Surface Sci. 197, 442–447.
- Müller-Buschbaum, H. and Martin, F. D. (1992). "Syntheses und kristallstruktur von Ba<sub>4.5</sub>Ca<sub>1.5</sub>La<sub>2</sub>Fe<sub>4</sub>O<sub>15</sub>, Ba<sub>5</sub>CaEu<sub>2</sub>Fe<sub>4</sub>O<sub>15</sub>, and Ba<sub>5</sub>CaNd<sub>2</sub>Co<sub>4</sub>O<sub>15</sub>", Z. Anorg. Allg. Chem. 617, 84–88; ICSD collection code 72338.
- Müller-Buschbaum, H. and Uensal, H. (**1996**). "Zur Kenntnis  $Ba_6Pr_2Co_4O_{15}$ und  $Ba_5SrPr_2Co_4O_{15}$ ", Z. Naturf., Teil B: Anorg. Chem., Org. Chem. **51**, 453–455; ICSD collection codes 380091 and 380092.
- Nolas, G. S., Sharp, J., and Goldsmid, H. J. (2001). Thermoelectric: Basic Principles and New Materials Developments (Springer, New York).
- Rietveld, H. M. (1969). "A profile refinement method for nuclear and magnetic structures," J. Appl. Cryst. 2, 65–71.
- Rüter, I. and Müller-Buschbaum, H. k. (1990). "Zur Krsitallchemie von oxometallaten der Zusammensetzung Ba<sub>6</sub>Nd<sub>2</sub>Al<sub>4</sub>O<sub>15</sub> Neue Ergebnisse an Ba<sub>4.5</sub>Ca<sub>1.5</sub>Nd<sub>2</sub>Fe<sub>4</sub>O<sub>15</sub> und Ba<sub>5</sub>CaSm<sub>2</sub>Fe<sub>4</sub>O<sub>15</sub>," J. Less-Common Metals 162, 175–180.
- Shannon, R. D. (1976). "Revised effective ionic radii and systematic studies of interatomie distances in halides and chalcogenides," Acta Crystallogr. A 32, 751–767.
- Terasaki, I., Sasago, Y., and Uchinokura, K. (1997). "Large thermoelectric power in NaCo<sub>2</sub>O<sub>4</sub> single crystals", Phys. Rev. B 56, 12685–12687.