

# Vertical displacement detection of an aluminum nitride piezoelectric thin film using capacitance measurements

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*Piezoelectric materials have a strong interaction between their mechanical and electrical properties that translates into innovative components and circuits architectures. This work describes an original method using the electromechanical properties of the aluminum nitride (AlN) piezoelectric material to characterize its vertical extension when an electric field is applied. The novel techniques based on measurements of a planar parallel plate AlN capacitor without and with bias employing an impedance analyzer. The parallel plate capacitor theory and piezoelectric material analysis are used to calculate the vertical displacement of the AlN film.*

**Keywords:** Aluminum nitride, Characterizations, Material parameters, Piezoelectric material

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## I. INTRODUCTION

Piezoelectric materials have become very useful in MEMS devices because of their electrical–mechanical reciprocity. MEMS merge the functions of sensing and actuating with computation and communication to locally control physical parameters. Piezoelectric materials are capable of very high energy and power densities at micro scales [1]. The high frequency of operation inherent in MEMS devices matches well with the relatively high-frequency capability of piezoelectric materials. The most commonly used piezo-materials in MEMS devices are lead zirconate titanate (PZT), zinc oxide (ZnO), and aluminum nitride (AlN). AlN has attracted considerable attention in recent years owing to its unique properties. Specifically, its high thermal conductivity, moderate piezoelectricity, low dielectric and acoustic losses, and high acoustic wave velocity have made highly textured AlN thin films a prime candidate for electro-acoustic applications such as filters, resonators, and sensors. Further, its chemical stability as well as compatibility with IC processing makes AlN thin films a competitive alternative to single crystalline piezoelectric substrates for microwave applications. A comparison between various piezoelectric materials is summarized in Table 1.

Therefore, it has become increasingly important to characterize the activity of piezoelectric materials under conditions relevant to such applications. Consequently, different methods have been sought to measure the piezoelectric activity. Table 2 summarizes the different methods that are presently used to extract or to measure the activity of a piezoelectric material. Nevertheless, these techniques have been

acknowledged by the scientific community; their results still need further understanding and validation. The use of mechanical devices looks a quick and easy solution. However, the need for high precision poses a problem. Direct measurement of induced charge becomes problematic for thin films because of the properties of metallic contacts used to apply the force and to collect the piezoelectric charges. The resonance techniques are based on the assumption that samples are infinitely thin or infinitely long, and the corrections for finite dimensions must be taken into account. Moreover, the relationship of resonant and anti-resonant frequencies to the piezoelectric and elastic properties of films becomes less certain. In optical techniques the sample is constrained by the substrate whose eventual deformation by the applied field must be considered.

Recently, we have presented in [8] a promising method of measuring the vertical extension of a piezoelectric thin film using an impedance analyzer. It does this by taking the ratio of parallel plate capacitance for two different bias conditions under a set of assumptions in deriving equations for the ratio

**Table 1.** Comparison between various piezoelectric materials.

Property	PZT	ZnO	AlN
$d_{33}$	High	Moderate	Low
$d_{31}$	High	Moderate	Low
Resistance	High	High	High
Constant	Huge	High	Low
RF losses	High	Moderate	Low
Sound velocity	Slow	Slow	High
Acoustic losses	High	Moderate	Low
TEC	High	High	Low
GHz capability	Poor	Poor	Good
Ferroelectricity	Yes	Yes	No
Environment	Unfriendly		Friendly
Density	High		Low
CMOS compatible	Not	Not fully	Fully

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**Table 2.** Concepts for piezoelectric characterization.

Method	Type	Physical effect	Ref.
Laser cantilever	Optical	Bias-displacement	[2]
Wafer	Mechanical	Force-charge	[3]
Loading	Mechanical	Force-charge	[4]
Resonant	Mechanical	Force-charge	[5]
AFM	Electrical	Resonant frequency	[6]
	Mechanical	Bias-displacement	[7]

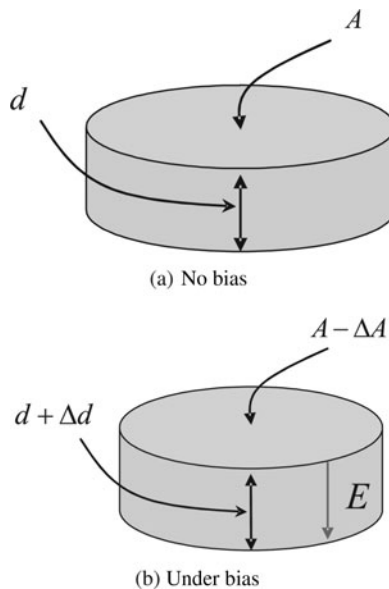
of capacitance for the two bias conditions. In this work, the determination of AlN thin-film displacement is proposed and described. The technique relies on using the impedance analyzer (or network analyzer) to measure the capacitance voltage dependence of AlN composite structure. The developed analytical model is used to extract the vertical extension of the film material. For validation, finite-element analysis is performed.

## II. THEORY AND ANALYSIS

The capacitance of a dielectric film is given by the equation [9]:

$$C_0 = \frac{\epsilon_0 \epsilon A}{d}, \tag{1}$$

where  $\epsilon_0$  is the permittivity of vacuum,  $\epsilon$  is the relative permittivity or dielectric constant,  $d$  is the thickness of the film, and  $A$  is the area of the capacitor. Having measured the capacitance of an AlN film, (1) can be used to find the electronic dielectric constant. At room temperature the piezoelectric AlN thin film material does not exhibit tunability of its dielectric constant when a dc bias field is applied. Further, AlN does not require any polling process due to its oriented structure. Figure 1(a) shows a solid circular piece of an AlN piezoelectric material. When the circular solid is driven with the application of a dc field  $E$  (Fig. 1(b)), it will cause its material



**Fig. 1.** AlN piezoelectric response to applied field.  $d_{31}$  is perpendicular to the cylindrical surface aligned with the direction of the applied field and  $d_{33}$  is parallel to the surface.

domains to contract; therefore, the thickness of the film increases by  $\Delta d$ , while the area decreases by  $\Delta A$  [10]. The modification in the material shape is translated into a change in the capacitance value, which is approximately calculated through the well-known capacitance parallel plate formula:

$$C_V = \epsilon_0 \epsilon \frac{(A - \Delta A)}{(d + \Delta d)}, \tag{2}$$

where both the vertical extension of the AlN material  $\Delta d$ , and the variation in area  $\Delta A$  are correlated with the magnitudes of both the longitudinal  $d_{33}$  and the transverse  $d_{31}$  charge constants as follows [11]:

$$\Delta d = V |d_{33}|, \tag{3}$$

$$\Delta A = V |d_{31}| A/d. \tag{4}$$

Moreover, it is well known that the magnitude of the  $d_{33}$  coefficient of the PZT is about twice the  $d_{31}$  [11]; therefore,

$$|d_{33}| = 2 \times |d_{31}|. \tag{5}$$

Thus,

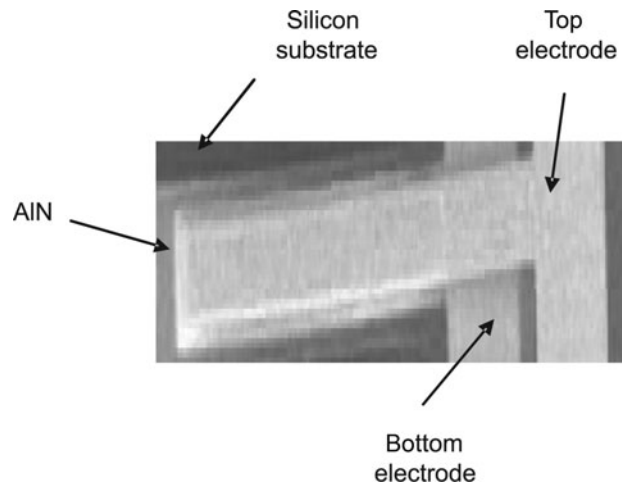
$$\frac{\Delta d}{d} \approx 2 \frac{\Delta A}{A}. \tag{6}$$

Rewrite (2) as follows:

$$C_V = \epsilon_0 \epsilon \frac{A (1 - (\Delta A/A))}{d (1 + (\Delta d/d))}. \tag{7}$$

Hence,

$$C_V = C_0 \frac{(1 - (\Delta A/A))}{(1 + (\Delta d/d))} \tag{8}$$



**Fig. 2.** Fabricated AlN parallel plate capacitor. The surface of the silicon substrate represent the  $xy$  plane, where the  $z$ -axis is perpendicular to the substrate.

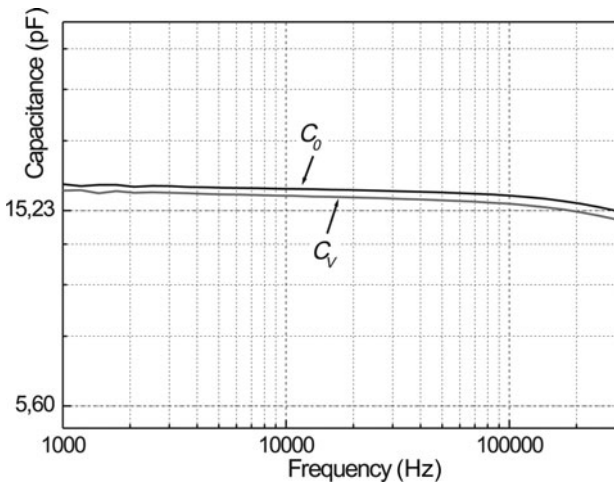


Fig. 3. AlN capacitance versus frequency (logarithmic scale):  $C_0$  is the unbiased capacitance and  $C_V$  is the capacitance with the application of 2 V.

Inserting (6) into (8) and solving for  $\Delta d$  yields:

$$\Delta d = d \left( \frac{1 - C_r}{0.5 + C_r} \right), \tag{9}$$

where  $C_r$  is the ratio between  $C_V$  and  $C_0$ .

The piezoelectric material is activated with the application of dc field and the capacitance will decrease due to the change in the geometrical dimensions as predicted by (3) and (4). Hence, knowing the thin film thickness and capacitance ratio will enable the vertical extension of the piezoelectric material to be determined.

### III. MEASUREMENTS AND ANALYSIS

A parallel plate capacitor composite of AlN piezoelectric material has been fabricated and is shown in Fig. 2. The capacitor dielectric material is composed of AlN thin film of

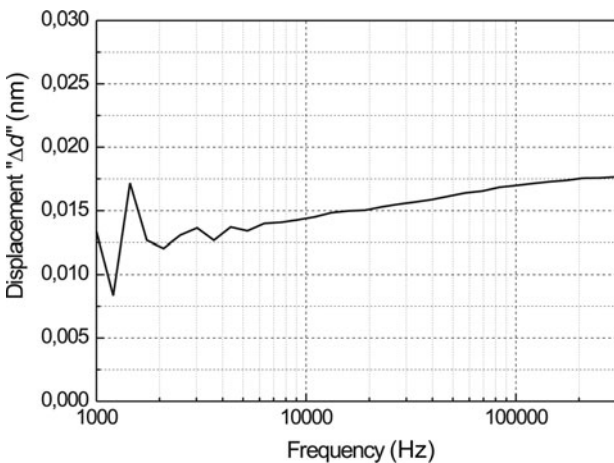


Fig. 4. Relationship between driving frequency and piezoelectric displacement.

Table 3. Material parameters.

Material parameter	Value
Young's modulus	80 (GPa)
Poisson ratio	0.22
Piezoelectric coefficient	5.7 (pm/v)

thickness 0.6  $\mu\text{m}$ . The electrodes are made from Molybdenum with a thickness of 0.1  $\mu\text{m}$ . The capacitor has an area of  $700 \times 200 \mu\text{m}^2$ . The capacitances of the fabricated device with and without dc bias were measured with the HP4294A impedance analyzer and are shown in Fig. 3. The measurements show a stable and smooth behavior over the frequency. These results represent first experimental evidence of the theory presented above. That is, applying a dc bias yields the expansion of the material due to the converse piezoelectric effect. This causes a decrease in the capacitance yielded by this structure as clearly depicted in Fig. 3. The amount of variation in capacitance due to the application of dc bias is around 3.5% from its unbiased value.

From (9) and the data of Fig. 3, the displacements of the piezoelectric material values as a function of the driven frequency are computed and are shown in Fig. 4.  $\Delta d$  shows non-stable behavior up to 2 kHz due to measurement setup that use long cables, and then becomes more stable up to 300 kHz. The value of  $\Delta d$  changes from 12.5 to 17.5 pm.

### IV. FEM ANALYSIS AND VALIDATION

The AlN material tested in this work has been measured and the results of the mechanical and electrical properties are listed in Table 3. Numerical simulations based on the finite-element method (FEM) using the piezoelectric analysis engine from CoventorWare [12] have been performed and the results are shown in Fig. 5. The simulations reveal that the vertical extension of the AlN material is homogeneously

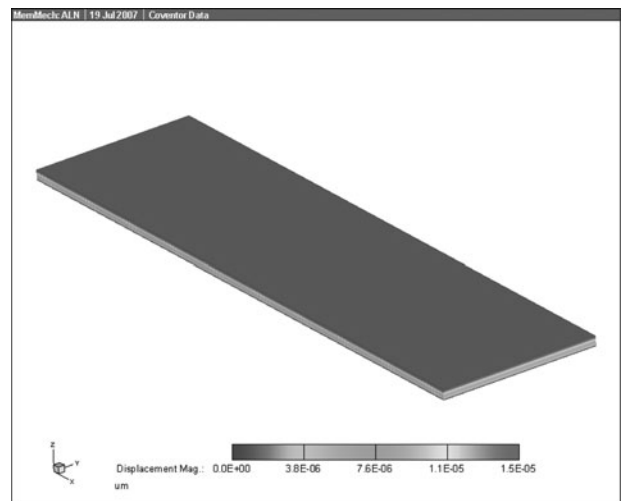


Fig. 5. Simulated vertical displacement of the AlN capacitor using FE analysis.

distributed around 15 pm. The results obtained by the proposed experimental approach and the numerical model show excellent agreement with each other. Considering the simplicity of the introduced method and the difficulty of the task, this represents a very satisfactory and promising approach.

## V. CONCLUSION

An original method for the extraction of the vertical extension of AlN piezoelectric material under dc bias is presented. The presented approach does not impose constraints or limiting conditions. The method described here is also valid for other arbitrary piezoelectric materials, but only for piezoelectric ones that are not ferroelectric. As a matter of fact, the technique circumvents complicated preparation and uses arbitrary sample geometry. It may be used to determine the piezoelectric vertical extension for films with a thickness ranging from several nanometers up to several hundreds of micrometers.

## REFERENCES

- [1] Torah, R. N.; Beeby, S. P.; White, N. M.: Experimental investigation into the effect of substrate clamping on the piezoelectric behaviour of thick-film PZT elements. *J. Phys. D: Appl. Phys.*, **37** (2004), 1074–1078.
- [2] Royer, D.; Kmetik, V.: Measurement of piezoelectric constants using an optical heterodyne interferometer. *Electron. Lett.*, **28** (19) (1992), 1828–1830.
- [3] Murali, P.: Ferroelectric thin films for micro-sensors and actuators: a review. *J. Micromech. Microeng.*, **10** (2000), 136–146.
- [4] Shepard, J. F.; Moses, P. J.; Trolrier-McKinstry, S.: The wafer flexure technique for the determination of the transverse piezoelectric coefficient ( $d(31)$ ) of PZT thin films. *Sensors Actuators A*, **71** (1998), 133–138.
- [5] Dong-Guk Kim; Ho-Gi Kim: A new characterization of piezoelectric thin films. *Appl. Ferroelectr.*, (1998), 65–68.
- [6] Zhang, Y.; Wang, Z.; Cheeke, J. D. N.: Resonant spectrum method to characterize piezoelectric films in composite resonators. *IEEE Trans. Ultrason, Ferroelectr. Frequency Control*, **50** (3) (2003), 321–333.
- [7] Gautier, B.; Ballandras, S.; Blondeau-Patissier, V.; Daniau, W.; Hauden, D.; Labrune, J.C.: Contribution to the understanding of quantitative measurements of piezoelectric coefficients of thin films using AFM piezoresponse mode. *Appl. Ferroelectr.*, (2002), 99–102.
- [8] Al-Ahmad, M.; Plana, R.: A novel method for PZT thin film piezoelectric coefficients determination using conventional impedance analyzer. in *Proc. 37th European Microwave Conf.* Munich/Germany, October 2007, 202–205.
- [9] Wadell, Brian C.: *Transmission Line Design Handbook*. Artech House: Norwood, 1991.
- [10] Nellya, N. Rogacheva: *The Theory of Piezoelectric Shells and Plates*, CRC Press LLC, New York, USA, 1994.
- [11] Jaffe, B.; Cook, W. R.; Jaffe, H.: *Piezoelectric Ceramics*, R. A. N. Publishers, Marietta, OH, 1971.
- [12] www.coventor.com



**Mahmoud Al Ahmad** was born in Jenin, West Bank, in 1976. He received his BA. degree in electrical engineering from Birzeit University, Ramallah, Palestine, in 1999 and both the M.Sc. and the Dr.-Ing. degrees in microwave engineering from Technische Universität München, Munich, Germany, in 2002 and 2006, respectively. Dr. Al Ahmad

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**Robert Plana** was born on March 1964 in Toulouse. He obtained his Ph.D. in 1993 at LAAS-CNRS and Paul Sabatier University on the Noise Modeling and Characterization of Advanced Microwave Devices, (HEMT, PHEMT and HBT) that includes reliability. In 1993, as an associate professor at LAAS-CNRS, he started a new research area concerning

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